

Introduction to Finite Volume Methods-II
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Lecture – 35
Fluid Flow Computation: Incompressible Flows-V

So, welcome back to the lecture series of finite volume and we will continue our discussion on the discrete momentum equation. And what we are doing that, we have looked at the staggered arrangement in the previous lecture. And then, we have discussed what is the problem with the staggered arrangement and why the collocated arrangement is a one of the preferred method in a finite volume approach.

Now, while doing the collocated arrangement, then we can actually modify the equation system and then you can get a pseudo momentum equation which will look exactly like an staggered arrangement. So, that allows you to avoid all these checker boarding problem that you come across in non collocated system. So, this is where we stopped in the last class and now we will continue from there.

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Fluid Flow problems: incompressible

$\int_{V_c} \nabla p \, dv = (\nabla p)_c V_c \Rightarrow \int_{\partial V_c} p \, ds = \sum_{f \in \text{func}(c)} p_f S_f$
 $\int_{V_c} f_b \, dv = (f_b)_c V_c$

Discretized mom. eq.:
 $a_c^v V_c + \sum_{F \in \text{NB}(c)} a_F^v V_F = b_c^v$

Time integration: 1st order Euler scheme
 Convection: HR scheme with DC
 Diffusion: implicit + explicit

$a_c^v = \text{Flux } C_c + \sum_{f \in \text{func}(c)} (\text{Flux } C_f)$
 $a_F^v = \text{Flux } F_f$
 $b_c^v = -\text{Flux } V_c - \sum_{f \in \text{func}(c)} \text{Flux } V_f + \sum_{f \in \text{NB}(c)} M_f (\nabla v)_f \cdot S_f - (\nabla p)_c V_c$

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So, if you recall, this is the discretized equation for the velocity system or the pseudo momentum equation and here the fluxes are like this. This is where we stopped. And, all the other term like time integration, convection term and the diffusion term can be

obtained which we have done earlier and then the coefficients would be calculated like this.

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Fluid Flow problems: incompressible


$$\text{Flux } G_f = \underbrace{\|m_f, 0\|}_{\text{Conv.}} + \underbrace{M_f \frac{E_f}{dCF}}_{\text{Diff.}}$$

$$\text{Flux } F_f = - \underbrace{\| -m_f, 0 \|}_{\text{Conv.}} - \underbrace{M_f \frac{E_f}{dCF}}_{\text{Diff.}}$$

$$\text{Flux } V_f = -M_f (\nabla V)_f \cdot T_f + m_f (V_f^{\text{HR}} - V_f^{\text{U}})$$

$$\text{Flux } C_c = \frac{p_c V_c}{\Delta t}$$

$$\text{Flux } V_c = - \frac{p_c^o V_c}{\Delta t} V_c^o - (f_o)_c V_c$$

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Now, in this particular system, these coefficients depend on velocity and pressure fields and there is a nonlinearity associated with that. So, the nonlinearities are handled essentially by your iterative solvers. And now, change in the value of the coefficients which can lead to a change in your flow field.

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Fluid Flow problems: incompressible

Under-relaxation (λ)
Patakar's implicit relaxation factor

$$\frac{a_c^v}{\lambda} V_c + \sum_{F \text{ around } c} a_F^v V_F = b_c^v + \frac{(1-\lambda)}{\lambda} a_c^v V_c^{(n)}$$


$$a_c^v \leftarrow \frac{a_c^v}{\lambda}, \quad b_c^v \leftarrow b_c^v + \frac{(1-\lambda)}{\lambda} a_c^v V_c^{(n)}$$

$$a_c^v V_c + \sum_{F \text{ around } c} a_F^v V_F = b_c^v$$

← under-relaxed non. eqn.

$$b_c^v = -V_c (\sigma p)_c + \hat{b}_c^v$$

$$V_c + \sum_{F \text{ around } c} \frac{a_F^v}{a_c^v} V_F = -\frac{V_c}{a_c^v} (\sigma p)_c + \frac{\hat{b}_c^v}{a_c^v}$$

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So, that effects the convergence and that is why, we need to do some sort of an under relaxation. So, since the system appears to be stiff, so use some sort of a under relaxation factor and this is adopting the Patankar implicit relaxation factor. So, this is Patankar's implicit relaxation factor. So, by invoking that, one can write that system of equation like $a_c v$ by $\lambda b_c v$ plus F which is summation over cell and $a_c v$ plus F equals to $b_c v$ plus $1 - \lambda$ times v divided by λ times $a_c v$ and $V_c n$.

