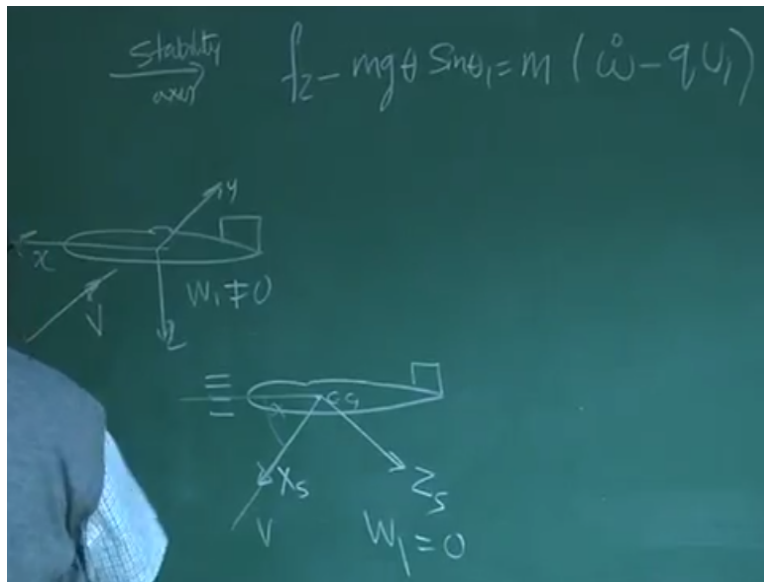


Aircraft Stability & Control
Prof. A.K.Ghosh
Department of Aerospace Engineering
Indian institute of technology-Kanpur

Lecture -46
Perturbed force

Let us take the second equation. What was second equation?

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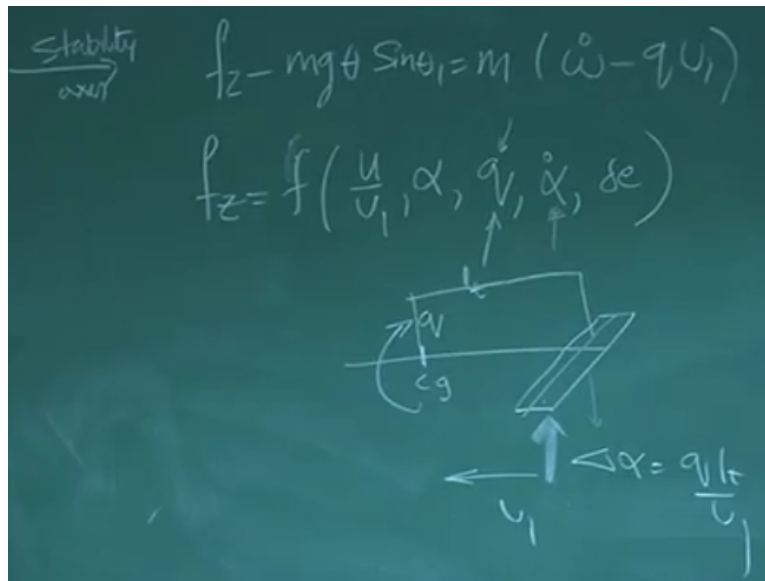


That is $f_z - mg \sin \theta = m (\dot{w} - q u_1)$. Please remember we can take stability axis system right. And I repeat what is stability axis system is this. This is an airplane this is your x , origin x is this, y is this and z is this and here the velocity vector like this, this is the normal modified axis system. If I am talking about stability axis system then what happens this airplane is this cg and this velocity vector.

So I align x axis like this and we call it x_s and this becomes z_s stability axis ok. This becomes α so I am keeping the x axis align to the velocity vector why? Because then there is no component of velocity in z direction so w_1 becomes 0, w_1 goes to zero. But here you see w_1 not equal to zero. Because this is the velocity vector there will be the component along the z direction. But here by choosing stability axis system w_1 becomes 0.

So that after applying this only you got this final equation should not forget right extremely important and why stability axis system because you know in velocity in this direction then lift but perpendicular to this dragging opposite to this. So that competitions becomes simpler again we have, will go mechanically like the way we have done.

