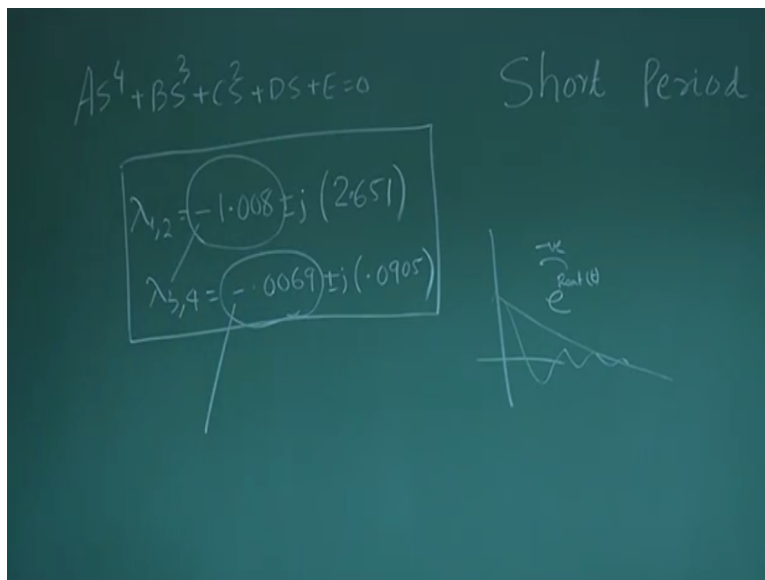


Aircraft Stability and Control
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Lecture-52
Short Period and Phugoid approximations

Good morning friends. We were try to understand that dynamic stability aspects of an aircraft if can see that when we will analyzing longitudinal mode and we put get the equations of the form as $as^4 + bs^3 + cs^2 + ds + e = 0$. And you know a, b, c, d, e all this can be computed using atomic derivative and national property extra.

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And when I solve this numerically we get suggestion for typical aircraft $\lambda_1, \lambda_2 = -1.008 + \text{minus } j 2.651$ as similarly $-0.00069 + \text{minus } j 0.0905$ what is important here it is note is that. These rules are complex conjugate right so it tells you oscillatory motion. Whether its oscillation = decay or not. What it tells us that is decided by the real part of the root. And you can see both appear the real part is negative. That is the oscillation will dump out we all know for the second order system.

Now with another different we could see that the minus one this is 0.0069 so which one will the decay faster. This will decay faster. So this excitation all most like the second order excitation this will decay faster because you know that for a second order system. If this decay like this,

this edible is governed by like this e to the power real part into t and the real part is negative the naturally this will decay faster as compare to this right.

So What will have seen for most of this type of aircraft you find solution of this equation will result in two pairs of complex conjugate this one lambda one and lambda two lambda three and lambda four the one prior the real part is highly largely negative larger than other roots that is the real part. And physically what we understand when the aircraft is disturbed with the primarily the two modes excited one is short period that when we disturb it immediately comes back.

And it will be short period mode you can understand there no much can the velocity u okay. However this is long period is the longer time and it is at the phugoid mode and it is accelerates like this and then downs the equilibrium. So we know do a short period approximation of with understanding this all of it in background and will do the short period approximation and let me write the equation first.

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Short Period Approximation

$$\begin{bmatrix} s - X_u & -X_\alpha & q \\ -Z_u & \{s(u - Z_\alpha) - Z_\alpha\} & -(Z_q + u)s \\ -M_u & -(M_\alpha s + M_{\alpha\dot{}}) & s - M_q s \end{bmatrix} \begin{bmatrix} \frac{u(s)}{\delta e(s)} \\ \frac{\alpha(s)}{\delta e(s)} \\ \frac{\theta(s)}{\delta e(s)} \end{bmatrix} = \begin{bmatrix} X_{\delta e} \\ Z_{\delta e} \\ M_{\delta e} \end{bmatrix}$$

This is our standard equation s minus x u minus x alpha g and the minus zu then s and then u l g minus z alpha dot minus z alpha then minus z q + u l into s and minus m u minus m alpha dot s + m alpha then s square minuses mqs this of course into u of s alpha of s theta of s equal to x delta e and z delta e m delta e you write it like this theta e by delta e. We should note down that we are note writing q here.

We have here understanding q is equal θ dot for small perturbation. So q alpha is nothing but s theta of s that was absolutely done. So that is fine is the part of algebra now we are almost going towards applying short period approximation, and what is the short period of the approximation that during this disturbance or during excitation you remain constant there is no change in the u perturbation right.

