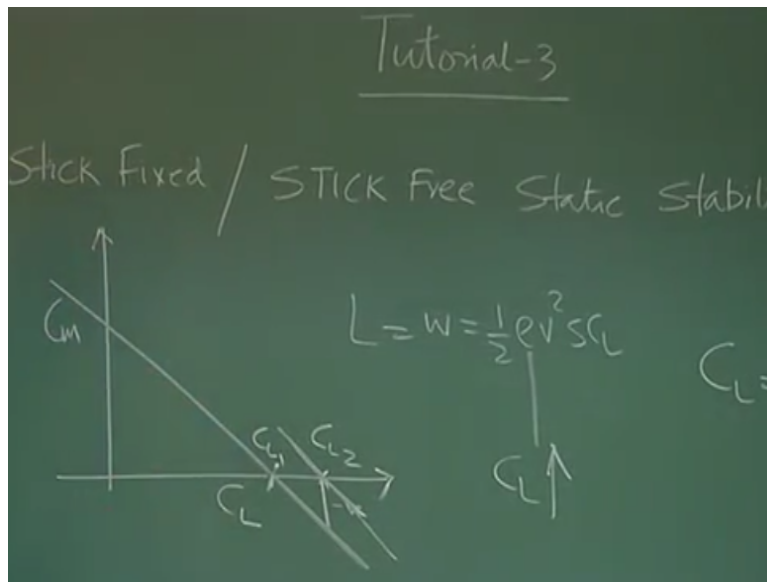


Aircraft Stability and Control
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Lecture – 58
Tutorial – 3

Friends, let us come to tutorial 3.

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In this tutorial as we discuss we will be revisiting the few concept the final points. One of the observation which I have after seeing the fore arm questions that is on stick fixed and stick free stability stick free static stability. Lot of confusion is there in fact lot of confusion was there when I was start this concept as the tech level so nothing surprising. So I will try to revisit this so that this confusion is removed for all time ok.

Please understand one thing, we are very clear about one point that this is c_m versus c_l and I am flying at c_l and I have to fly another $c_l 2$ let say. Then, if have to go to this $c_l 2$. The airplane because this is statically stable it will generate the negative moment. Why? Because if I have to increase the c_l from here, $c_l 1$ to $c_l 2$ that means I am keeping the speed same what does it mean.

It means have to change the angle of attack ok right. But when I try to also think this way at this point lift is equal to weight at this point so I was lift equal to weight I am not changing the altitude that means, see lift is equal to weight $\frac{1}{2} \rho v^2 S C_L$ if I am not changing the altitude that is ρ remaining same.

If I have to fly at the higher C_L if C_L is higher that means to maintain lift equal to weight I need to fly at the lower speed then only it is possible right. If I am balancing lift is equal to weight at C_{L2} where C_{L2} is more than C_{L1} that means the velocity the speed here less than velocity here. There is no confusion and then next question comes how do you increase C_L and do you know C_L is nothing but C_{L0} not plus $C_L \alpha$ into α that means if you want to change C_L and want to increase angle of attack.

The moment I try to change C_L from C_{L1} to C_{L2} this C_m versus C_L graph tells you that there will negative moment briskly generated because they air craft is statically stable but you want to fly at this C_L so you have to deflect the elevator such that this negative moment is neutralized right.

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$(\delta e)_{reqd}$ to trim an airplane at $C_{L_{trim}}$
 $0 = C_m = C_{m_0} + C_{m_\alpha} \alpha_{trim} + C_{m_{\delta e}} \delta e_{reqd}$
 $C_L = C_{L_0} + C_{L_\alpha} \alpha_{trim} + C_{L_{\delta e}} \delta e_{reqd}$

We under that understanding we try to address the question what is the delta e required to trim an airplane at C_L trim. What was the approach? Approach was C_m we write C_m equal to C_{m0} not plus $C_{m\alpha}$ into α plus $C_{m\delta e}$ into δe and we know C_L equal to C_{L0} not plus $C_{L\alpha}$ into α plus $C_{L\delta e}$ into δe in the class we have taken the C_{L0} not is zero which is

not really zero. But for simply sake we have taken it for zero you can add those expressions but what you have realized.

If I want to fly at particular c_l and that to be a trim point that means at that point this c_m is equal to zero so what we did we put c_m equal to zero and this α we said this is α_{trim} and δe is $\delta e_{required}$ and here α_{trim} and $\delta e_{required}$ right.

