

Satellite Attitude Dynamics and Control
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Lecture - 54
Gyrostat (Contd.)

Welcome to the lecture number 54, so we have been discussing about the Gyrostat.

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lecture - 54

Linearized Rotational Dynamics of Gyrostat

$\vec{M}_{ext} = M_1 \rightarrow M_2 + M_d + M_{solar} + M_{aerody} + M_{thunder} + M_{mag-field}$
 $M_2 \rightarrow$ moment due to gravity gradient
 M_3

1- Analysis $M_1 = -3n^2 (J_2 - J_3) C_{23} C_{33}$

$J_1 \dot{\omega}_1 - \omega_2 \omega_3 (J_2 - J_3) + \dot{h}_2 + \omega_2 \dot{h}_3 - \omega_3 (\dot{h}_2 - h_0) = -3n^2 (J_2 - J_3) C_{23} C_{33}$

+ M_{solar}
+ $M_{thunder}$
+ M_{mag}

So, we derive the equation of motion for the Gyrostat in the expanded format and now we are going to linearize that system in order to get basically once you are trying to control the satellite and you are looking for the local control, means the small disturbances I have occurred and for that you are trying to control the satellite.

So, in that case you have to linearize it and get into the linearized equation of motion, we have done it so many times for the gravity gradient satellite for the spin stabilized satellite. So, for them we have linearize the equation of motion and we have written that so it is the same part only thing some extra added things are added here.

So, here the external torque see once we are writing the equation that M_{ext} and then we are writing here as M_1 and the other part as M_2 and the third part as M_3 . So, this can consist of M gravity gradient plus M disturbance plus M torque due to other

things like there may be the torque due to the solar radiation, torque may be due to the aerodynamic drive ok.

Then torque may be due to the thrusters then torque may be due to the magnetic move field and so on just keep adding ok. So, the torque this is long one direction, so this will be corresponding direction torque we have to write it like this. So, here what I am going to do that this part will be always present, the moment due to gravity gradient this is moment due to gravity gradient.

So, it is a customary to write this equation what we have derived earlier, so instead of just writing I will just write M 1 instead of M g 1 and this you know this quantity will be equal to minus 3 omega 0 square which we have written as omega n square in the gravity gradient equation.

So, n equal to omega 0 this is the orbital frequency orbital frequency of the satellite, this is the orbital frequency of the satellite and this times minus I 2 minus I 3 and then also we have written here C 23 C 33 ok. So, these are the coefficients from the direction cosine matrix and obviously this is along the body axis.

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3 equations for the gradient

$$M_1 = [J_1 \dot{\omega}_1 - \omega_2 \omega_3 (J_2 - J_3)] + \dot{h}_1 + \omega_2 h_{\omega_3} - \omega_3 (h_{\omega_2} - H_0)$$

$$M_2 = [J_2 \dot{\omega}_2 - \omega_3 \omega_1 (J_3 - J_1)] + \dot{h}_2 + \omega_3 h_{\omega_1} - \omega_1 h_{\omega_2}$$

$$M_3 = [J_3 \dot{\omega}_3 - \omega_1 \omega_2 (J_1 - J_2)] + \dot{h}_3 + \omega_1 (h_{\omega_2} - H_0) - \omega_2 h_{\omega_1}$$

2nd term in the previous equations

$$\vec{\omega} \times [h_{\omega_1} \hat{e}_1 + h_{\omega_2} \hat{e}_2 + h_{\omega_3} \hat{e}_3 - H_0 \hat{e}_2] = \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix} \begin{bmatrix} h_{\omega_1} \\ h_{\omega_2} - H_0 \\ h_{\omega_3} \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} -\omega_3 (h_{\omega_2} - H_0) + \omega_2 h_{\omega_3} \\ \omega_3 h_{\omega_1} - \omega_1 h_{\omega_3} \\ -\omega_2 h_{\omega_1} + \omega_1 (h_{\omega_2} - H_0) \end{bmatrix}$$

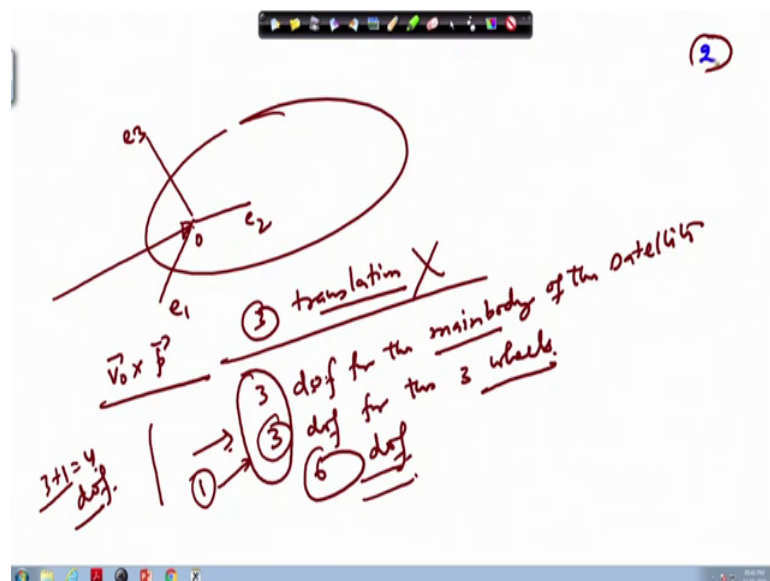
So, one body axis and if this linearized equation has to be modified, so simply on the right hand side say if I expand the previous equation here written this particular one. So, if I right here the gravitational term were the M g 1 and the other terms right now I will

ignore and put that is 0 whenever required so you can just insert that value on the right hand side you will get the equation I will show you what I mean so far as I work so that will be much more clear.