Perturbation u will be 0. Because you could understand this is very short period that come the very short time it comes to equilibrium so that's not a bad approximation. So why to handle all those three by three matrices, since u and u matrix is not consult for us. So you neglect this to this term first this one here we neglect this.

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The image shows a chalkboard with the following handwritten content:

$$\begin{vmatrix} s(u_1 - z_\alpha) - z_\alpha & -(z_q + u_1)s \\ -(M_\alpha s + M_x) & (z - M_q s) \end{vmatrix}$$

Assume $z_\alpha = z_q = u_1 = 0$
 No thrust term is included

And then we get the equation from the determinant $s(1 - z \alpha \dot{\alpha} - z \alpha - z q + u_1 s - m \alpha \dot{\alpha} s + m \alpha + s^2 - m q s)$ okay this determinant matrix form get reduced to this and I am directly writing this determinant. Because I want to find the characteristic equations and I know the determinant = 0 is the characteristic equation right. If I write that, that I get equations then which will be very you will see that very handy for designer to design the airplane.

Before I go to that we give this is g means I update θ one equal to 0 which is fine if I am doing it in steady state. And also when I do it here when I assume $\dot{z} = z q$ and also θ one all other identical is 0 and please understand here. We have not incorporated the thrust term right so no thrust term is included because you know that if you understand this how to derive this I think it will establish no way handling the drag time okay.

So this whole structure is included please note down this. So when I write the determinant = 0 I get an equation.

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Characteristic Eq.
 $\begin{vmatrix} | & | \\ | & | \end{vmatrix} = 0$
 Det. $s u_1 \left\{ \begin{matrix} s^2 - \left(Mq + \frac{Zx}{u_1} + M\dot{\alpha} \right) & \left(\frac{Zx Mq}{u_1} - M\alpha \right) \\ \hline & \end{matrix} \right\} = 0$
 $s^2 - \left(Mq + \frac{Zx}{u_1} + M\dot{\alpha} \right) s + \left(\frac{Zx Mq}{u_1} - M\alpha \right) = 0$
 $s^2 + 2\zeta \omega_n s + \omega_n^2 = 0$

Now we are looking for the characteristic equations and that will be determinant of this = 0 and that will be give me the result something. Like this determinant is $s u_1 s^2 - m q + z$ alpha by $u_1 g + m$ alpha dot $s + z$ alpha $m q / u_1 g$ minus m alpha that will be equal to this is on this one is here and here and this equal to 0 right. This equal to 0 means this one is 0 or this one is 0 or both are 0 from this you will get $s = 0$ one this whole term = 0.

$s = 0$ long term this one is shout of the neutral stability because the airplane whether it goes strength goes like this and like that it is that this atomic concern this is same thing for it right. So we are not take this suggestion at all and we will use this equation and then I get final characteristic equation for this short period as $s^2 - m q + z$ alpha / $u_1 g + m$ alpha dot into $s + z$ alpha $m q / u_1 g$ minus m alpha = 0 as simple as that okay.

Could you see that when I put short period approximation we have got equations which is second order equation and it very much handy in handling this equation because you know find out damping ratios and natural frequency and that is only comparing it with this form which I already did.

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The image shows handwritten equations on a chalkboard. The first equation is $\omega_{n, SP} = \sqrt{\frac{Z_{\alpha} M_{\dot{q}}}{U_1} - M_{\alpha}}$. The second equation is $\zeta_{SP} = -\frac{M_{\dot{q}} + \frac{Z_{\alpha}}{U_1} + M_{\alpha}}{2 \omega_{n, SP}}$. Below these equations, the words "Short Period" are written and underlined.

So now if I compare it what do I get. If I compare I get omega n short period equal to root z alpha m q / u1g minus m alpha and zeta short period = minus mq + z alpha / u1g + m alpha dot / 2 omega n short period. So this is basically we are getting for the short period. So I repeat it again which airplane is fly if you there is an excitation from the external disturbances. The airplanes will have a tendency should excite primarily in the short period or phugoid mode.

What is short period disturbance and it is comes like this and it downs like equilibrium through conversion of potential kinetic energy that is long period this is only about short period which is this. What is the exceptional in short period mode and how you are simplifying the equations. We assume that the short period is you will not to going change. So that the three by three matrix is primarily two by two matrix neglecting those equations right.

And we have got natural frequency for short period and type z for short period mode okay. This is very important relationship short period mode we will see I learning of SAS when operating at

the initial relationship for developing the final solution. Now we come back to the phugoid approximation.

