

Instability & Patterning of Thin Polymer Films

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Spontaneous Instability & Dewetting of Thin Polymer Film-V

Welcome back, we will continue our discussion on the linear stability analysis, which we were performing for trying to understand the Spontaneous Instability of an ultra thin liquid film.

(Refer Slide Time: 00:34)

$$\frac{\partial h}{\partial t} - \frac{h^2}{\mu} P_x h_x - \frac{1}{3\mu} h^3 P_{xx} = 0.$$
$$\Rightarrow \frac{\partial h}{\partial t} - \frac{1}{3\mu} [3h^2 P_x h_x + h^3 P_{xx}] = 0.$$
$$\Rightarrow \frac{\partial h}{\partial t} - \frac{1}{3\mu} (h^3 P_x)_x = 0. \quad \leftarrow \text{Conservative Form.}$$
$$P = p + \phi \quad \leftarrow \text{Interfacial Interaction.}$$

↑ Laplace Pressure.

You, may recall that in the previous class, we reached up to we were doing the derivations. So, we were looking at the order of magnitude analysis of the governing equation and incorporating the appropriate conditions, which include the kinematic boundary condition and other conditions that we have been looking in, so we have reached up to this stage; so this is a quick recap I would like to do.

(Refer Slide Time: 00:52)

Eqn. of Continuity : $\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$.

X-Comp. N.S. : $\rho \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + w \frac{\partial u}{\partial z} \right) = - \frac{\partial p}{\partial x} - \frac{\partial \phi}{\partial x} + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial z^2} \right)$

Z-Comp. N.S. : $\rho \left(\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + w \frac{\partial w}{\partial z} \right) = - \frac{\partial p}{\partial z} - \frac{\partial \phi}{\partial z} + \mu \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial z^2} \right)$

$\Delta p = \gamma h_{xx}$

$\frac{\partial h}{\partial t} + u_s \frac{\partial h}{\partial x} = w_s$

$(h_t + u_s h_x = w_s)$
Kinematic Boundary Condition.
Combines u_s and w_s

Hydrodynamics of a Free Liquid Interface of a Thin Film

So, we started off with the continuity equation and the **x and y component**, x and z component Navier-Stokes equation understanding or plugging in our concept of a fluctuating interface instead of a completely flat interface. And we also derive two classes before the condition of the kinematic boundary condition, which **which** takes care of the surface fluctuations are non zero interfacial velocities.

And once we started looking into, so these are the set of equations that we have looked into, continuity the x and z component Navier-Stokes equation along with the the Young-Laplace equation for an axis symmetric surface. Simplified for the long wave approximation and this is the kinematic boundary condition, we started to do an order of magnitude analysis; we just discussed briefly what an order of magnitude analysis is.

(Refer Slide Time: 01:46)

Order of Magnitude Analysis

Entire Zone over which the film is coated: (L) .

Expanses of $z \rightarrow (0, h)$. $h \rightarrow$ Film thk.

$h \ll L$ Film is few (tens) of nm thick
 Film is cast over few cm^2 area.

$o(x) \sim L$
 $o(z) \sim h$

Let $o(u) \sim u$.
 $o(x) \sim L$
 $o(z) \sim h$

Continuity Eqn:
 $\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$

$\frac{o(u)}{o(x)} \sim \frac{o(w)}{o(z)}$

Adrian Bejan
Boundary Layers.
 Boundary Layers: $\frac{\partial^2 u}{\partial x^2} \sim 0$
 X-Component P.N.S Eqn. Within a Boundary Layer.
 Boundary Layer Approximation
 Order of Magnitude Analysis

Direct consequence of Mass balance.
 No term can be neglected.

And that eventually showed us which are the relevant and which are the non relevant terms.

(Refer Slide Time: 01:59)

$o(u) \sim u$, $o(w) \sim \epsilon \cdot u$ \Rightarrow $o(u) \sim 1$, $o(w) \sim \epsilon$.

$o(x) \sim L$, $o(h) \sim h$ \Rightarrow $o(z) \rightarrow 1$, $o(x) \sim \epsilon^{-1}$.