So, in that context so we are start with the our equation, so M_1 this equal to S will write it on the right hand side let us first write the, I will copy this part first from this place this whole thing. So, J_1 times ω_1 dot here while writing everything has got into $I_1 I_2 I_3$ form. So, maybe I will modify this to $I_1 I_2$ and I_3 because, otherwise every were I have to change let me do that this is $J_1 J_2 J_3 J_1 J_2$.

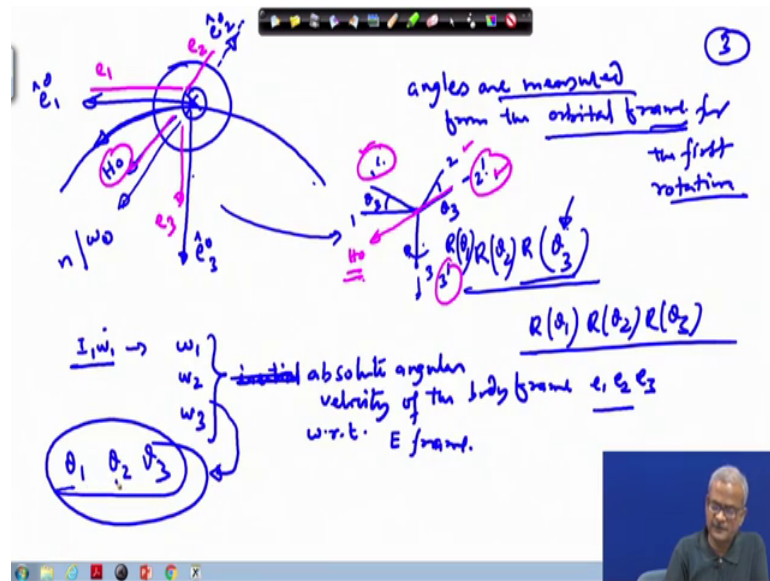
So, here then this becomes ω_2 times $\omega_3 J_2$ minus J_3 and then pick up the other terms with is h_2 dot and plus ω_2 times h_3 minus ω_3 times h_2 and minus H_0 this is what is here h_2 minus H_0 and we right here M_1 on the right hand side. So, this M_1 instead of writing here M_1 the gravity gradient term which I will pick up from this place and right here, oh ok.

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This some over other S_6 is written, this should be 2 this is 2 and then sum the 3 ok.

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So, here we are writing the gravity gradient term which is J_2 minus J_3 times $C_2 C_3$ times $C_3 C_3$. Now what I was telling that this is only the gravity the gradient term and other terms right now I am assuming 0 ok, like the M solar radiation plus M aerodynamic torque plus movement due to the safe you have the thrusters ok, movement due to the magnetic movement or the magnetic field.

So, all these things I will assume this to be 0 right now and I will simplify this equation. So, whenever required on the right hand side of this equation if you put this quantities, so automatically you will get the linearized dynamics along with the other terms. Now this term here \dot{h}_2 is present this term can be utilised for steering the satellite ok, inside if you change the angular momentum of the this wheel by actuating a motor ok.

So, by changing this you will produce a torque on has if you are a speeding it up, so the main body will also feel a torque in the opposite direction ok. So, along the 3 axis by using this h_1, h_2, h_3 we can steer the satellite and that is the internal control and the external control occurs like from the solar radiation from the magnetic moment from the aerodynamic torque and so on ok. So, therefore, it is h_1 here on the left hand side because, this is internal part and the external part can be shown on the right hand side.

So, this gravity gradient which is present here, so it has appeared on the right hand side but as we simplify this equation, so we will take it on the left hand side itself and right

hand side will put to 0 and anytime you can put the other forces there and do the competition.

So, in this context we need to look into what will be the corresponding angular velocity in terms of θ_1 , θ_2 , θ_3 . So, what exactly we have done we need to 2 and the 3 equation. So, your satellite is this is the e_3 direction e_1 cap and the satellite is like this.

So, the 2 direction is going inside and so the orbital angular velocity it lies here in this direction or the orbital frequency it is a corresponding vector it will lie here because, it is the satellite is going here along this in the orbit and therefore it will lie here in this direction which we have written as ω_0 or the same thing as n we have written ω_0 or n the notation we have used.

So, this is your e_2 positive direction, so satellite is going in this orbit and then it is a perturbed from this condition ok. So, we are measuring the angles from the orbital reference frame, so angles are being measured this we have discussed earlier, but here I am again repeating for the sake of your convenience.

So, angles are measured from the orbital frame; which one? The first rotation whichever you choose ok, there after the things will change say this is your right now this is the corresponding axis which is shown here. So, if I give rotation about the first axis so this rotation about the first axis, so I should show in the positive direction positive direction will be toward this. So, this will go from this place to this place and this will go here so this is 1 this is 2, so this will become 1 prime and this will become 2 prime this is 3.