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There we got f_z is now we are smarter will write u by u_1 then α putting it on q you make put it on α dot and δe . You might have seen in f_x modeling we have been put q and we have been put α dot. Theoretically they should be there but they are small so we have neglected it right. For f_z we need to know that why there should be q ? Which know very well that if this is the cg and if the horizontal tail or the wing whatever it is? If there is q , then this q if is going up likes this so the tail is going down. So relative air is going up like this.

And is moving forward so there will be $\Delta \alpha$. Which is $q l_t$ by u_1 right? I say l_t is the distance between aero dynamic centers. So this $\Delta \alpha$ will give you in detail force in the terms of lift and depending up on the original axis. This will have component along the z axis right. So that is why q will played important role in f_z in and you soon it will have a more most essential role in terms of movement.

pitching movement we also see that α dot will play role and will come back to the physical signification of α dot in development force is f_z when I talk about the derivative α dot

and delta e you know very well right because delta there will be a force lift and that will have a component always z know but modeling is ok. This part will be almost mechanically you see this is a first problem positively so I can write.

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The image shows a chalkboard with handwritten mathematical equations. At the top, the total force F_z is expressed as a sum of partial derivatives:

$$F_z = \frac{\partial F_{zA}}{\partial u_1} u_1 + \frac{\partial F_{zA}}{\partial \alpha} \alpha + \frac{\partial F_{zA}}{\partial q_c} q_c + \frac{\partial F_{zA}}{\partial \dot{\alpha}} \dot{\alpha} + \frac{\partial F_{zA}}{\partial \delta e} \delta e$$
 Below this, the force is written as a function of these variables:

$$F_z = f\left(\frac{u}{u_1}, \alpha, \frac{q_c}{2u_1}, \frac{\dot{\alpha}}{2u_1}, \delta e\right)$$
 On the left side of the board, there is a vertical list of variables: $\frac{u}{u_1}$, α , $\frac{q_c}{2u_1}$, and $\frac{\dot{\alpha}}{2u_1}$.

F_z as $d F_z$ by du by u_1 into u by u_1 + $d F_z$ by $d\alpha$ into α plus $d F_z$ by $d q_c$ by $2u_1$ let me write and tell you. And $d F_z$ by $d\alpha \dot{c}$ by $2u_1$ into $\alpha \dot{c}$ by $2u_1$ + $d F_z$ by $d\delta e$ into δe . You could see this two $\alpha \dot{c}$ and q_c by $2u_1$. Remember we have two convert u into non-dimensional by dividing by u_1 you want all this thing should be non-dimensional form. But you could see here these q_c $\alpha \dot{c}$ are time dimension per radian per second.

So what we do is now we write F_z as a function of u by u_1 . Then α non-dimensional for q_c we write q_c by $2u_1$. And you that q_c by $2u_1$ is non-dimensional. Then for $\alpha \dot{c}$ we write $\alpha \dot{c}$ by $2u_1$ but then δe . same theory same understanding and you need to keep this augment non-dimensional. So for u you make it u by u_1 q_c is the conventional thing q_c by $2u_1$ somebody ask why to take it as convention q_c by $2u_1$ as a non-dimensional are dimensionless ok.

So if I write like this now from here I can write $d F_z$ by du by u_1 into u by u_1 , $d F_z$ by $d\alpha$ into α , $d F_z$ by $d q_c$ by $2u_1$, $d F_z$ by $d\alpha \dot{c}$ by $2u_1$ then $d F_z$ by

d delta e into delta e correct. So what is now? What is important now? Important this. Can I get quick estimate or formulation to evaluate this derivative at steady state? Let's first attack d f z a, du by u1. Before we start doing it f z means aero dynamic perturbed force along z direction ok. So let us do that. I can write f z a is equal to minus cl into half rho v1 plus u whole square s. what is this.

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The image shows a chalkboard with the following handwritten equations:

$$F_{zA} = -C_L \frac{1}{2} \rho (u_1 + u)^2 S$$

$$F_{zA} = -C_L \frac{1}{2} \rho u_1^2 \left(1 + \frac{u}{u_1}\right)^2$$

$$\frac{\partial F_{zA}}{\partial u/u_1} = -q_{\infty} S C_L \cdot 2 \left(1 + \frac{u}{u_1}\right) - q_{\infty} S \left(1 + \frac{u}{u_1}\right)^2 \frac{\partial C_L}{\partial u/u_1}$$

$$= -q_{\infty} S C_L \cdot 2 - q_{\infty} S \frac{\partial C_L}{\partial u/u_1}$$

This I am trying to find out d f z a by du by u1. We call this is the aircraft. This is u1. And some the perturbed because perturbation this is you total speed is u1 plus u. so what will be the total force will be half rho v square u1 plus u, s into cl right. So now what I do, I write f z a is equal to minus cl into half rho u1 square s into one plus u by u1 square. No problem 1 plus u by u1 is square square fine. So now I am find out d f z a by du by u1.