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Phugoid approximation

α : degree of freedom to be superfluous

$\alpha \rightarrow \text{Const}$

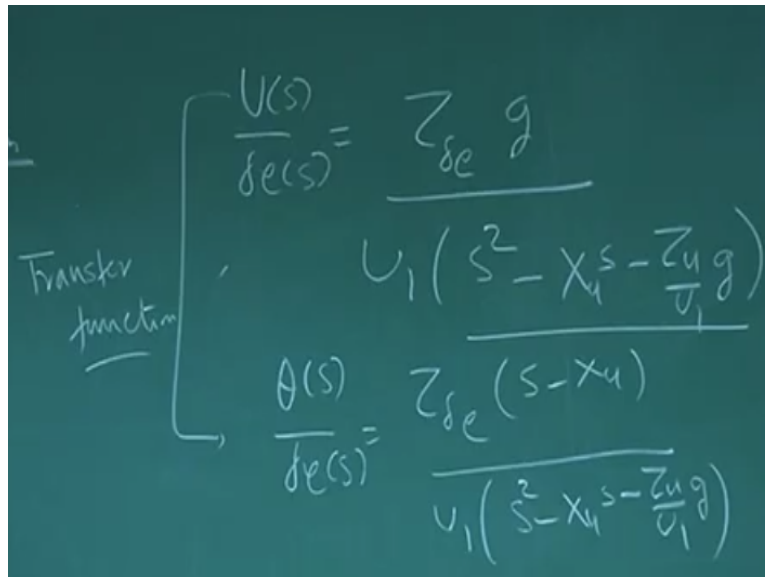
$$\begin{bmatrix} s - x_u & g \\ -z_u & -v_1 s \end{bmatrix} \begin{bmatrix} \frac{U(s)}{\delta e(s)} \\ \frac{\theta(s)}{\delta e(s)} \end{bmatrix} = \begin{bmatrix} X_{\delta e} \\ Z_{\delta e} \end{bmatrix}$$

As the Phugoid approximation is concerned which is not really very great approximation but how about it gives the good result. And Phugoid approximation is the alpha degree of freedom should be superfluous but many are superfluous that. The Phugoid mode approximation which is not good approximation but it is not that bad I also and it is not worse approximation and not a very good approximation.

It gives you something in the P phugoid approximation the angle of attack perturbation angular perturbation is angle of attack is neglected okay. In the short period u was neglected right. With that alpha remaining constant will be the approximation. If you do that we will get the equation for you that is important to note down this. We can easily find out which one will be omitted. u of s / delta e(s) as zeta of s / delta of s you see no alpha is here two by two matrix = x delta e and z delta e now the characteristics equation will becomes very simplified let us see in phugoid what are the additional thing we are going to get.

Please remember this point of the dynamic stability of next to trick to as different course together we will get lambda of course for dynamic stability that's the huge. But we are giving the some favor and that ready for next course don't get disturb because of so many equation and so many interruptions of coming try make the understanding and make yourself ready.

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Transfer function

$$\frac{U(s)}{\delta e(s)} = \frac{z \delta e g}{u_1 \left(s^2 - x_u s - \frac{z_u g}{u_1} \right)}$$

$$\frac{\theta(s)}{\delta e(s)} = \frac{z \delta e (s - x_u)}{u_1 \left(s^2 - x_u s - \frac{z_u g}{u_1} \right)}$$

If I do this then I find from this u of $s/\delta e(s) = z \delta e g / u_1 g$ of $s^2 - x_u s - z_u / u_1 g$ and the theta of $s/\delta e$ of $s = z \delta e \int s - x_u / u_1 g \int s^2 - x_u s - z_u / u$ what is u of δx and δa is a transfer function from the short period of you know that is αe and $\delta e \delta a$ was a transfer function it was a transfer function okay.

Now if I am to find the roots then what I have to do and ensure that in settlement to 0 characteristic equation.

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$$s^2 - X_u s - \frac{Z_u}{v_1} g = 0$$

$$s^2 + 2\zeta \omega_n s + \omega_n^2 = 0$$

$$\omega_n = \sqrt{\frac{-Z_u}{v_1} g}$$

$$2\zeta \omega_n = -X_u \quad \zeta_{\text{phugoid}} = \frac{-X_u}{2\omega_n}$$

If i to the 0 here that s square - x u s - zu / v1 g = 0 here you see the form S square + 2 delta w n s + wn2 = 0.