So, 3 prime will remain here, the next rotation I give about the 2 axis, so this rotation I am writing as θ_1 this is θ_2 . So, all the rotations angles are measured from the orbital reference frame for the first rotation and there after it has changed because now it has become I_1 prime I_2 prime and a 1 prime 2 prime and 3 prime, so no longer this is the orbital reference frame. So, 3 you cancel rotation we can give say first we have given about the three. So, we are writing that as θ_3 not θ_1 , so this is θ_3 which is equivalent to ψ_3 so this is θ_3 .

So first rotation we give as θ_3 , so this is the corresponding rotation matrix there after we give the next rotation as the θ_2 about the 2 axis and then about the 1 axis means

R_{θ_1} , R_{θ_2} and R_{θ_3} is the corresponding set of rotation we are choosing and inside the wheel already you are giving the bias momentum. So, you are giving the bias momentum along this direction I told you that it is along the e_2 direction of the body axis. So, write in the beginning your body axis is coinciding with this frame, so your body axis is like this is e_1 this is e_2 and vertically down is your e_3 .

So, H_0 will be pointing write in the beginning here in this direction if you give disturbance, so this H_0 vector will be then in other direction. So, H_0 is bias momentum so I am not giving it along the positive e_2 direction ok, but this will always point opposite to e_2 direction. So, if your from this say in the next level ones your distorted by this so 1 will come to this position and then the body axis will be here this $2'$ position it will come your body axis $1'$, $2'$ and $3'$ ok.

So, your h vector then will be just opposite to this $2'$ direction, so this is what we are calling as the bias momentum. So, this is given to the wheel and this will help maintain the orientation of the satellite, if the wheel is large or the velocity of the wheel it is a angular velocity of the wheel is very high a small wheel very high angular velocity.

So we go about doing all this things, so in your equation of motion where $I_1 \dot{\omega}_1$ it is appearing. So, we need to find out this ω_1 , ω_2 and ω_3 , these are your inertial or is simply say the absolute angular velocity of the body frame e_1 , e_2 and e_3 means with respect to this is with respect to the e frame.

And therefore we need to, if we are work trying to work in terms of the θ_1 , θ_2 how with respect to the orbital reference frame your system is getting disturbed what will be it is orientation with respect to the orbital reference frame that we will measure in terms of θ_1 , θ_2 and θ_3 ok. So, this ω_1 , ω_2 , ω_3 must be converted in terms of θ_1 , θ_2 , θ_3 as we have done earlier also. So, let us convert that, so first I will simply a state those values and there after I will do that I have done it earlier also.

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Handwritten notes on a whiteboard:

- $$\begin{aligned} w_1 &= \dot{\theta}_1 - n\theta_3 \\ w_2 &= \dot{\theta}_2 - n \\ w_3 &= \dot{\theta}_3 + n\theta_1 \end{aligned}$$
- $$\vec{w}_y \rightarrow \text{ang. vel. of the satellite w.r.t. to the orbital frame (but components along the body axes)}$$
- $$\vec{w} = \vec{w}_0 + \vec{w}_r$$
- $$\begin{bmatrix} w_1 \\ w_2 \\ w_3 \end{bmatrix} = \vec{w}_r = -\omega_0 \hat{e}_2 + \begin{bmatrix} w_{r1} \\ w_{r2} \\ w_{r3} \end{bmatrix}$$
- $$\begin{bmatrix} w_{r1} \\ w_{r2} \\ w_{r3} \end{bmatrix} = \begin{bmatrix} \phi \\ \psi \\ \gamma \end{bmatrix} = \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix}$$
- $$\begin{bmatrix} w_{r1} \\ w_{r2} \\ w_{r3} \end{bmatrix} = \begin{bmatrix} 1 & 0 & -s\theta_2 \\ 0 & c\theta_1 & s\theta_1 c\theta_2 \\ 0 & -s\theta_1 & c\theta_1 c\theta_2 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & -\theta_2 \\ 0 & 1 & \theta_1 \\ 0 & -\theta_1 & 1 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix} = \begin{bmatrix} \dot{\theta}_1 - \theta_2 \dot{\theta}_3 \\ \dot{\theta}_2 + \theta_1 \dot{\theta}_3 \\ \dot{\theta}_3 - \theta_1 \dot{\theta}_2 \end{bmatrix}$$

But again I will repeat $\theta_2 - n\theta_3 = \dot{\theta}_3 + n\theta_1$; and how we are getting? For this we are using the information that ω this will be equal to absolute angular velocity ω_r plus ω_0 , means this the orbital reference frame and or either we can write it this way, first we write ω_0 and with respect to orbital reference frame how your body is moving.

So, that gives it the absolute angular velocity; and what this quantity is? This is ω_0 times \hat{e}_2 with minus sign ok, here your angular velocity is directed along this direction which is the negative \hat{e}_2 direction ok.

So, this will come with minus ω_0 times \hat{e}_2 it is a pointing along this direction and what this quantity is this quantity is your angular velocity with respect to the orbital frame. But we will take it along the body axis ok, with respect to the orbital frame this is ω_r ω_r is the angular velocity angular velocity of the satellite with respect to the orbital frame.

But components taken along the later on we have to do, but components along the body axis. So obviously that we are trying to measure in terms of we will write this as first as ω_r 1, see in the matrix notation we can write as ω_r 1 ω_r 2 ω_r 3. So, this the left hand side in the matrix notation, this can be written as ω_1 ω_2 ω_3 this is the absolute angular velocity, this is the absolute angular velocity.