So first I do like this. When I say minus q infinity s this is half rho v square s and then cl and then derivative of this then it will be 2 into 1 plus u by u1 right. Then second is minus 2 infinity s 1 plus u by u1 square into dcl by du by 1 no objection. So now I put condition at steady state. When I say at steady state what does it mean the perturbed quantity is zero. So this becomes minus q1 is cl1 into 2 this will become zero.

So minus q 1s into this is zero this goes into d cl by du by u1. So what is the final expression?

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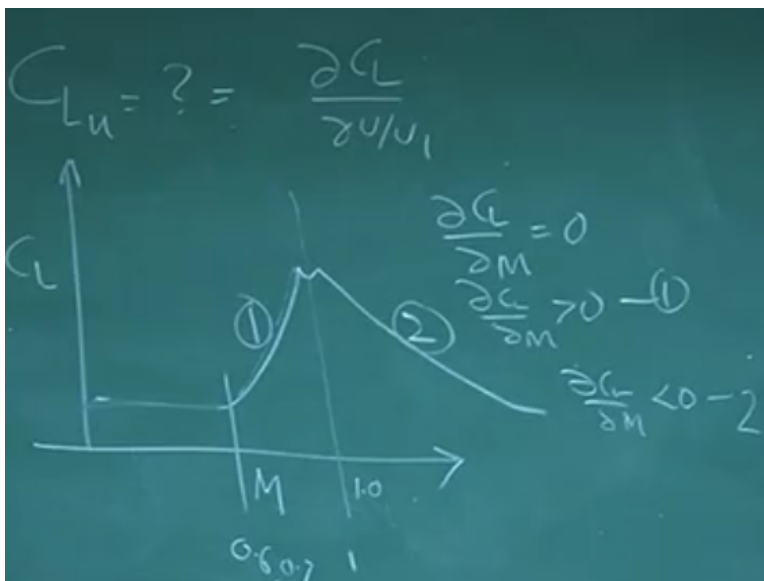
Handwritten equations on a chalkboard:

$$\frac{\partial f_z}{\partial u_1} = -q_1 s \{ 2C_{L1} + C_{L_u} \}$$

$$C_{L1} = \frac{2W_1}{\rho V_c^2}$$

Final expression is as simple as $\frac{df_z}{du_1}$ equal to minus $q_1 s$ $\{ 2C_{L1} + C_{L_u} \}$. You could see $\frac{df_z}{du_1}$ is as simple as this. This is the how many things you understand. What is q_1 ? Q_1 is the dynamic pressure at steady state. If it is cruise it is half ρv_{cruise}^2 . C_{L1} is at cruise C_{L1} will be $2W$ by $s \rho v_{cruise}^2$ that is lift equal to weight. What is C_{L_u} ? Let us understand this is C_{L_u} . This is important.

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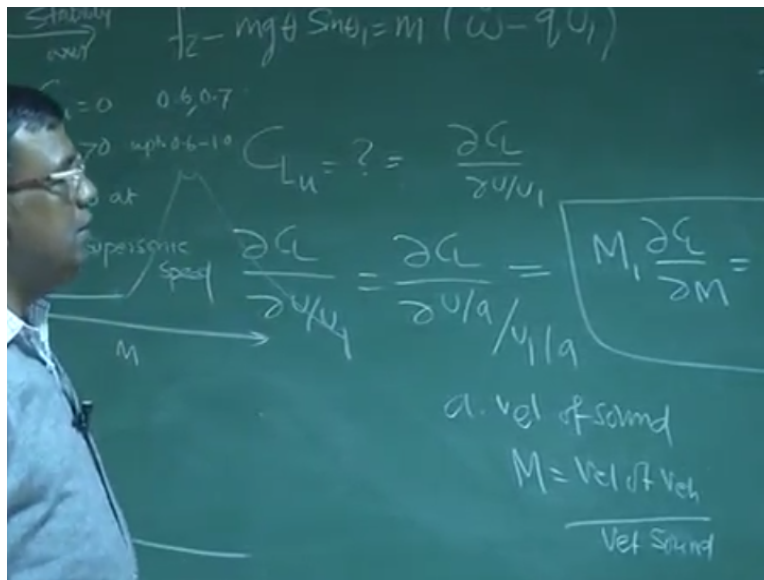