$o(t) \sim \epsilon^{-1}$

X-Component Navier Stokes Equation:-

$$\rho \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + w \frac{\partial u}{\partial z} \right) = - \frac{\partial p}{\partial x} - \frac{\partial \phi}{\partial x} + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

$\frac{1}{\epsilon} \cdot \frac{1}{\epsilon} \cdot \frac{1}{\epsilon} \cdot \frac{1}{\epsilon} \cdot \frac{1}{\epsilon^{-1}} \cdot \frac{1}{\epsilon^2}$

$\Rightarrow \frac{\partial p}{\partial x} + \frac{\partial \phi}{\partial x} = \mu \frac{\partial^2 u}{\partial z^2}$

$P = p + \phi$

$\frac{\partial P}{\partial x} = \mu \frac{\partial^2 u}{\partial z^2}$

It is a Pseudo Steady State Equation, as u itself is function of time.

And finally, this is the form of the final governing equation, which we obtained from the x component navier stokes equation.

(Refer Slide Time: 02:18)

z-Component Navier Stokes Equation.

$$\rho \left(\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + w \frac{\partial w}{\partial z} \right) = - \frac{\partial p}{\partial z} + \mu \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial z^2} \right)$$

$\frac{\rho}{\epsilon^2}$ $1 \cdot \frac{\rho}{\epsilon^2}$ $\frac{\rho}{\epsilon^2}$ $\frac{\rho}{\epsilon^2}$ $\frac{\rho}{\epsilon^2}$

$$\Rightarrow \frac{dp}{dz} = 0$$

$P \neq f(z) \Rightarrow$ So ~~is~~ No distribution of P across the film in z direction.

$$\frac{\partial^2 w}{\partial x^2} \quad \frac{\partial}{\partial x} \left(\frac{\partial w}{\partial x} \right)$$

$$\frac{1}{\epsilon^2} \left(\frac{\epsilon}{\epsilon} \right)$$

We also obtained $\frac{dp}{dz} = 0$, p is the non gravitational pressure $\frac{dp}{dz}$ is equal to 0 from the z component of navier stokes equation.

(Refer Slide Time: 02:25)

Simplified X-Component Navier Stokes Equation.

$$\mu \frac{\partial^2 u}{\partial z^2} = \frac{\partial p}{\partial x}$$

$$\mu \frac{\partial u}{\partial z} = P_x z + C_1$$

B.C.1 \rightarrow The Zero Shear Boundary Condition at $z=h$, $\mu \frac{\partial u}{\partial z} = 0$.

$$C_1 = -P_x h$$

$$\mu \frac{\partial u}{\partial z} = P_x (z-h)$$

$$u = P_x \left(\frac{z^2}{2} - zh \right) + C_2$$

$$u = P_x \left(\frac{z^2}{2} - zh \right)$$

Consequences of $\frac{\partial p}{\partial z} = 0$ is.

~~$h = f(x,t)$~~ but $h \neq f(z)$

$h \neq f(z)$ $h \neq f(z)$

Invoke the No Slip B.C. at $z=0$, $u=0$

$C_2 = 0$ | $\text{Film-Substrate interface.}$

And then we started to work with the governing equation for the system started to integrate it with appropriate boundary conditions.

(Refer Slide Time: 02:39)

$$\frac{\partial h}{\partial t} - \frac{h^2}{\mu} p_x h_x - \frac{1}{3\mu} h^3 p_{xx} = 0.$$

$$\Rightarrow \frac{\partial h}{\partial t} - \frac{1}{3\mu} [3h^2 p_x h_x + h^3 p_{xx}] = 0.$$

$$\Rightarrow \boxed{\frac{\partial h}{\partial t} - \frac{1}{3\mu} (h^3 p_x)_x} = 0. \quad \leftarrow \text{Conservative Form.}$$

$p = \underbrace{p}_{\substack{\uparrow \\ \text{Laplace Pressure}}} + \underbrace{\phi}_{\leftarrow \text{Interfacial Interaction}}$
 Liquid surface

① Film exposed to Atm
 ② Film Surface Perfectly Flat. $p_B = p_L$

And which has finally, laid us to this particular point, which gives us $\frac{\partial h}{\partial t}$ is equal to $\frac{1}{3\mu} h^3 p_{xx}$ in the conservative form.