So, we have to get up to this equation now ω_r ω_r^2 ω_r^3 these are the body rates and they are connected with as we have derived earlier, like if you remember we have written the equation in terms of the $\dot{\phi}$ $\dot{\theta}$ and the $\dot{\psi}$ and this we multiplied by a matrix and converted it to the corresponding p q r or we have use the notation for this perhaps ω_r^1 or ω_r^1 , I do not remember exactly.

So, this is the notation means this is the angular velocity along the body axis x body axis y body axis z body axis or either the 1 other the 2 and this is along the third direction and this matrix we have written here ok. So, this derivation I will not be doing here, I will just re call from the previous one, so here your ω_r^1 ω_r^2 ω_r^3 this can be written as $\begin{bmatrix} 1 & 0 & -S\theta_2 \\ 0 & C\theta_1 & 0 \\ 0 & S\theta_1 & C\theta_2 \end{bmatrix}$, I am repeating it there was no need to repeat, but because it is a not a book where I am writing here. So, it will be difficult for you to immediately go back to the lectures and look into that, so therefore I am just repeating it, $C\theta_1$ times $C\theta_2$ and this $\dot{\phi}$ $\dot{\theta}$ $\dot{\psi}$ then we are writing as $\dot{\theta}_1$ $\dot{\theta}_2$ $\dot{\theta}_3$ this is what we have done.

So if we assume a small angle, so this gets reduced to one will remain 1 this will remain 0 and this will be minus θ_2 this remains 0 $\theta_2 \cos \theta_1$ this becomes one for a small θ_1 θ_2 θ_3 . So, θ_1 θ_2 θ_3 are small, so that approximation can be done this are small. So, this one gets reduced to θ_1 and this part is 0 this is minus θ_1 and $C\theta_1 C\theta_2$ that becomes 1 times $\dot{\theta}_1$ $\dot{\theta}_2$ $\dot{\theta}_3$ so this gets reduced to.

Now, we can see that we can write this as $\dot{\theta}_1$ minus θ_2 times $\dot{\theta}_3$; θ_2 times $\dot{\theta}_3$ dot and the other part this we can write as $\dot{\theta}_2$ plus θ_1 times $\dot{\theta}_3$ dot and this one as $\dot{\theta}_3$ minus θ_1 times $\dot{\theta}_2$ dot. So, this is your ω_r this quantity then it becomes ok, thereafter if you see this the these are the terms which are together these are the small terms ok, so this is the second order terms so we ignore it.

So, conveniently you can remember that ω_r^1 ω_r^2 can be replaced by this because this term are second order term. So, the they can be ignored ok, therefore your this part gets reduced by $\dot{\theta}_1$ $\dot{\theta}_2$ $\dot{\theta}_3$ and this part we have to write just use it write it properly.

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The image shows a handwritten derivation on a whiteboard. At the top left, a coordinate system is shown with unit vectors \hat{e}_1 , \hat{e}_2 , and \hat{e}_3 . A vector \hat{e}_2^o is shown pointing along the \hat{e}_2 axis. The rotation matrix R is defined as $R(\theta_1)R(\theta_2)R(\theta_3) = R$. The matrix R is written as:

$$R = \begin{bmatrix} \theta_1 - n\theta_3 & & \\ \theta_2 - n & & \\ \theta_3 + n\theta_1 & & \end{bmatrix}$$

The vector \hat{e}_2^o is expressed as a linear combination of the body frame unit vectors:

$$\hat{e}_2^o = c_{12}\hat{e}_1 + c_{22}\hat{e}_2 + c_{32}\hat{e}_3$$

The derivation also shows the matrix A and the vector \hat{e}^b :

$$\hat{e}^b = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

$$A = \begin{bmatrix} c_{11} & c_{12} & c_{13} \\ c_{21} & c_{22} & c_{23} \\ c_{31} & c_{32} & c_{33} \end{bmatrix}$$

So, you then the omega 1 omega 2 omega 3 these vector can be written in terms of minus omega 0 times or we are writing in terms of n. So, this will write as n because n is much more convenient to write.

So, minus n times \hat{e}_2 cap and then plus omega r 1 omega r 2 omega r 3 which is nothing but theta 1 dot theta 2 dot theta 3 dot, here \hat{e}_2 this is a vector 0 1 0 this a unit vector along the second axis of the orbital frame ok. So, \hat{e}_2 is vector is written like this, so that if we want to convert this into the body frame means what will be it is components along the body frame of this vector.

So, that will be can be written as along the body frame as here the attitude matrix times 0 1 0 and you know that attitude matrix it can be written in terms of $C_{11} C_{12} C_{13} C_{21} C_{22} C_{23} C_{31} C_{32} C_{33}$ and then 0 1 0 ok. So, the corresponding components then will turn out as $C_{12} C_{22}$ and C_{32} .

So, this factor then becomes minus $C_{12} C_{22}$ and C_{32} of the attitude matrix and attitude matrix how you are getting from the orbital frame $\hat{e}_o 1 \hat{e}_o 2$ and $\hat{e}_o 3$ you are giving 3 rotations, the first rotation you have given by r theta 3 the second by r theta 2 and the third by r theta 1, so in the sequence you are giving this rotation ok. So, this r matrix this is equal equivalent to r and from this we have to choose this values ok, so this times n and plus theta 1 dot theta 2 dot and theta 3 dot and I have also ok.