So, now you can redefine your $a_c v$ which is essentially $a_c v$ divided by λ and $b_c v$ it is redefined as $b_c v$ plus $1 - \lambda$ times v by λ , $a_c v$ $V_c n$. Now, the under relaxed momentum equation, one can write like $a_c v$ plus F equals to $b_c v$. So, this is what you write as under relaxation or under relaxed momentum equation.

Now, for the derivation of the collocated pressure correction term, the pressure gradient is taken out from the $b_c v$ or the source term and can be explicitly written as $b_c v$ equals to $-V_c \Delta p_c$ plus $b_c v$. And now you substitute this in the this equation, you get V_c plus summation of F over NB_c a F V by $a_c v$ V F V by $a_c v$ V v f minus v c divided by $a_c v$ Δp_c plus V divided by $a_c v$.

So, what are the coefficients which are associated with this particular arrangement?

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Fluid Flow problems: incompressible

$$H_c[v] = \sum_{f \in \text{NB}(c)} \frac{a_f}{a_c} v_f \quad ; \quad B_c^v = \frac{\hat{b}_c^v}{a_c^v}, \quad D_c^v = \frac{V_c}{a_c^v}$$

rewrite:

$$V_c + H_c[v] = -D_c^v (\nabla p)_c + B_c^v$$

Pressure Correction (collocated) $v^{(c)}, \dot{m}^{(c)}, p^{(c)}$

$$V_c + H_c[v^*] = -D_c^v (\nabla p^{(c)})_c + B_c^v$$

Cont. $\sum_{f \in \text{NB}(c)} \dot{m}_f' = -\sum_{f \in \text{NB}(c)} \dot{m}_f^* \quad , \quad \dot{m}_f' = \rho_f V_f^* S_f$

Rho-Chen formulation

$$v_f^* = \bar{v}_f^* - D_f^v (\nabla p_f^{(c)} - \nabla p_f^{(n)})$$

$$\begin{cases} v = v^* + v' \\ p = p^{(c)} + p' \\ \dot{m} = \dot{m}^* + \dot{m}' \end{cases}$$

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So, we can define the following vector operations which is $H_c V$ equals to summation of this V by $a_c V F$ and here $B_c v$ equals to $b_{hat} p$ by $a_c v$ and $D_c v$ equals to V_c divided by $a_c v$. Now, the equation previous equation this one, you can reformulate as or rewrite in a vector notation like V_c plus $H_c v$ equals to minus $D_c v \Delta p_c$ plus $B_c v$. So, this is how you can write and this should be very useful later on when we will do the discussion of the other terms.

Now, one has to find out the pressure correction term. So, the pressure correction in collocated arrangement, so how do we find out that? Now, you can use our previous iteration values like $v_n m \cdot n p n$. So, these are the previous iteration values that we can use and this vector form of the momentum equation if we put this things and the intermediate velocity field which we will be calculated as V_c^* plus $H_c v^*$ equals to minus $D_c v \Delta p_n c$ plus $B_c v$.

Now, the final solution should satisfy the exact solution. Now, now the difference between these two equation is going to give us the correction equation. And now, when you look at the velocity field, they must satisfy the conservative equation or the continuity equation and then if there is no mass flux from there, we get the pressure correction equation.

Now, if you say the correction in a standard form which we have been using v equals to v^* plus v' , p equals to p_n plus p' , m equals to m^* plus $m \cdot \text{prime}$, so all with the guess value and the corrections which should satisfy the conservations equation. Now, substituting this into the equation, will get the conservation equation for the. So, we will use these things first in the continuity equation. So, the continuity equation essentially give us back that all the faces $m \cdot \text{prime} f$ equals to minus faces where $m \cdot f^*$ with $m \cdot f^*$ equals to $\rho f V^* f \cdot S f$.

Now, the face velocity is computed using the Rhie Chow formulation. So, once we use this Rhie Chow formulation, you get V_f^* equals to V_f^* average minus $D_f v \Delta p_f n$ minus $\Delta p_f n$ average. Now, in the computed mass flow rate field is conservative, the right hand side of this equation should this continuity conservation equation should go to 0; from this side should go to 0. Now, if you have a incorrect velocity field, then there will be a source term and from there, the correction has to be

imposed. Now, the mass flow rate corrections can be written in terms of velocity corrections and which one can derived from this vector equation.