We also understand the p is a function of pressure plus ϕ . Now, this pressure if we are considering the liquid surface had the film in perfectly flat, the pressure right at the surface on the liquid side p_l or p_s or whatever you want to write and let us say this is the p outside or p_b . So, had this film been (No audio from 3:29 to 3:38) and (No audio from 3:40 to 3:48) perfectly flat, then we know that the surface been mechanical equilibrium, then p_b would have been equal to p_l .

But now that we understand that we have surface fluctuations (No audio from 04:02 to 04:12), which means that the surface is no longer flat therefore, p_b is not equal to p_l anymore. In fact p_b , let us draw it separately.

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$\frac{\partial h}{\partial t} - \frac{1}{3\mu} (h^3 p_x)_x = 0$
 $P = p + \Phi$
 $p_s = p|_{z=h} = p_b - \gamma h x x$
 $\therefore p_x = \frac{\partial}{\partial x} (p_b - \gamma h x x)$
 $p_x = -\gamma h x x x$

\circledast p_b and p_s are inter-related
 thru' the Young-Laplace Equation,
 $p_b = 1 \text{ atm} = \text{Constant}$.
 For the present situation, where small slope approximation is valid ($h x = 0$)
 $\rightarrow \Delta p = (p_b - p_s) = \gamma h x x$.
 $\Delta p = \gamma \left[\frac{h x}{x(1+h x^2)^{3/2}} + \frac{h x x}{(1+h x^2)^{3/2}} \right]$
 nature of instability is long wave $\Rightarrow h \gg x$ $h x \approx 0$

So, this is the situation we have, this is the equation which we have derived up to this point, anyone who has a confusion about the origin of this equation or joining late please refer to the previous couple of lectures, which gives you a very clear idea about how this equation comes.

Now, we are do that P is equal to or we understand P is equal to p plus π , we are now looking at this p at the interface, so over here. So, let us say that, this is p_s and this is p_b . Since the liquid is not flat, the film surface is not flat therefore, p_b is not equal to p_s and p_b and p_s are interrelated through the young Laplace equation.

If the film is exposed to atmosphere, then of course, p_b is equal to 1 atmosphere and is equal to constant. So, what we have for the situation (No audio from 06:12 to 06:22), where a small slope approximation is valid that is $h x$ is equal to 0, we have Δp which is p_b minus p_s in this is equal to $\gamma h x x$, this is the convention, so p_b minus p_s , so do not confuse the signs.

So, it remains like this therefore, it **it** gives us p_b equal to $\gamma h x x$, let me just quickly remind that for an axis symmetric surface, this is the complete expression for the young Laplace equation. And if we assume that the nature of instability is long wave (No audio from 07:04 to 07:42), that is h is much larger than x , then of course, one gets each x is close to 0 and therefore, once you substitute that you get to this form of the young Laplace equation.

Now, what we get is p_s is equal to essentially p evaluated at z is equal to h and which is p_b minus $\gamma h \times x$ therefore, p_s p_x if we differentiate it, so this is essentially you are looking at $\frac{d}{dx} (p_b - \gamma h x)$, p_b is constant, so what you are left with is minus $\gamma h \times x$.

Similarly, so this is one important parameter, now why we are looking into it is essentially we need to find out an expression for p_x in this expression (Refer Slide Time: 08:53) and we know p is equal to small p that is the pressure the plus π . So, we need to essentially, find out independently p_x and π and that precisely, what we are doing and in doing, so you see that, we now have an expression for p_x .

(Refer Slide Time: 09:27)

$\phi =$ Interfacial Potential.

$\Delta G = \frac{A}{12\pi h^2}$

$\phi = \frac{\partial(\Delta G)}{\partial h} = \frac{A}{6\pi h^3}$

↑ Potential and in N-S/Eqns like Navier Stokes or NS Gravity and/or other body forces.

↑ This Expression Considers ONLY the attractive van der Waals Interaction.

At this length scale (~ 100 nm), Gravity and other body forces can be neglected.

In reality, for an unstable film ϕ is made up of antagonistic interactions, with different rates of decay.

Two major components, for a general dielectric film longer range interfacial vdw interaction.

Now, what is π ? π is the essentially it is the interfacial potential and which we have seen that considering the x based on the excess interfacial potential and from an expression of $\frac{d}{dx} \Delta G$ is equal to a minus A divide by $12 \pi h^2$, which comes from the when considering the interfacial Van der Waals interaction, we have already have obtained an expression of π , which is $6 \pi h^3$.