If so e if you get time go back and look into the lectures I have written this $C_{\theta_2} S_{\theta_3} \hat{e}_1 + C_{\theta_1}$, this is the how the body frame is associated with the your orbital frame. So, $C_{\theta_1} C_{\theta_3} + S_{\theta_1} S_{\theta_2} S_{\theta_3} \hat{e}_2$ and plus minus $S_{\theta_1} C_{\theta_3} + C_{\theta_1} S_{\theta_2} S_{\theta_3}$.

So, this \hat{e}_2 vector is nothing but the quantity which I have shown here, and this is written in terms of \hat{e}_1 , \hat{e}_2 and \hat{e}_3 and that how you can get you look back into the lectures I have done this in quite details ok. So, I am avoiding it here, so this quantity is basically your the first term is $C_{12} \hat{e}_1$ plus the second term is $C_{22} \hat{e}_2$ and the third one is $C_{32} \hat{e}_3$ ok.

So, this term is here this term is here and this term is here, in this place and once we do the approximation, so in the approximation you can see that the \hat{e}_2 term it can get reduced to C_{02} and this will be 1 and this will be θ_3 times θ_3 times \hat{e}_1 θ_3 times \hat{e}_1 , the second term will then appear as this will be 1 and this is all the this becomes a third order term this particular part and therefore that drops out.

So, this will be simply \hat{e}_2 and here again this term is the second order term S_{θ_2} and $S_{\theta_3} S_{\theta_2} S_{\theta_3}$ or $\sin \theta_2 \sin \theta_3$, so this term also drops out we are left with this which is minus θ_1 , so this is minus θ_1 times \hat{e}_3 ok. So the corresponding term then this becomes θ_3 this becomes 1 and this becomes minus θ_1 and then obviously we can simplify all this things.

So, I will right here in this place itself this result so if we take this part. So, this becomes $\theta_1 \dot{\theta}_3 - \theta_2 \dot{\theta}_3 + \theta_3 \dot{\theta}_1$. So, this is what you get as $\omega_1 \omega_2 \omega_3$, so this quantity is nothing but your, I will write face on the next page $\theta_2 \dot{\theta}_3 - \theta_3 \dot{\theta}_2 + \theta_3 \dot{\theta}_1$.

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$R = R(\theta_1)R(\theta_2)R(\theta_3) \rightarrow$
 $\vec{\theta} = \begin{pmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{pmatrix}$
 $R = \mathbb{I} - \vec{\theta} \times = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} - \begin{bmatrix} 0 & -\theta_3 & \theta_2 \\ \theta_3 & 0 & -\theta_1 \\ -\theta_2 & \theta_1 & 0 \end{bmatrix}$
 $R = \begin{bmatrix} 1 + \theta_3 & -\theta_2 & \theta_1 \\ -\theta_3 & 1 & \theta_1 \\ \theta_2 & -\theta_1 & 1 \end{bmatrix}$
 $m_1 = -3n^2(I_2 - I_3) \rightarrow c_{23}c_{33} = \theta_1$
 $m_2 = -3n^2(I_3 - I_1) \rightarrow c_{33}c_{13} = (-\theta_2)$
 $m_3 = -3n^2(I_1 - I_2) \rightarrow c_{13}c_{23} = \theta_1(-\theta_3) = 0$
 $c_{23} = \theta_1$
 $c_{13} = -\theta_2$
 $c_{33} = 1$

One thing also I will remind you that for a small rotation, so of the order does not matter, means the we have chosen the order choosing the order here r theta 3 we have use this order, but if the angles are small so this order is immaterial and in that case the r we have written as simply as I matrix or the I this is identity matrix unit matrix not the inertia matrix.

So, we can change the notation maybe and minus theta tilde cross where theta tilde is nothing but theta 1 theta 2 theta 3. So, instead of using that much of expansion we could have directly written in terms of this becomes 1 1 1 0 0 0 0 and minus theta tilde cross. So, that become 0 0 a this is the skew symmetric matrix so minus theta 3 theta 2 theta 1 theta 1 here minus theta 2 and this is theta 3.

So, this gets reduced to 1 minus theta 3 theta 2 with minus sign here this gets plus sign here and this is minus theta 3 and then this becomes 1 this will come with positive sign here this will come with a negative sign and this will become with a positive sign, so this is your R matrix. And this you can directly used to convert from the orbital frame to the body frame which we have already done here in this place ok.

So, this part we have already done here, n times theta 3 minus n times, so basically C 1 2 C 2 2 and C 3 2 where we are looking for which were nothing but the this part, this is your C 1 2 C 2 2 and C 3 2. So, this is the vector we have chosen here theta 3 1 and

minus theta 1, so utilise it and write the equations; so, there after we can expand the equation.