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Fluid Flow problems: incompressible

$$v'_c + H_c[v'] = -D'_c[\nabla p']_c \Rightarrow \text{element } c'$$

$$v'_F + H_F[v'] = -D'_F[\nabla p']_F \Rightarrow \text{element } F'$$

$$\dot{m}'_f = \rho_f v'_f \cdot S_f \quad ; \quad v'_f = \bar{v}'_f - D'_f(\nabla p'_f - \nabla p'_f)$$

$$\sum_{\text{faces}(c)} (\rho_f \bar{v}'_f \cdot S_f) + \sum_{\text{faces}(c)} (\rho_f D'_f(\nabla p'_f) \cdot S_f) - \sum_{\text{faces}(c)} (\rho_f D'_f(\nabla p'_f) \cdot S_f) = - \sum_{\text{faces}(c)} \dot{m}'_f$$

neighboring vel. corrections

$$\bar{v}'_f + H_f[v'] = -D'_f[\nabla p']_f \Rightarrow \bar{v}'_f + D'_f(\nabla p')_f = -H_f[v']$$

$$\sum_{\text{faces}(c)} (\rho_f D'_f(\nabla p')_f \cdot S_f) = - \sum_{\text{faces}(c)} \dot{m}'_f + \sum_{\text{faces}(c)} (\rho_f H_f[v'] \cdot S_f)$$

So, the corrections equation for the velocity would become V_c prime plus H_c v prime minus D_c v delta p prime c. So, that is the correction for the velocity field. So, this is for element C.

Now, the neighboring element F, the similar equation will be there which is H_F v prime minus D_F v delta p prime F which also hold good for element F. Now, the mass flow rate corrections at cell face is estimated as $\rho_f V_f$ prime dot S_f where the correction velocity field is obtained as minus D_f v delta prime f minus delta prime f bar. Now, if we put together all these equations, so, finally, we will get the pressure corrections equation in this format which is faces over $\rho_f V_f$ dot S_f plus all the faces $\rho_f D_f$ v delta p prime, this dot S_f , then minus $\rho_f D_f$ v delta p prime. So, dot S_f equals to minus, this is going to be m dot star f.

Now, this portion actually represents the neighboring velocity corrections on the velocity of the element. Now, this influence will become much more visible when we interpolate this things to the face and get an equivalent expression like V_f prime plus H_f v prime minus D_f v delta p prime which will lead to v prime plus D_f v delta p prime and equals to minus H_f v prime. Now, once we substitute this one here, you can get summation of f

NB $\rho_f D_f v \Delta p' \cdot S_f$ equals to minus f which is $m \cdot f$ plus f goes over the faces, $\rho_f H_f \cdot S_f$.

So, this term one can find it out more explicitly in the following form.

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Fluid Flow problems: incompressible

$$\sum_{f \in \text{nb}(c)} (-\rho_f \bar{D}_f^T (\nabla p')_f \cdot S_f) = - \sum_{f \in \text{nb}(c)} \dot{m}_f + \sum_{f \in \text{nb}(c)} \left(\rho_f \left(\sum_{f \in \text{nb}(c)} \frac{a_{f'}}{a_c'} v_f' \right) \cdot S_f \right)$$

$$\overline{\bar{D}_f^T (\nabla p')_f} \cdot S_f = \left((\nabla p')_f \bar{D}_f^T \right) \cdot S_f = (\nabla p')_f \cdot \left(\bar{D}_f^T \cdot S_f \right)$$

$$= (\nabla p')_f \cdot S_f'$$

$$S_f' = \bar{D}_f^T \cdot S_f = \begin{bmatrix} \bar{D}_f^x & 0 & 0 \\ 0 & \bar{D}_f^y & 0 \\ 0 & 0 & \bar{D}_f^z \end{bmatrix} \begin{bmatrix} S_f^x \\ S_f^y \\ S_f^z \end{bmatrix} = \begin{bmatrix} \bar{D}_f^x S_f^x \\ \bar{D}_f^y S_f^y \\ \bar{D}_f^z S_f^z \end{bmatrix}$$

$$\begin{aligned} (\nabla p')_f \cdot S_f' &= (\nabla p')_f \cdot E_f + (\nabla p')_f \cdot T_f \\ &= \frac{E_f}{d_c} (\rho_p' - \rho_c') + (\nabla p')_f \cdot T_f \end{aligned} \quad \left| \quad S_f' = \underline{E_f} + \underline{T_f} \right.$$

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So, you can find out this is f which is minus $\rho_f D_f v p' \cdot S_f$ which is minus $n f c m \cdot f$ plus f goes from their ρ_f summation of over $n B c a b$ by $a c v V$ prime F . So, this is $\bar{\rho} \cdot S_f$. So, this is done and the previous equation this underline term. So, this term is critical for solution of this equations. Now, in the original simple equation or algorithm, this was actually neglected for the coupling of pressure and velocity.