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The image shows a chalkboard with the following handwritten text and equations:

- Top line: K Fixed / STICK FREE Static Stability
- Equation 1: $\xi_e = \xi_{e_0} + \frac{d\xi_e}{dc_{l_{trim}}} \cdot c_{l_{trim}} - \frac{d\xi_e}{d\alpha} \cdot \alpha$
- Equation 2: $\frac{d\xi_e}{dc_{l_{trim}}} = -\frac{\frac{\partial c_m}{\partial \alpha}}{C_{m_{\delta e}}}$
- Equation 3: $\frac{\partial c_m}{\partial \alpha} = -\left(\frac{N_0}{\bar{x}_g}\right)$
- Equation 4: $C_L = C_{L_0} + C_{L_\alpha} \alpha$
- Bottom left: $(\delta e)_{reqd}$
- Bottom right: Stick Fixed

Now what we did is we solve this equation and we derive an expressions δe equal to δe_{not} plus $d \delta e$ by $d c_l$ trim by c_l trim right and you also know approximately $d \delta e$ by $d c_l$ trim is equal to minus $d c_m$ by $d c_l$ by $c_m \delta e$. So with this understanding it is very clear if I want to fly at particular c_l if I know its stability characteristic if I know its neutral point and c_g location why I am saying that, because after all $d c_m$ by $d c_l$ is approximately minus of neutral point minus $x c_g$ and this neutral point we talk about stick fixed.

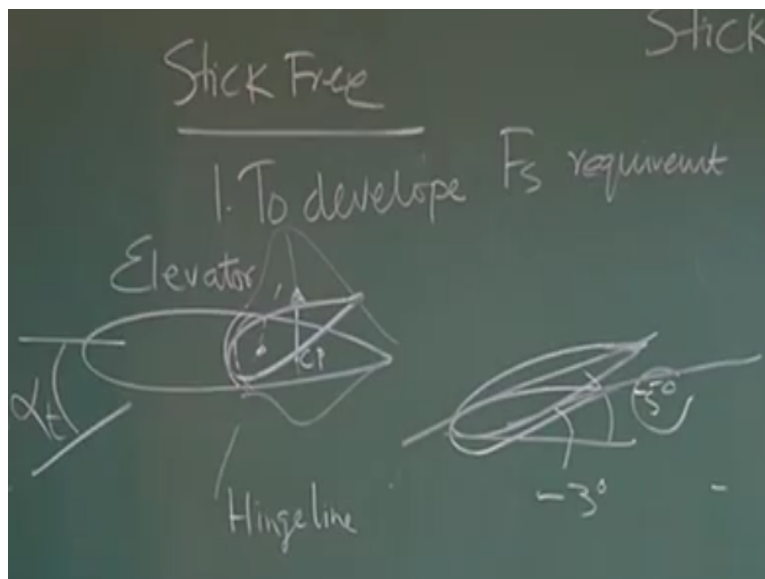
So what is the message, message is if we want to fly at the particular c_l trim once you this values you know what is the δe required and here we use the concept of stick fixed neutral point right. Why is the stick fixed neutral point because we are assuming that although this elevator at any angle of attack because it is hinged here it can start floating we are not allowing that. We are saying that we will not allowing it to float so fixed.

So this tells you this expression tells you δe required is minus 5 degree. We will take this elevator minus 5 degree which is this and that's all. And the stick is locked the elevator cannot move up and down and when I am talking about stick fixed this also means at when I am starting the refresh from where I am going to measure the elevator in that it is assumed that given at this condition elevator is not allowed to float elevator is here only from here.

So what is the final message if I have to flight at particular. Trim whatever δe required as I said minus 5 degree so you have to from this reference we will push the elevator here and lock it. So here also stick fixed in the sense we are not giving it permission to float. So whenever we are flying in the air craft how much elevator required to trim an air craft for the given c_l is decided by this neutral point stick fixed that is no floating of the elevator allowed.

So that is the number right. But why there is need for the stick free stability. Please understand the stick free stability we define for simple reason that we wanted to model. How much stick force pilot will apply to get the elevator that's the minus 5 degree for this case.