Let us focus on C_{L_u} and but finished this $\frac{dC_L}{du_1}$ right. I remember is already done something C_{D_u} ok. Let us see here if I got C_L what this Mach number will find the fort will work something that again point 16 point will past tense will goes will dip transforming and go like

this ok. To see this if I darken it go like this. And this point is in an around 1. It could be point 98. It could be point 1.2 depending around the shack the difficulty.

Now if I see here if I tack to tell you what is the DCL by DM up to 0.6 or 0.7 again this is 0 but for one region one it is DCL by DM is positive for region one .D cl by D m < 0 for region two. At react supersonic speed DCL by DM is less than zero. At subsonic is act .6 to .7 dcl by dm almost zero and between .6 to 1.1, 1.2 another around this religion slow try to means positive ok. This Must

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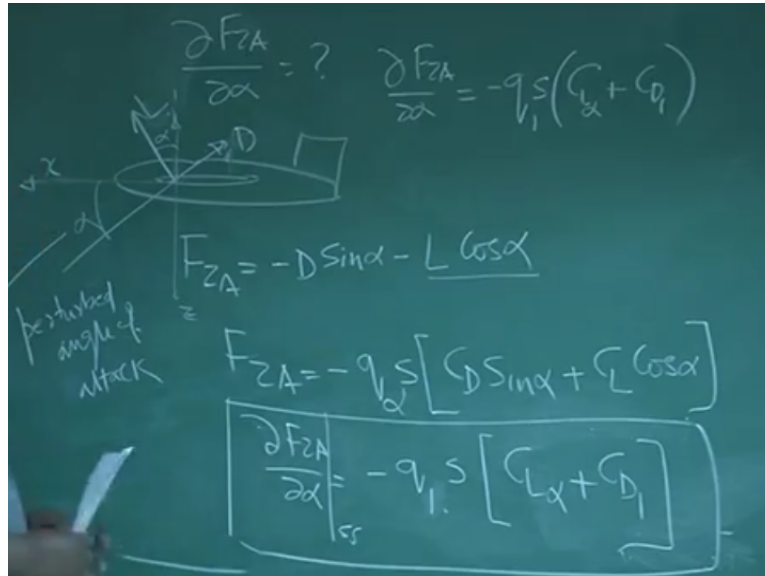


Understand this will try to interpret CLU. This Dcl by Du by u1 I can write that Dcl by Du by a you train investigate and understand dcl by du by u1 which I can write dcl by u by a. a is force velocity of sound right ok. And I assume that understand make number velocity of vehicle /velocity of sound. So this I can write as m1 into dcl by dm. this is CDU equally I can see the to this expression that not this is CLU ok right CLU I can divide by a I can m1 dcl by CLU just with cl is make number and with almost like this ok.

And you know that up to point 0.7 this DCL by DM is zero CLU will be 0 up to 0.6 to 0.7 make then CLU will positive up to 0.6-1.0 and CLU will be negative. at high supersonic speed extremely important that is what Clu. you could see that as we apply this for a high speed how

there is derivatives important role change is sign from subsonic to supersonic ok high subsonic to supersonic you understood this. fza by du by u1 so know will do.