But because this is a correction equation, the modification or the dropping of these turn will not affect the final solution since at convergence, the correction becomes 0; however, it may affect the convergence rate in the larger. Convergence rate in that the larger is neglected term, the higher will be the error present in the approximate at each iteration.

Now, the remaining term can be easily treated and the coefficient of the pressure correction terms can be obtained in a simplified form. For example, we take these term which is present there and $\Delta p' \cdot S_f$ which is $\Delta p' \cdot D_f v$ transpose $\cdot S_f$ which is $\Delta p' \cdot$ this transpose $\cdot S_f$ which is $\Delta p' \cdot f \cdot S_f$ prime.

Now, the expanded expression is giving that S_f prime equals to D_f prime transpose dot S_f which will be $D_f u$ 0 0, 0 $D_f v$ 0 0, 0 0 $D_f w$ into $f_x S_f y S_f z$ which will get you $D_f u S_f x$, $D_f v S_f y$, $D_f w S_f z$. So, now, you can work with this prime component the surface vector component and the pressure correction gradient can be calculated like Δp prime $f \cdot S_f$ prime equals to now Δp prime dot E_f plus Δp prime dot T_f . So, which is like an implicit component, this is the cross diffusion component. This we have seen while looking at the discretization of the diffusion equation.

So, this will become E_f by $d_c F$ and p_F minus p_c prime plus Δp prime $f \cdot T_f$ where the S_f prime will have two component E_f plus T_f . So, one is along the line which is connecting between the cell centre and this is normal to that. So, these are already discussed while discussing. Now, if you drop the non orthogonal contribution and linearize the term of the pressure correction equation, then this guy will become Δp prime $f \cdot S_f$ prime equals to E_f by $d_c F$ where p_F minus p_c prime which will become D_f minus p_F prime minus p_c prime.

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Fluid Flow problems: incompressible

$$(\nabla p')_f \cdot S'_f = \frac{E_f}{d_{CF}} (p'_F - p'_c) = D_f (p'_F - p'_c)$$

$$a'_c p'_c + \sum_{F \in \text{NB}(c)} a'_F p'_F = b'_c$$

$$a'_F = \text{Flow}_F = -\rho_f D_f$$

$$a'_c = - \sum_{F \in \text{NB}(c)} \text{Flow}_F = - \sum_{F \in \text{NB}(c)} a'_F$$

$$b'_c = - \sum_{F \in \text{NB}(c)} \text{Flow}_F + \sum_{F \in \text{NB}(c)} \left(\frac{\rho_f \bar{H}_F [v] \cdot S_f}{d_{CF}} \right)$$

$$= - \sum_{F \in \text{NB}(c)} m'_F + \sum_{F \in \text{NB}(c)} \left(\frac{\rho_f \bar{H}_F [v] \cdot S_f}{d_{CF}} \right)$$

original
SIMPLE
- neglected

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Now, once we substitute that in that this in the pressure corrections equation, so that we will look a simple correction equation like plus F go over all the cells $a_F p$ prime p_F prime equals to $b_c p$ prime. So, and the coefficients are $a_F p$ prime equals to flux F_f which is minus $\rho_f D_f$, $a_c p$ prime equals to minus F which is flux F_f minus summation over all the cell $a_F p$ prime and $b_c p$ prime equals to summation flux V_f

plus summation over rho f H f V prime dot S f which one can write summation over this plus summation over rho f H f dot S f. So, you can actually different approximation can be used for these terms, I mean either of these or this. And once you use different approximation for this term, that will lead to a different sort of algorithm but when we will look that the original simple algorithm, the original simple algorithm, these terms are essentially neglected, these are neglected.

Now, one can think about once you neglect that, what can happen to the solution. The solution finally, still you can achieve the solution because it is a iterative process, but it may slow down or some sort of errors will accumulate over the iteration.