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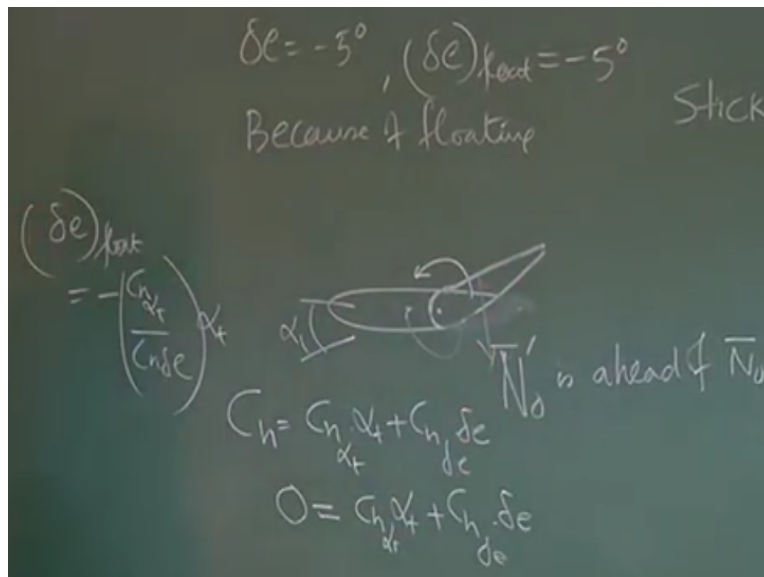
So for stick free concept was used for one is to develop the stick force requirement to deflect it to decide angle but how much angle that is always decided by the stick fixed case ok. How much force is required in that analysis we will be using stick free concept this should be very clear ok.

Now let us see what happens if we recall this is the elevator and this we write elevator and you know for the given alpha tail because there will be pressure distribution above the elevator and mostly the center pressure at the whole distribution over and over and below of the elevator will result in the center pressure wing behind the hinge line this is the hinge line normal it is like that.

So what is that at alpha t if we leave it free if we leave it not fixed then this will give the moment and by its own nature of the hinge moment characteristics it will float to equilibrium some angle right and that will depend upon alpha t for define alpha t will go on changing. So, let us say if I have to take it to minus 5 degree let us say by inherit nature it will automatically go to 3 degrees minus 3 degrees and basically pilot has to put the effort to take it to another 2 degrees that is above it require for 5 degrees and who decided the 5 degree through stick fixed neutral point say minus 5 degrees.

Now because of floating tendency it has one and half two let us say minus 3 degrees so how much effort pilot should put effort to take the aircraft to this but there what happens the moment it comes here again it can have a floating tendency so the pilot has to keep on holding the elevator in normal case right. So that is why we put trim tab extra. The point here is please understood when we talking about stick free concept.

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We are assuming that at the given α_t the elevator has already floated like this and that why $c_{l\alpha}$ of the tail reduces and that why neutral point stick free is ahead of neutral point stick fixed because it floats at the particular equilibrium so the $c_{l\alpha}$ tail is reduced ok. That is why neutral point stick free is ahead of neutral point stick fixed and this condition is taken as first equilibrium point from here we take to the next one.

For example let us see suppose δ_e required is minus 5 degree as given by this relationship where n not stick fixed is used and that is only to be used right. But we have seen suppose because of floating and if I recall what is floating and is $c_{l\alpha}$ equal to $c_h \alpha_t$ into α_t plus $c_h \delta_e$ into δ_e remember $c_h \alpha_t$ means if there is α_t tail there will be nose down movement because of α_t same time they will restoring moment because of $c_h \delta_e$.