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$$\omega_{np} = \sqrt{\frac{-Z_u}{v_1} g}$$

$$= \sqrt{\frac{g}{v_1} \frac{q_1 s (C_{L\alpha} + 2C_{L1})}{m v_1}} \approx \sqrt{\frac{p g s}{m} C_{L1}}$$

$$q_1 = \frac{1}{2} \rho v_1^2 \quad C_{L1} = M_1 \frac{\partial C_L}{\partial \alpha} \rightarrow$$

The omega n is equal is to root of - zu / v1 into g, and two zeta omega as n = - x u that is all okay. That zeta phugoid = - x u / 2 omega np and this so Phugoid you know by now what is z and x u almost fresher's at it all now we will keep at up this and see that what happen let as 2 zeta omega n take and try the exact meaning of omega np = and root - zu / v1 g dot g right I for zu I got a expressions that = g / v1 g q1 int c one alpha + 2 cl1 / mv one okay which I can approximately to and a root of p g s / m int c l one what has been done.

To see here c then is not a c alpha this is a c_l okay. What is approximation here let us related as c_m the $c_l n = m l \Delta c_l / \Delta n = 0$ that I am typically talking about so up it here up mark point 6 what is $q = \frac{1}{2} \rho v_1^2$. q_l is use this the moment are use this smart enough this get this expression okay. This is the expression how do I get from here to here your smart of $q_l = \frac{1}{2} \rho v_1^2$ square is here the $u_l g$ square and $u_l g$ square is cancel the $c v_1$ and v_1 is cancel.

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The image shows a chalkboard with the following handwritten equations and steps:

- Top left: $\omega_{np} = \sqrt{\frac{\rho g s}{m} c_{l1}}$
- Middle: $c_{l1} = \frac{m g}{\frac{1}{2} \rho v_1^2}$
- Bottom left (boxed): $\omega_{np} = \frac{g \sqrt{2}}{v_1}$ with a checkmark.
- Bottom right (boxed): $\frac{\rho g s}{m} \cdot \frac{m g}{\frac{1}{2} \rho v_1^2}$

Arrows indicate the substitution of c_{l1} from the middle equation into the top-left equation, leading to the boxed result on the bottom right.

And $\omega_{np} = \text{root of } \rho g s / m c_{l1}$ what is the c_{l1} the c_{l1} is nothing but $m g / \frac{1}{2} \rho v_1^2$ square. To this expression ω_{np} phugoid I s equal t as $g \sqrt{2} / v_1$ will you see this is c_{l1} here under root of $\rho g s / m$ and $m g / \frac{1}{2} \rho v_1^2$ square. Will you see that $1/2$ was here ρ and ρ will be cancel so what is the best edge here? For a phugoid mode you see that natural frequency in phugoid mode version provided to the forward velocity u_1 so more $u_1 g$ is less okay right.

It is very very important of the version rather you could see zeta phugoid we watch .

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We watch the zeta phugoid is got as $-x_u/z \omega_n p = q_1 (c_{Du} + 2 c_{D1}) / 2 m u_1 \omega_n p$ what have we done we substituted the equation for x_u and what are the x_u what is expression of the x_u is $-q_1 s (c_{Du} + 2 c_{D1}) / m u_1$ nothing the big deal will be done the q_1 is derived as right look something big at as simple $\omega_n = g / v_1 \sqrt{2}$ understand one thing for beginning we understanding.

We assuming no transfer is right is all like a fall of case and I have been always telling a thrust and drag was similar nature. What is doing here similar fiction expend doing as so now ω_n is substitute here and also write $mg = q_1 s C_{L1}$ and $m = q_1 s C_{L1} / g$ we substitute this the ω_n is here the α is here this is expression I get.

The zeta p is a very important in this lesson $c_{Du} + 2 c_{D1} / 2 c_{L1} \sqrt{2}$ and if c_{Du} will be 0 this will be remember c_d versus mach number 0.6/0.7 and goes like this and $c_{Du} = m_1 \delta c_d / \delta m$ but this point is will be a 0 so assuming I can neglected is zeta $p = c_{D1} / c_{L1} \sqrt{2}$ and the $q_1 c_{L1} / \sqrt{2}$ okay. These rows are canceled in this expression.

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$$\zeta_p = \frac{1}{\frac{c_l}{c_D} \sqrt{2}}$$

if $\frac{c_l}{c_D} \uparrow$ Phugoid mode

What is important of the is not a good approximation in let us do that $1 / c_l / c_D \sqrt{2}$ it tell you if c_l and c_D is large try to see that care full by doing that damping ratio for phugoid mode became weaker and weaker that is very important right okay the slide is traction time to phugoid mode and this is very very important okay. so we have finish long tutorial part is concerned it what will doing immediately go for stability augmentation system and then give only make lecture.

Lateral relational case which and send of the if for I am sure by now we will get tired and then wined it up please try derive the explanation. okay thank you very much.