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$$I_1 \dot{\omega}_1 - \omega_2 \omega_3 (I_2 - I_3) + \dot{h}_1 + \omega_2 h_3 - \omega_3 (h_2 - H_0) = -3n^2 (I_2 - I_3) \theta_1$$

$$I_1 (\ddot{\theta}_1 - n \dot{\theta}_3) - (\dot{\theta}_2 - n) (\dot{\theta}_3 + n \theta_1) (I_2 - I_3) + \dot{h}_1 + (\dot{\theta}_2 - n) h_3 - (\dot{\theta}_3 + n \theta_1) (h_2 - H_0) = -3n^2 (I_2 - I_3) \theta_1$$

$$I_1 \ddot{\theta}_1 - I_1 n \dot{\theta}_3 - [\dot{\theta}_2 \dot{\theta}_3 + \dot{\theta}_2 n \theta_1 - n \dot{\theta}_3 - n^2 \theta_1] (I_2 - I_3) + \dot{h}_1 + \dot{\theta}_2 n h_3 - \dot{\theta}_3 h_2 + \dot{\theta}_3 H_0 - n \theta_1 h_2 + n \theta_1 H_0 + 3n^2 (I_2 - I_3) \theta_1 = 0$$

$$I_1 \ddot{\theta}_1 + [(n^2 \theta_1 + 3n^2 \theta_1) (I_2 - I_3) + n \theta_1 H_0] - [I_1 n \dot{\theta}_3 - (I_2 - I_3) n \dot{\theta}_3 - H_0 \dot{\theta}_3] + \dot{h}_1 - n h_2 = 0$$

Once we have got this the rest of the things will be straight forward and also for the small angles similarly a in the inertia term this gravity gradient term will be getting terms like M_1 equal to $3n^2(I_2 - I_3)$ then C_{23} times C_{33} and M_2 equal to $-3n^2(I_3 - I_1)C_{13}$ and M_3 we get as $-3n^2(I_1 - I_2)$. So, this will be C_{13} times C_{23} so this we have already done ok.

Now, we also need this quantities ok, so these quantities you can choose from this matrix here for simplicity because the angles are a small so C_{23} it refers to your the terms we can choose directly from this place C_{23} . So, C_{23} is nothing but your theta 1 ok, so C_{23} this becomes theta 1 and here of course one term is missing, here there is 1 one once we add this we have added with minus sign this is got this term has got subtracted from this term. So, we are getting this so one is here ok.

So, this is this term is C_{23} is theta 1 similarly we have C_{13} C_{13} C_{13} the first row third one so this is your C_{13} ok. So, C_{13} is minus theta 2 and similarly C_{23} we have already done C_{33} , so C_{33} is nothing but your term which is present here C_{33} .

So, C_{33} this equal to 1 and we can insert it here and rewrite our equation, so here itself let us reduce this part. So, this part will be C_{13} times C_{23} you can see C_{13} times

C_1^3 this will be of second order. So, this quantity will be $\theta_1 - \theta_2$ so this will be equal to 0 this is second order term. So, will neglect it C_3^3 is 1 C_1^3 is minus θ_2 , so this becomes equal to minus θ_2 and this term C_2^3 time C_3^3 that becomes θ_1 . So, this term is θ_1 , this term is minus θ_2 and this term is 0.

So next we start rewriting our equation, so we have $I_1 \dot{\omega}_1 - \omega_2 h_1 \dot{\theta}_1 + \omega_2 h_3 - \omega_3 h_2 - H_0$ on the right hand side we have minus $3n^2 I_2 - I_3$ and the other term this is θ_1 this term ok. So, we pick up this and here we get as θ_1 ok, left hand side we have to rewrite because we have not linearized it so ω_1 is $\dot{\theta}_1$. So, that becomes $\ddot{\theta}_1$ and then minus n times θ_3 ok, so that becomes n is a constant so we will not differentiate this this is $\dot{\theta}_3 - \omega_2$. Similarly this is $\dot{\theta}_2 - n$ and this becomes $\dot{\theta}_3 + n \theta_1$ which is $\omega_3 I_2 - I_3$ times this plus $h_1 \dot{\theta}_1$ and plus ω_2 .

So, ω_2 again this is $\theta_2 \dot{\theta}_2 - n h_3 - \omega_3$ which is we have to expand it, so ω_3 is $\dot{\theta}_3 + n \theta_1 h_2 - H_0$ this equal to minus $3n^2 I_2 - I_3$ times θ_1 , already we have linearized this is the linearized part; is the linearized part ok. So, this quantity we have written here so breakup and do the approximation this type of work already we have done this is I_1 ok.

So, $I_1 n \dot{\theta}_3$ here this part we will expand it, so minus $\dot{\theta}_2 \dot{\theta}_3 - n \theta_1 \dot{\theta}_3 - n^2 \theta_1 h_2 - I_2 - I_3$. So, this terms are old terms what we have discussed earlier they are the same term, only thing this h related term they are now appearing as the extra one, $\theta_2 - n h_3$.

Here also we can break and if we break it so this will be $\dot{\theta}_3 h_2 + \dot{\theta}_3 H_0 - n \theta_1 h_2$ and this makes it minus $n \theta_1 H_0$ and this minus minus that gets plus sign. And then this term also we bring on the left hand side $I_2 - I_3$ times θ_1 this will be equal to 0.

So, here the second order terms will be dropped out, so this term is 0, this being second order this term is dropped out being second order and the terms like this will be equal to 0 why because h_2 is initially 0 and then you are speeding of the wheel.

So, this quantity turns out to be a small so this we set to 0 similarly $\theta_1 h^2$ will set it to 0 and here H_0 is large quantity. So, this quantity will stay they this will stay here in this one also we have to break up. So, $\theta_2 \dot{h}^3$ so I will break and write it here in this place. So, $\theta_2 \dot{h}^3$ times $\theta_2 \dot{h}^3$ and then $n h^3$ ok. So, similarly this term this is 0 this particular term this term will stay.