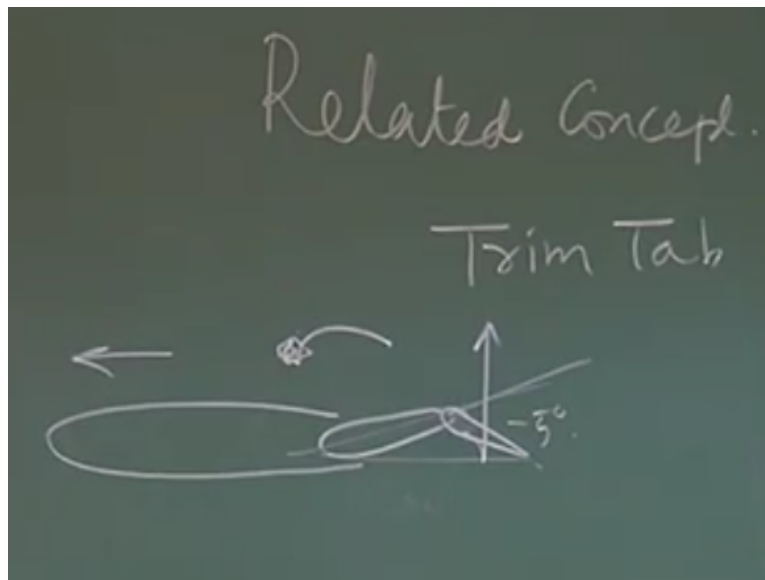
So as it goes up δ_e so it comes down and δ_e will restore it. So there will be equilibrium at equilibrium the contribution will cancel each other so c_h will become zero. So c_h zero that will be $c_h \alpha_t$ into α_t plus $c_h \delta_e$ into δ_e or δ_e float required to minus $c_h \alpha_t$ by $c_h \delta_e$ into α_t this we know.

So why I am talking about floating tendency? Suppose you have designed $c_h \alpha_t$ there $c_h \delta_t$ here such a way that because of floating this δ_e float at that α_t also becomes minus 5 degree. I repeat this question suppose I want δ_e minus 5 degree to trim the airplane at given c_l trim and we are clear that this should be evaluated by stick fixed. What we found we allow it to float by itself it floats up to minus 5 degree.

So naturally if this happens for the particular α_t pilot need not apply any force it will automatically go to minus 5 degree we will get the trimmed at whatever trim is required right. So the understanding is how much c_l trim is required is decided by stick fixed neutral point. That is when we are analyzing neutral point we have not allowed the elevator to float so it is there fixed right. So that $c_{l\alpha}$ of the tail remains $c_{l\alpha}$ tail without any deflection of elevator ok at the tail. This distinction has to be very clear.

And also you know stick free case is valid realistic when we are talking about reversible control that is if I move the elevator the stick also move, if I move the stick elevator also move. But from modern aircraft reversibility is not there that is irreversible for that this stick free concept loses its significance as well as finding the stick force is concerned right. So this should be very very clear.

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So related concept to stick free is trim tab if you now realize that this is the tail so this is the elevator and put it trim tab like this, what happens suppose you do not put the trim tab here if I have to fly at minus 5 degree elevator. Please understand where the elevator minus 5 degree is required. So what the pilot will do.

Pilot will try to pull the stick in a sense it will try to reduce the speed and increase the angle of attack so C_L is more and maintain lift is equal to weight. But imagine the pilot has to keep on holding the stick but at the moment he relieves because of reversible the elevator will go down or it may not be able to maintain this positions so pilot will get tired and how this maintain minus 5 degree major contribution is the force applied on the stick so in the stick there is the moment.

What is done to give relieve to the pilot we put it trim tab the trim tab should deflect like this and as you are moving like this you could see that trim tab will generate the force in this direction and that will give the moment like this which will keep on holding the elevator at the particular

decide angle. Now once the pilot sets the trim tab the pilot can leave the stick what we say we say that hands off flying. That is the beauty of trim tab.

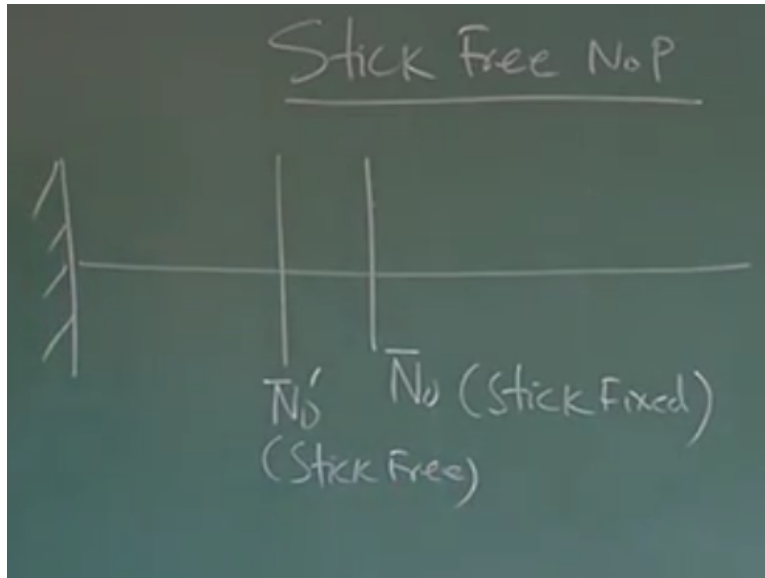
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The image shows a chalkboard with three equations written in white chalk. The first equation is $C_h = C_{h\alpha_t} \alpha_t + C_{h\delta_e} \delta_e + C_{h\delta_t} \delta_t$, with an arrow pointing to δ_t labeled 'Tab'. The second equation is $0 = C_{h\alpha_t} \alpha_t + C_{h\delta_e} \delta_e + C_{h\delta_t} \delta_t$. The third equation is $\delta_t = - \frac{C_{h\alpha_t} \alpha_t + C_{h\delta_e} \delta_e}{C_{h\delta_t}}$.