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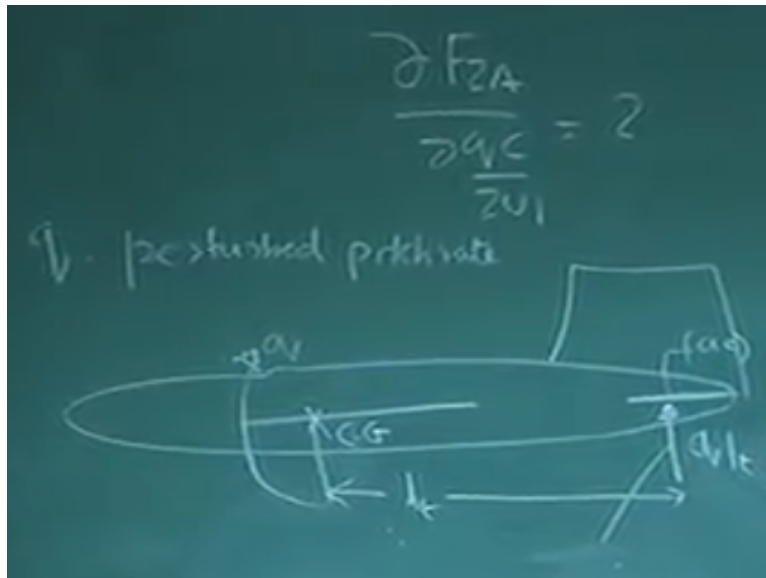


DFZA by d alpha ok what is this? If we recall when we draw this diagram calculate the d f x a by d alpha. If is there, this is alpha right. This is cl and here is cd that one this is alpha so I can right FZA= Z direction is downward. FZA I can write of $-D \sin \alpha - L \cos \alpha$ right are if I don't write C_D and write D and L is better so and the z is particularly down.

And what will happen $L \cos \alpha$ which is the opposite direction of z so minus $L \cos \alpha$ qualified $D \sin \alpha$ see one component and one component upward $D \sin \alpha$ again upward direction minus $D \sin \alpha$ right the second is $F_{ZA} = -q_\infty S [C_D \sin \alpha + C_L \cos \alpha]$ what are the alpha . alpha is the perturbed angle you not forgot this alpha is the perturbed angle of attack ok this is find what is our aim $\frac{\partial F_{ZA}}{\partial \alpha} = -q_\infty S [C_{L\alpha} + C_{D1}]$ and no infinity.

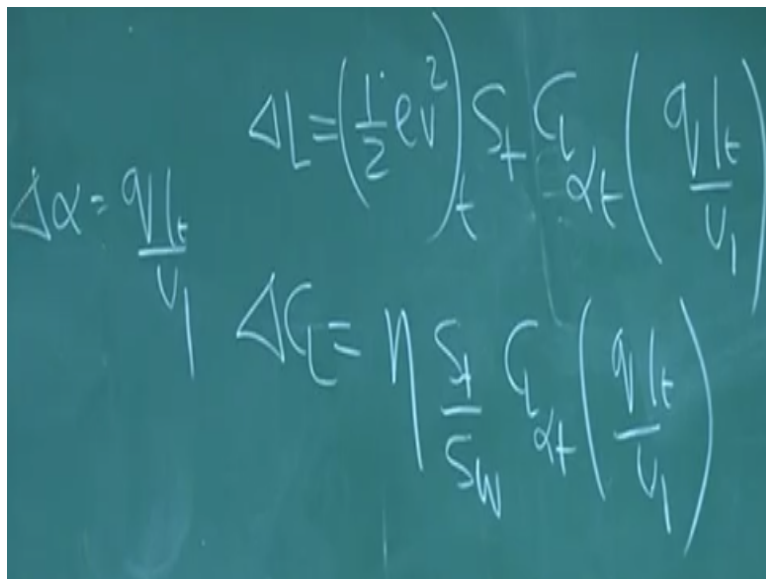
There is one and you except determined to derive this relationship this class 10 th problem you take it to derivative. One derivative is C_D and one derivative is $\sin \alpha$ like that and put at steady state as α steady state alpha is zero and you should get $\frac{\partial F_{ZA}}{\partial \alpha}$ as minus. $\frac{\partial F_{ZA}}{\partial \alpha} = -q_\infty S (C_{L\alpha} + C_{D1})$ correct yes ok any problem. You should not have any problem. You want to just put an effort simply class 10 and 11 you take derivative.

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And damping ratio for pure pitch longitudinal motion because this is very straight forward you know that the CorrectText equation is. $\frac{\partial F_{zA}}{\partial q}$ by $2u_1$ right. Let us understand what is this. What is q , q is the perturbed pitch rate right. Now think of this air plane. This is the tail, this is the wing and let's see somewhere is the cg is there is the q . vertical tail. Do you know that the q is the perturbed pitch rate.