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Fluid Flow problems: incompressible

$$\dot{m}_f^* = \rho \bar{V}_f^* \cdot S_f = \rho \bar{V}_f^* \cdot S_f - D_f^v (\nabla p_f^{(n)} - \nabla p_f^{(n-1)}) \cdot S_f$$

$$\bar{V}_c^{**} = \bar{V}_c^* + \bar{V}_c', \quad \bar{V}_c' = -D_c^v (\nabla p')_c$$


$$\dot{m}_f^{**} = \dot{m}_f^* + \dot{m}_f', \quad \dot{m}_f' = -\rho_f D_f^v \nabla p_f' \cdot S_f$$

$$p_c^* = p_c^{(n)} + \lambda p_c'$$

$S_f' = E_f + T_f$

(a) Min. Correction Approach $E_f = (e_{cf} \cdot S_f') e_{cf}$

$e_{cf} = \text{unit vector in the CF direction}$



Now, after getting all these corrections and the Rhie Chow interpolation, finally, the mass flow rate can be calculated as rho V f, now rho V star f dot S f minus D f v minus delta p f n minus delta p f n bar dot S f.

Now, the pressure and velocity field which are corrected and calculated at the cell centre, they can be used to correct the mass flow rate. And now one thing is there, once you get those things, then the velocity field is corrected as V c star plus V c prime where V c prime is corrected as del p prime by c and m dot star star f which is corrected as plus m dot f prime and m dot f prime equals to minus rho f D f v delta p f prime dot S f and p c star is p c n plus lambda pc prime. So, some sort of an under relaxation which is used to update the pressure.

Now, the kind of decompositions which can be used as we have looked at in our previous diffusion calculation for this component where your S_f is E_f plus T_f , so here one can different multiple approaches can be adopted one can do minimum correction approach which we can refer to our diffusion system where this can be calculated as $E_f \cdot e_{cF}$ and e_{cF} is the unit vector in the cF direction.

Now, once we combined that, so the readers are or all of your strongly encourage to go back and look this calculations in the context of diffusion equation because these are discussed in details there.

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Fluid Flow problems: incompressible

$$E_f = \frac{d_{cf}^2 \nabla_f^2 s_f^x + d_{cf}^2 \nabla_f^2 s_f^y + d_{cf}^2 \nabla_f^2 s_f^z}{d_{cf}^2} d_{cf}$$

$$D_f = \frac{E_f}{d_{cf}} =$$

(b) Orthogonal correction approach $E_f = S_f' e_{cF}$

$$D_f = \frac{E_f}{d_{cf}} = \sqrt{\frac{(\nabla_f^2 s_f^x)^2 + (\nabla_f^2 s_f^y)^2 + (\nabla_f^2 s_f^z)^2}{(d_{cf}^x)^2 + (d_{cf}^y)^2 + (d_{cf}^z)^2}}$$

(c) Over-Relaxed approach $E_f = \frac{S_f' \cdot S_f'}{d_{cf} \cdot S_f'} d_{cf}$

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So, E_f would become $d_{cF} \times D_f \times S_f^x$ plus $y D_f \times S_f^y$ plus $d_{cF} \times D_f \times S_f^z$ divided by d_{cF}^2 and d_{cF} which following the expression one can find out E_f by d_{cF} . So, one can put those expression back here.

Now, other way round, one can do the orthogonal correction approach where you find E_f as $S_f' \cdot e_{cF}$ and then you calculate E_f by d_{cF} which is nothing but $D_f \times S_f^x$ square $D_f \times S_f^y$ square $D_f \times S_f^z$ square divided by d_{cF}^x square d_{cF}^y square d_{cF}^z square. So, and third option could be over relaxed approach over relaxed approach where you get $E_f \cdot S_f \cdot S_f' \cdot d_{cF} \cdot d_{cF}$. These are again; these are all discussed in details in the context of diffusion system.

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Fluid Flow problems: incompressible

$$D_f = \frac{(\overline{D_f^x s_f^x})^2 + (\overline{D_f^y s_f^y})^2 + (\overline{D_f^z s_f^z})^2}{d_{cf}^x \overline{D_f^x s_f^x} + d_{cf}^y \overline{D_f^y s_f^y} + d_{cf}^z \overline{D_f^z s_f^z}}$$

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So, the reader can go back and look at those derivation in details there. Then, you can correlate the thing here easily, $D_f w S_f z$ square divided by $d_{cf} x D_f u S_f x$ plus $d_{cf} y D_f v S_f y$ plus $d_{cf} z D_f w S_f z$. So, one can be done. So, we will stop here today and we will take from here in the follow up lectures.

Thank you.