Mathematically what we have shown C_h is equal to $C_{h\alpha_t} \alpha_t$ plus $C_{h\delta_e} \delta_e$ plus $C_{h\delta_t} \delta_t$ where this is the deflection trim tab deflection right. So when its hands off this is equal to zero equal to $C_{h\alpha_t} \alpha_t$ plus $C_{h\delta_e} \delta_e$ plus $C_{h\delta_t} \delta_t$. So I can easily find out what is the δ_t required that will be minus $C_{h\alpha_t} \alpha_t$ plus $C_{h\delta_e} \delta_e$ divided by $C_{h\delta_t}$.

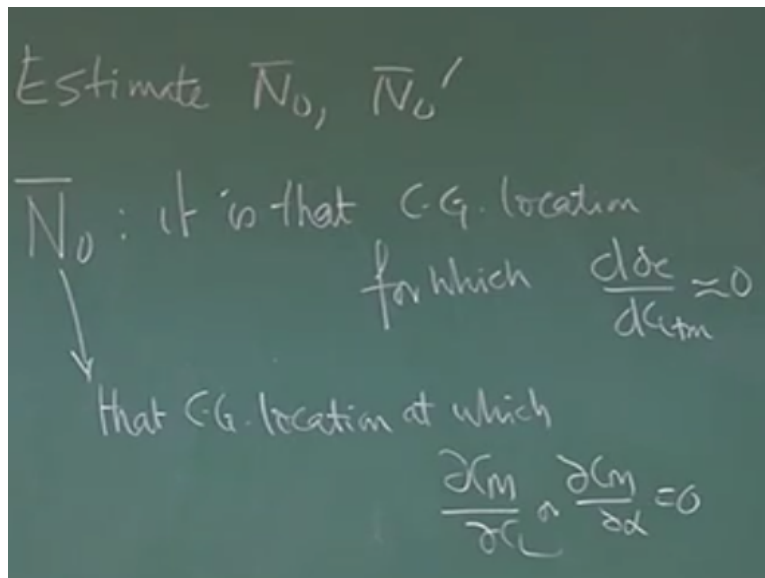
So if it is derived properly for even α_t given δ_e which I need to keep it I can easily find out how much trim tab deflection is required so I can easily calibrate this deflection is done this understanding ok. Final correction will done by the pilot through the lever. This is very important as well as flying quality of the airplane is concerned right.

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When we are talking about stick free neutral point we realize that if this is the reference line and measuring from here and this is n not bar is stick fixed then n not bar prime stick free will be ahead of stick fixed neutral point right. And if you also recall when we are talking about how to estimate neutral point stick fixed neutral points stick free in that problem formulation.