But these expression, please remember it comes from the only from the attractive Van der Waals interaction, so typically this π is the potential and in Navier Stokes equation it includes gravity or let us gravity and other body forces are neglected or I will say that at this length scale. So, **let it** let me put it like this for simplicity, that at this length scale,

which is of the order of roughly 100 nanometer, we have already argued that gravity other body forces can be neglected.

Of course, your talking of a situation, where you do not apply any external imposed electric or magnetic field and that is the reason, that they do not show up as the body forces. But, in cases where **you you can** you can apply essentially or in principle an electric field or a magnetic field to a thin film to restabilize it, I think we will take it up in one of the last lectures.

So, that is what is the situation, where the instability is triggered by the application of an external field rather than the spontaneous instability, that we are talking here, the only laviting thing about this particular expression though we will continue our discussion with this expression is that, this considers this expression considers only the attractive Van der Waals interaction.

A morph a rather, but in **in** reality **for a** for an unstable film pi is made up of antagonistic interactions with different rates of decay, two major components as we have already talked for a general dielectric film are the longer range interfacial Van der Waals interaction (No audio from 14:02 to 14:15). And rather short range satiric repulsion which any way we have talked about the hot c r model and the contact repulsion, because of the overlap of electron charge clouds, etcetera.

So, this is in essentially a satiric, so essentially the molecules are coming in contact with each other and therefore, manifests in the repulsion. So, these are the two general terms, which are most popular **in a** in a general dielectric film.

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A popular representation of ϕ for an unstructured, thin liquid film that can be used rather well even for a polymer film (in liquid form, that is heated beyond T_g / exposed to its solvent vapor), is given as,

$$\phi = \left(\frac{A_s}{6\pi h^3} \right) - \left(\frac{S_p}{L_p} \right) \exp\left(-\frac{h}{L_p}\right) + \left(\frac{B}{h^9} \right)$$

$A_s \Rightarrow$ Effective Hamaker constant.

$S_p \Rightarrow$ Denotes the strength of any medium or short range interaction; it is attractive when ($S_p < 0$) and repulsive, when ($S_p > 0$)

$L_p \rightarrow$ ~~Excess~~ Represents the corresponding decay length. \ast To remove any NON physical singularity in the event ($S_p \rightarrow 0$)

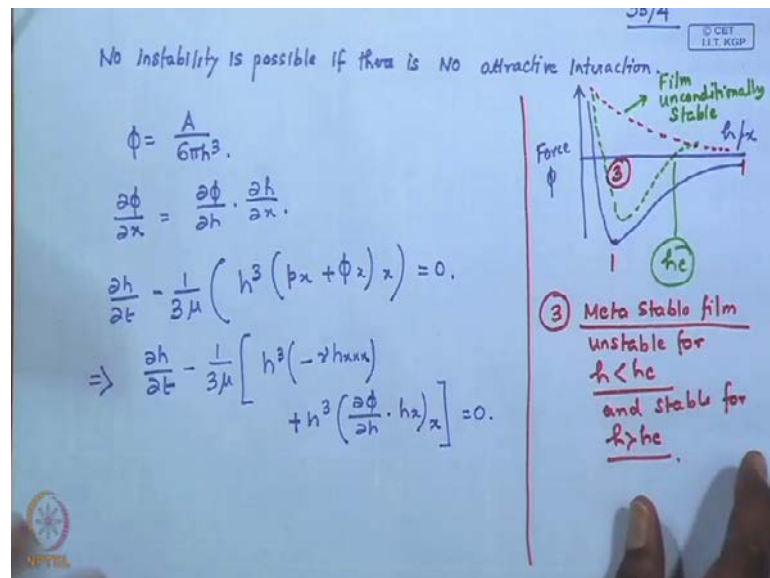
This term accounts for the polar interactions/entropic confinement effects in a polymer.

A popular representation of ϕ (No audio from 15:03 to 15:18) for an unstructured thin liquid film that, can be used rather well even for a polymer film in liquid form that is heated beyond T_g or exposed to its solvent vapor is given as ϕ is equal to A_s . So, we just write A_s for the effective hamaker constant for the system which we already know (No audio from 16:44 to 16:54).