So, those you can see that this n^2 we are not neglecting why because this is not a variable term, your variable terms are $\theta_1 \theta_2 \theta_3 h^1 h^2$ all those things not the n term neither the H_0 term ok. So therefore, if we rearrange the equation so this will be $I_1 \theta_1 \ddot{\theta}_1$ and then we are start collecting the terms related to θ_1 . So, there after the $\theta_1 \dot{\theta}_1$ term we will collect here; so $\theta_1 \dot{\theta}_1$ it appears $\theta_1 \dot{\theta}_1$ term is not here. So, we have the θ_1 term is there so θ_1 term will collect. So, this is your n^2 minus $n^2 \theta_1 \dot{\theta}_1$ and this is minus sign here so that gets it to plus sign $n^2 \theta_1 I_2$ minus I_3 .

So, we will take it this gets the plus sign and then from this place we have then this term plus $3 n^2 \theta_1 \dot{\theta}_1$ and outside the bracket we have I_2 minus I_3 and this will turn up with a plus sign here in this place and somewhere. So, rest we have the θ_1 term available here the θ_1 term is one more term is in this place. So, this is, so will put it together $n^2 \theta_1 H_0$ ok, then the $\theta_3 \dot{\theta}_3$ term which are present here that we will collect, this one.

So, we get the terms like we have the minus sign if we keep it outside, so this becomes I_1 times $n^2 \theta_3 \dot{\theta}_3$ and then from this place we have $\theta_3 \dot{\theta}_3$ term. So, minus minus that makes it plus so plus and minus sign we take it outside. So, this will come with a minus sign I_2 minus I_3 times $n^2 \theta_3 \dot{\theta}_3$ and then we have $\theta_3 \dot{\theta}_3$ and $\theta_3 \dot{\theta}_3$ is also here, so this comes with a minus H_0 because this is plus here H_0 times $\theta_3 \dot{\theta}_3$ $\theta_3 \dot{\theta}_3$. So, this way we have to rearrange the terms.

So, we have taken care of the following terms, we have use this term and $n^2 \theta_1 H_0$ we have used this we have used this, this one we have used this also we have used and this also we have used. So, we are left only with $h^1 \dot{\theta}_1$ this term is already 0 this part this one we are left with this part is not included because they are 0. So, we are left with plus $h^1 \dot{\theta}_1$ minus $n^2 h^3$ and this equal to 0. So we need to rewrite this equation in a compact format, so we will do it on the next page.

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$$I_1 \ddot{\theta}_1 + [4n^2(I_2 - I_3) + nH_0] \theta_1 - [(I_1 - (I_2 - I_3))n - H_0] \dot{\theta}_3 + \dot{h}_1 - n h_3 = 0 \quad \text{--- (A)}$$

$$I_2 \dot{\omega}_2 - (I_3 - I_1) \omega_3 \omega_1 + \dot{h}_2 + \omega_3 h_1 - \omega_1 h_3 = -3n^2(I_3 - I_1)(-\dot{\theta}_2)$$

$$I_2 \ddot{\theta}_2 - (I_3 - I_1)(\dot{\theta}_3 + n\theta_1)(\dot{\theta}_1 - n\theta_3) + \dot{h}_2 + (\dot{\theta}_3 + n\theta_1)h_1 - (\dot{\theta}_1 - n\theta_3)h_3 - 3n^2(I_3 - I_1)\theta_2 = 0$$

$$I_2 \ddot{\theta}_2 - 3n^2(I_3 - I_1)\theta_2 + \dot{h}_2 = 0 \quad \text{--- (B)}$$

Pitfalls

So, the first term is $I_1 \ddot{\theta}_1$ will have to go back and look into all these equations, this term we will take it outside the n a square term from this place and then write as this basically becomes $4n^2(I_2 - I_3)\theta_1$, so θ_1 we can take it outside ok. So, $4n^2(I_2 - I_3)\theta_1$ so plus $4n^2(I_2 - I_3)\theta_1$ minus $(I_1 - (I_2 - I_3))n\dot{\theta}_3$ plus $H_0\dot{\theta}_3$ plus $\dot{h}_1 - n h_3 = 0$.

So, this is the second term and then the third term we pick up from this place $\dot{\theta}_3$ we can flatly take it outside and inside we have $(I_1 - n\theta_3)$ so this term we can combine together. So, that will give me $(I_1 - n\theta_3)(\dot{\theta}_3 + n\theta_1)$ and then minus h_3 plus $(\dot{\theta}_3 + n\theta_1)h_1 - (\dot{\theta}_1 - n\theta_3)h_3 - 3n^2(I_3 - I_1)\theta_2 = 0$.

So this constitutes our equation for the related to θ_1 ok, the same way we have to write for the other one also ok. So, this equation is fine, now similarly we pick up the other also. So, $I_2 \ddot{\theta}_2$ if you follow this notation and expand and work like this, so the you can derive all this things this is the circular equation we have written earlier $\dot{h}_2 + \omega_3 h_1 - \omega_1 h_3$ this equal to $-3n^2(I_3 - I_1)\dot{\theta}_2$. So, same way insert, I will take some shortcut step and leave it to you to work out this things. So, \dot{h}_2 will be $\dot{\theta}_2$ double dot minus $n\dot{\theta}_2$. So, $n\dot{\theta}_2$ term will become 0 so this gets lost from this place.