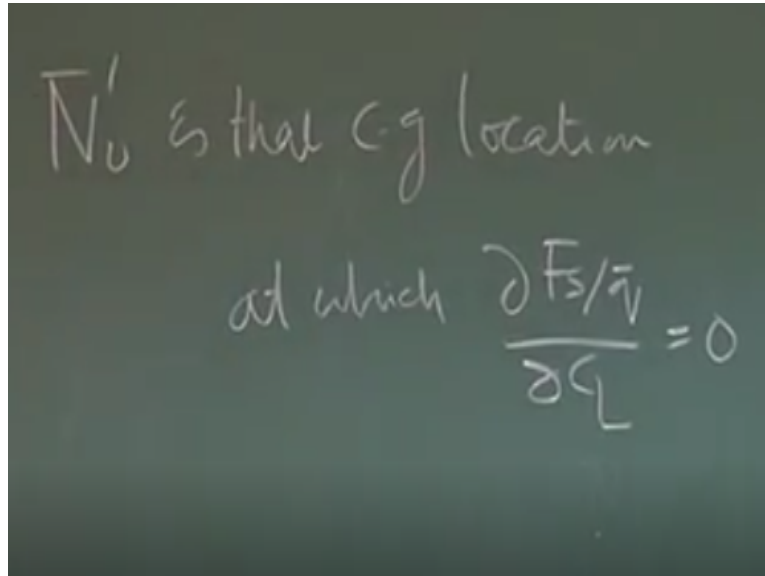
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What we said for n not it is that c g location for which effectively $d \delta e$ by $d c l_{trim}$ is equal to zero little bit approximation although you know neutral point stick fixed with that c g location exact definition is it is that c g location at which $d c m$ by $d c l$ or $d c m$ by $d \alpha$ is equal to

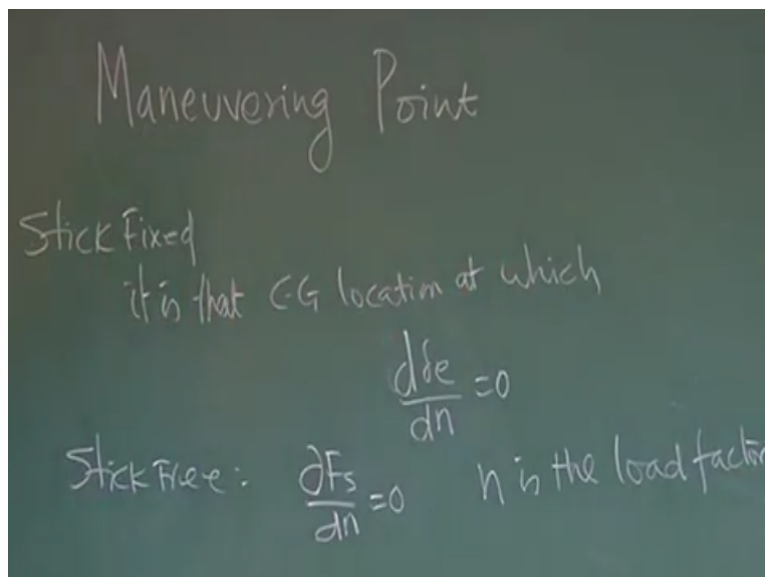
zero it is neutral stability but why did not you find stick free neutral point what did you say through the formulation.

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It is said that n not prime is that C.G. location at which $d F_s$ stick force by dynamic pressure by $d C_L$ is equal to zero so this distinction should be there in your mind.

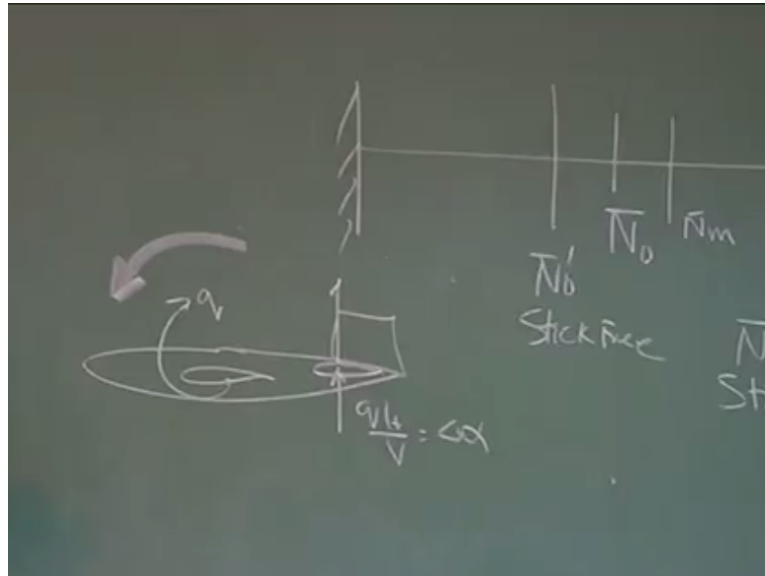
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Similar concept is used when we are talking about maneuvering point. How did you find maneuvering point for stick fixed? It is that C.G. location at which $d \delta e$ by $d n$ is equal to zero

and for stick free we define maneuvering point stick free $d f s$ by $d n$ equal to zero but f is the stick force n is the load factor ok.