Now, this term you can immediately see that, this term is the corresponds to the interfacial Van der Waals term. So, A_s is the effective hamaker constant (No audio from 17:12 to 17:24), S_p denotes the strength of medium or short range interaction with and it is **it it** denotes any medium or short range interaction it is attractive, when S_p is less than 0. Because S_p is less than 0 because; so and repulsive, when S_p is greater than 0 and L_p represents the corresponding decay length.

This terms sort of accounts for the A_b type interaction or the polar interaction, so it is this term for the polar interaction as well as the any entropic confinement effects (No audio from 19:38 to 19:48) **in** in a polymer. So, this third term is rather interesting this is more of an artificial term and particularly included for simulation, which is present to remove any non physical singularity in the event S_p tents to 0 that is, there is no repulsive term present in the system.

(Refer Slide Time: 21:34)



Because as we have already talked about that under the hydrodynamic frame work, no study of wetting or rewetting is possible until and unless there is a short range repulsion or repulsive terms are present. So, in the event there are no repulsive terms present in your system physically, you cannot run your simulations based on the hydrodynamic frame work or based on the way, we are performing the analysis that is considering the navier stokes equation to be the governing equation.

So, you need to have sort of something is a non physical singularity a very local which sort of is (()) to a local contact repulsion or something like that, that term has to be present. Of course, one has to understand, that no study of instability is possible if there is no attractive interaction or in other words no not only study, but no instability (No audio from 21:40 to 21:57). So, this is the you may want to recall that if **if** plot delta g verses the force potential verses h of the separation distance or x whatever, this is the type of a film which is going to be unstable.

So, this **this** part of the system is rep is due to the attractive interaction, in case there is no attraction there is repulsion all the way, you will get a curve like this which will represent the film to be unconditionally stable at all conditions (No audio from 22:35 to 22:45). And this is a typical curve for a meta stable film, where one can say that, this is a critical thickness corresponding to that meta stable film, where the film is. So, the third curve represents the curve of a meta stable film, which is unstable for and stable for h greater than h c.

(Refer Slide Time: 26:31) So, that expression of p_x we already have which we will simply plug this one in and of course, the expression of p_x is here (No audio from 26:30 to 26:47) and finally, what we have is it is if we write this equation in a little compact form what we will get is h_t , where as I have mentioned previously also a suffix refers to differentiation, so $\frac{dh}{dt}$ is essentially h_t (No audio from 27:23 to 27:37).

So, if h_t is equal to 0, then one gets a steady state solution; however, we know that h is a function of h_x right and which is essentially a non uniform steady state and as it is not flat which originates from the origin is the interfacial fluctuations. So, this is essentially a fourth order non-linear P D E and it might have infinite number of it **it it** actually has infinite number of steady state solutions, so any h is essentially a solution for this if the if h_t is equal to 0.

So, essentially since h is equal to h_x which is the surface is not flat, so it is essentially a quasi a steady state solution is a trivial solution **(())** here, it is a quasi steady state situation. Now, one of the major utilities of this particular equation is to test numerically whether a film of initial thickness h_0 remains stable or becomes unstable and ruptures with time.

(Refer Slide Time: 30:08) So, in the previous class or couple of classes before we had shown a video of a spontaneous rupture of a film, so I just try to replay it, so this is what you are talking about, so what we have done or what we would like to test that by means of spin coating. So, we **we** you have created a film which has a thickness of h_0 and qualitatively, we already know several factors that if a film is a thinner than the chances of the possibility of instability is higher, because the interfacial there are two interfaces will be closer to each other therefore, the magnitude of the interfacial attraction will be stronger, etcetera, etcetera.

But, here this equation gives us the opportunity to quantify that and in terms, so essentially one can use this equation to test whether a film of initial thickness h_0 remains stable with time or not. So, essentially what is done to do that is the tick is the film the **the** initial height h_0 is sort of perturbed with a function; if the function of f_x and t and let us say the perturbation amplitude is epsilon. So, therefore, h becomes h at any given instance of or rather let me put it, $h_x t$ becomes h_0 plus epsilon into $f_x t$ and we neglect any possible **(())** terms.

So, essentially we try to find the stability of the solution by try to check the stability of the thickness of the film by giving a small fluctuation, around h is equal to h_0 and this perturbation amplitude is sort of a **ma gives** gives us the extent of how the film, how to what extent the film thickness deviates from its equilibrium thickness h_0 . So, what we can do is h becomes h_0 plus $\epsilon f(x,t)$ which is linearised of h around h_0 using the simple Taylor series expansion and therefore, if we now plug in this value of h into the equation here.