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As this airplane goes for a q then there is the q into l_t relative airplane I put in the aero dynamic center. And see this is tail moment term I can write $\Delta \alpha$ is $q l_t$ by u_1 . And if you want to take moment then I will take l_t . if this is the $\Delta \alpha$ then what is the ΔL . ΔL will

be half rho u square half tail f tail cl alpha tail into delta alpha which is q lt by u1. So what is delta cl. You know that for delta we have to divide it by cl so this will be neta into st by sw cl alpha tail into q lt by u1.

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Handwritten mathematical derivations on a chalkboard:

- Top left: $L_{\delta e} = \frac{C_{\alpha} \cdot \eta \cdot S_{\alpha}}{S}$
- Top middle: $f_z = \frac{\partial F_{ZA}}{\partial u_1} \frac{u}{u_1} + \frac{\partial F_{ZA}}{\partial \alpha} \alpha + \frac{\partial F_{ZA}}{\partial q/c} \frac{q/c}{u_1} + \frac{\partial F_{ZA}}{\partial \dot{c}} \frac{\dot{c}}{u_1} + \frac{\partial F_{ZA}}{\partial e} \delta e$
- Middle left: $\Delta L = \left(\frac{1}{2} e v^2\right)_{\alpha} + \frac{C_{\alpha}}{\alpha} \left(\frac{q}{u_1}\right)$
- Middle right: $\Delta L = \eta \frac{S_{\alpha}}{S_w} \frac{C_{\alpha}}{\alpha} \left(\frac{q}{u_1}\right)$
- Bottom middle (boxed): $\frac{\partial F_{ZA}}{\partial \delta e} = -q S_{\alpha} \frac{C_{\alpha}}{\delta e}$
- Bottom right: $F_{ZA} = -\frac{1}{2} e v^2 \left(\frac{C_{\alpha}}{\delta e}\right)$

Now it is interesting to see that we will find out clq. You know what cl alpha is. Cl alpha is dcl by d alpha. Alpha is non-dimensional. We will now write clq dcl by dq c by 2u1 because is a dimensional quantity so qc by u1 is non-dimensional. So we define clq by dcl by dq c by du1 ok. No problem on that. So seen delta cl is this.

Do know that the f z function of u by u1 alpha under the qc by z u1 and acquire by alpha dot c you write by z v1 but del e the same do same understanding and it to the for you v1 but qc by zv1 is the common cell if you see the right from it convenience to see the max of the from q c by q1 dx by see the by delta e what is important this ca.

I get estimate the formulation evaluate as the first we you by one exactly z is I can write f z a minus cl half row u1+u what is this v1 is called that graph this is u1 the portal minus u total is v1+u figure the port is square but I know f z a minus cl half row v1 as 1+u by v1square f z a by v1 minus q alpha cl minus 1+u by u1 then second is minus that is last step has study stage what the begin in the perturbed minus q1 s cl then 2 that is zero minus q1 that is cl by v1 the final expression as simple as f z a by minus1 is 2cl1+clu that see how many what is q1 ?

Q1 is dynamic expansion c_{l1} is 2 by v_2 square what is c_{lu} ? minus focus on c_{lu} that is c_l by u by v_1 the will something that the c_l max point the goal with go write and left most and this of Q is cognitive then $c_l q$ as sure benefit greater than zero will proof. The down figure it past the pull the force in live direction but issue opposite f_z that so will write f_z of minus the row of square c_q of the q c by $2 v_1$ that is of the square in c_q with this part complete is $c_l q$ with c_q .

By that means $b f_z v_1$ that $f_z a$ by minus q_1 is $c_l q$ has simple as a the resort of the right equal to minus $q_1 s c_l q$ of the simple. I can write is this the tail and this is the elevator the delta is positive right. That will go force upward direction lift with the gain opposite is z direction write $f_z a$ minus half the expert $c_l \Delta e \Delta e$ see is figure of Δe minus sign because list in the opposite direction of what in the figure $z f_2 a$ nothing but $- q_1 s c_l \Delta e$. And you know very well how to calculate Δe on no direction of with c_l .

$\Delta e c_l q$ the control of this c_l alpha tail into tau yeta $s t$ by s reference is come on back to this. For this you have to know the f_z know what is expert the today you are finish this and this what is left is alpha dot derivative we will take separate class on alpha dot and we try to understand this.