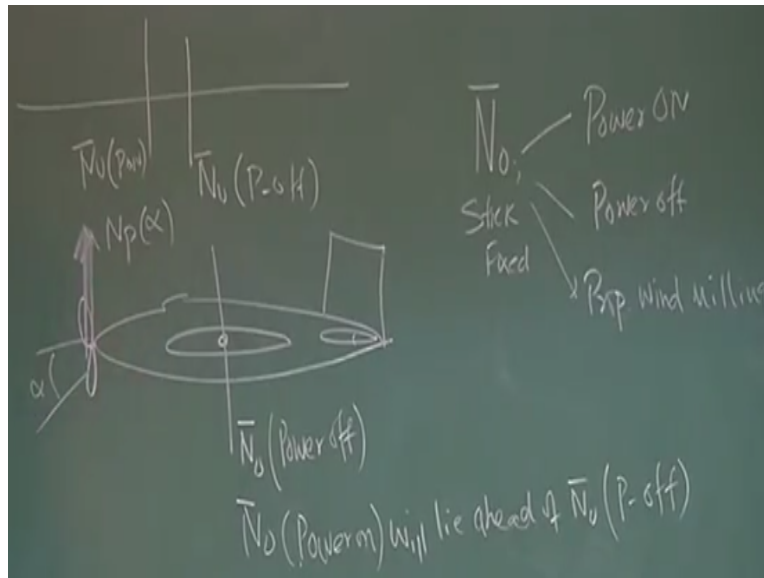
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And we have also seen if this is your n not stick fixed and this is n not prime stick free then n m stick fixed maneuvering point will be if I am measuring from here it will be some where here n m stick fixed maneuvering point because we have seen as airplane goes for the maneuver this is the q and there is the $q l t$ by v this much of angle of attack roughly get induced and gives the force here and that gives the nose down movement which try to restore or stabilizing tendency strictly dumping in nature.

So in our side we says that the aircraft tends to have more stability during maneuver and that is why n m stick fixed maneuvering point is behind stick fixed neutral point ok. Then there was a question that if.

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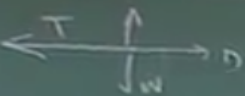


Not stick fixed whether I should take power on and take power off or propeller wind milling this questions where there right. Physically understand you know this is the airplane suppose you estimate neutral point stick fixed and let say this end point is some where here this is the end point when you compute n not bar let us say that we have not taken the contribution of engine ok right. That is this and we will say that power off typically glide without an engine.

Now suppose the engine is kept somewhere here I see engine piston lever engine properly I will say. The movement of propeller is here ahead of c g we know that angle of attack of an alpha will generate a normal force here at the function of alpha and that will make the aircraft lower stable this stabilizing in nature so n not power on will lie ahead of n not power off clear that is if it is n not bar power off then n not power off will be ahead of n not power on because this is more stable case for the nose mountain engine.

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Cruising.



$$\delta e = \delta e_0 + \frac{d\delta e}{dC_L} C_L$$

$$\frac{d\delta e}{dC_L} = \frac{-SM}{C_{M\delta e}} = \frac{(\bar{N}_0 - \bar{x}_c g)}{C_{M\delta e}}$$

Now let us see suppose you are cruising that's why you are cruising, for your cruising that means you have a thrust this is drag this is lift this is the weight this is the nose mountain engine configuration now if I have to calculate delta e d delta e by d c l is minus static margin by c m delta e which is minus n not bar minus x c g bar by c m delta e.

So if it is cruising that time this thrust is on I should you power on n not right. But if it is coming for the landing approaching for landing then it what happens theoretically this engine should be short although the engine is on the propeller is not rotating however you will see that it comes down there because of wind mill effect propeller will rotating and generate little bit of thrust although you will find competitive gives 20 percent thrust but what you say wind mill theoretically because of the wind the propeller is rotating and generating some margin of thrust.

So naturally this case I should use how much delta e is required for landing and all I must use n not corresponding to wind milling I should not use n not corresponding to power on isn't it and if the engine is off if wind milling is not there then I need to use n not power off for calculation of delta e required so that distinction should be there in your mind ok. Thank you.