So, now h **zero** is essentially a constant and what you have is ϵ and f is a ϵ is also a constant, so f is a function of x and t .

(Refer Slide Time: 33:17)

$$f_t - \frac{1}{3\mu} \left[(-2f_{xxx} + \left(\frac{\partial\phi}{\partial h}\right) f_x) h_0^3 \right] x = 0.$$

$$h = h_0 + \epsilon f(x,t)$$

$$\frac{\partial h}{\partial t} = \frac{\partial}{\partial t} [\dots]$$

$$= \epsilon \cdot \frac{\partial f}{\partial t}$$

$$\frac{\partial h_0}{\partial t} = 0$$

$$h_x = \epsilon f_x$$

$$h_{xx} = \epsilon f_{xx}$$

$$h_{xxx} = \epsilon f_{xxx}$$

$$\frac{\partial^2 \phi}{\partial x^2} = \epsilon \frac{\partial^2 \phi}{\partial x^2}$$

$$h^3 = [h_0 + \epsilon f(x,t)]^3$$

$$= h_0^3 + 3h_0^2 \epsilon f(x,t) + 3h_0 \epsilon^2 f(x,t)^2 + \epsilon^3 f(x,t)^3$$

$\epsilon =$ itself is a small perturbation
 Neglect H.O. Terms.

$\phi_h =$ Non linear function of h .
 $= \phi|_{h_0} + \frac{\partial\phi}{\partial h}|_{h_0} (h_0 - h) + \dots$

So, this equation now in the linearised domain transforms to (No audio from 33:20 to 33:42), so you can see that a mechanically all the terms containing h have, now been substituted with f for **it** it is very simple essential **if you** if you just want me to go into little deeper a little step by step just to clear your doubts. What we have is h is equal to h_0 plus $\epsilon f(x,t)$, so $\frac{\partial h}{\partial t} \frac{\partial}{\partial t}$ of this whole thing and what you was since h_0 is constant, so $\frac{\partial h_0}{\partial t}$ is equal to 0, so you are left with $\epsilon \frac{\partial f}{\partial t}$.

Similarly, if you perform let us say a **tom like** you take a tom like $h \times x \times x$, so you have h is equal to h_0 plus $\epsilon f(x,t)$ you take $h \times x$; so what you get is $\epsilon f \times x$, because $\frac{\partial h_0}{\partial x}$ again is equal to 0, $h \times x \times x$ you get $\epsilon f \times x \times h \times x \times x$ you get $\epsilon f \times x \times x$ or in

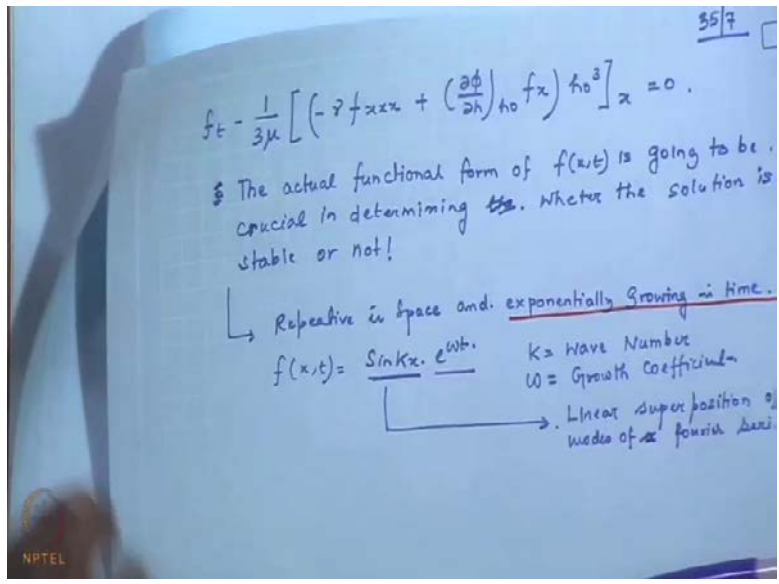
other words del three h del x cube here, which is written in a compact form as h x x x is epsilon del f 3 del x t, so the, that is essentially del 3 f del x t.