So, we just get here $I_2 \ddot{\theta}_2$ and then of course we have the other terms $\dot{\theta}_3 + n \theta_1$ and this is $\dot{\theta}_1 - n \theta_3 + h_2 \dot{\theta}_3 + \omega_3 \theta_3 + n \theta_1 + h_1 \dot{\theta}_1 - \omega_1 \theta_1 - n \theta_3$ and then multiplied by $h_3 + 3n a^2$ and this is θ_2 .

So, minus minus that gets plus so we will have a minus sign here in this place and this will be equal to 0. If you have any extra moment like the magnetic moment, so will remove this we will simply put here the magnetic M_{magnetic} plus $M_{\text{aerodynamic}}$ and so on and this also you need to linearize, but what function they will appear it depends on that, so you need to rewrite in this way ok.

But for as for as the gyrostats are concerned, so here in this case the gravity gradient obviously they will appear and we are these terms will act as the actuating term, while you we try to do carry out the control ok. But currently we are going to write in this way whatever is written here so if we rearrange it ok, so I hope that you will be able to do the rearrangement I am skipping those steps and follow the approximation we have done this here the variable term $\theta_3 + h_2$ and so on those terms will be 0.

So, those kind of terms you can delete so if you do that, so this will get reduced to $-3n a^2 I_3 \ddot{\theta}_2 + h_2 \dot{\theta}_2$. So, this is your equation number b so this is related to your pitch dynamics ok, the first one was this one is related to the roll dynamics this is related to the pitch, in the same way the third equation can also be worked out.

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$$I_3 \dot{\omega}_3 - \omega_1 \omega_2 (I_1 - I_2) + \dot{h}_3 + \omega_1 (h_2 - H_0) - \omega_2 h_1 = 0$$

$$I_3 (\dot{\theta}_3 + n \dot{\theta}_1) - (\dot{\theta}_1 - n \dot{\theta}_3) (\theta_2 - n) (I_1 - I_2) + \dot{h}_3 + (\dot{\theta}_1 - n \dot{\theta}_3) (h_2 - H_0) - (\theta_2 - n) h_1 = 0$$

$$I_3 \ddot{\theta}_3 - [n^2 (I_1 - I_2) - n H_0] \theta_3 + \{2 \dot{\theta}_1 (I_1 - I_2) n - H_0\} \dot{\theta}_3 + n h_1 = 0$$

$J_1 \equiv I_1$
 $J_2 \equiv I_2$
 $J_3 \equiv I_3$
 ~~I_1, I_2, I_3~~

So, the third equation is $I_3 \dot{\omega}_3 - \omega_1 \omega_2 (I_1 - I_2) + \dot{h}_3 + \omega_1 (h_2 - H_0) - \omega_2 h_1 = 0$ and then we have $I_1 - I_2$ always right like this. So, that it is convenient to work with h_3 dot and then ok. So, for in this equation the other terms also we have to write. So, those terms here $\omega_1 h_2 - H_0 - \omega_2 h_1$ and on the right hand side we have the gravity term.

So, the gravity term we need to write which is $-3n^2 (I_1 - I_2)$ and then this is multiplied by 0, so this equal to 0. So, right hand side here in this case it become 0. So, with this simplification so this term here it is a getting out ok, so rest we need to insert the values for.

So, here this will be θ_3 dot plus n times θ_1 dot, then ω_1 we are replacing by θ_1 dot minus n times θ_3 and this is θ_2 dot minus $n (I_1 - I_2)$ plus plus h_3 dot plus ω_1 is θ_1 dot minus n times θ_3 times $h_2 - H_0$ minus n times h_1 this equal to 0. So, this is the equation we get here in this case.

So if we again expand it and rewrite this will get reduced to θ_3 double dot plus n times $I_1 - I_2$ or $I_1 - I_2 - I_3$ this multiplied by $n - H_0$ plus h_3 dot plus $n h_1$ which is the last term here this and this will be equal to 0 ok. So, usually ones you are writing this equation so many of the books they will write it this way, the minus sign will taken out of this and here it will be made as a plus sign ok.

So, instead of using here like the minus sign if you write in terms of I_1 minus I_3 so the this gets in terms of a plus sign. So, these are the some of the common changes it is a done, so what you can do that I_2 this is I_2 ok. We are started with somewhere $J_1 J_2 J_3$, but we have ultimately converts to $I_1 I_2 I_3$, now I cannot change it because I forgot while writing ok.

So, there is no way of rewriting all those things like here we were writing in terms of $J_2 J_3$, so for I will mention here explicitly that J_1 is identical to I_1 J_2 is identical to I_2 and J_3 is identical to I_3 for the wheels you can use the notation like $I_w1 I_w2 I_w3$, so this is your the third equation ok.

So this is the way we get all the linearized equation and this linearized equations are done for the local control not for the global control. So, will continue in the next lecture so we have finished the Gyrostat and something I wanted to cover I told you that in the moment angular momentum term, the last term there was perhaps I have included that in my lecture or not I have done that or I do not remember that.

So therefore, I will include that as a either as a supplementary material or either I will give as the assignment, so that once the solution to the assignment comes you can look into that solution. So, next time we are going to a start with the control moment Gyros, so here reaction wheels a in the further gyrostats this reaction wheals are being used for controlling the satellite.

Similarly the control movement gyros can be used to control the satellite and they have their own adventures, so if you so we are going to discuss that in the next lecture not today, because it will take time we will continue in the next lecture.

Thank you very much for listening.