So, that is how you convert this equation into this equation, in terms of f h into an equation in terms of f, one might argue what about h cube, well you can write h is equal to h 0 plus epsilon f x t, then h cube becomes this whole thing cube and. So, its essentially h 0 cube plus epsilon f x t epsilon square plus epsilon f x t square plus f x t plus, so it is epsilon into epsilon square, then epsilon cube **I am sorry I am sorry** for this expression.

So, it is h 0 cube plus h 0 square 3 (()) factor is there epsilon f x t plus 3 h 0 epsilon square f x t square plus epsilon cube f x t cube

Now, epsilon itself is a small perturbation therefore, all these terms tent to 0, so that is how you essentially get this h cube over here gets replaced with h 0 cube the only other thing is pi h is a non-linear function of h. We which if we expand, which you can write as a pi h h 0 plus del 2 pi del h square even (()) as h 0 into h 0 minus h square into epsilon f and so on.

(Refer Slide Time: 37:58)



So, if you neglect all the high higher order terms, then you can get pi h is equal to pi h 0 as well and therefore, you get to the final equation which is, let us write it again which is f t minus 1 3 rd mu gamma (No audio from 38:04 to 38:17).

Now, one can understand that the function $f(x, t)$, the actual functional form (No audio from 38:24 to 38:40) is going to be crucial in determining, the whether the solution is stable or not. And therefore, we need to choose an appropriate perturbation function which can sort of test the stability of a film the logic here, very simply put is that you take a pick up a or choose a function, which sort of can have the maximum destabilizing influence on the **on the on the** stability of a film.

So, idea is that if any film is stable against the worst type of a perturbation function worst **in the** in the sense that it has the maximum potential to damage or **or** destabilize the film, then for any other type of perturbation or fluctuation the film will definitely be stable or let me put it again.

So, you pick up a perturbation function f , which is a function of x and t we **(())** in such a fashion that **it** it is going to be most difficult in terms of the stability of a film, so if it destabilizes the film it is perfectly fine. So, in real setting the film is likely to destabilize there are possibilities that it might not destabilize, because the function we are going to choose the functional form **(())** again qualitatively discussed is such.

But if a film is found to be stable against this perturbation function, we are speaking up then the logic is that this is the worst type of worse possible destabilization that is **that is** possible at the interface, but since it can sustain or withstand this this type of a perturbation and it is going to be stable against in any other form of perturbation because which is going to be mild.

So, this is what you known as the concept of linear stability analysis and is routinely used in various branches of science and engineering, it is a very standard mathematical procedure, **which, why**, what linear stability analysis, because what you are doing is that you are taking a non-linear differential equation. And your linearizing it with a perturbation function around a mean film thickness h_0 or **or** any mean solution for that matter to be general to put it in general terms and then checking it is stability.

So, what we do we pick up a perturbation function which is repetitive in space and exponential in time this is the type of a perturbation function, we pick up; let us say the functional form we take is $f(x, t) = \sin Kx e^{\omega t}$. So, essentially this $\sin Kx$ is repetitive in space and K corresponds to different wave number, $e^{\omega t}$ takes care of the exponentially growing with time part of the perturbation

function. So, K is the wave number, ω is the growth coefficient and K can have all $(())$ from 0 to infinity, so essentially it is a linear super position of all modes of a furious series (No audio from 42:47 to 43:06).

(Refer Slide Time: 43:17)

35/7

$$f_t - \frac{1}{3\mu} \left[-\gamma f_{xxxx} + \left(\frac{\partial \phi}{\partial h} \right) h_0 f_x \right] h_0^3 = 0.$$

‡ The actual functional form of $f(x,t)$ is going to be crucial in determining whether the solution is stable or not!

↳ Repeated in space and exponentially growing in time.

$$f(x,t) = \sin kx \cdot e^{\omega t}$$

$k =$ Wave Number
 $\omega =$ Growth Coefficient

↳ Linear superposition of all modes of a Fourier series.

↳ Growth of the amplitude is only possible when $\omega > 0$

So, considering this functional form or corresponding to this functional form of (No audio from 43:17 to 43:45) this is the equation like to have it in place, so based on this, what we can find out is our f_t is equal to (No audio from 43:57 to 44:05) and (No audio from 44:07 to 44:32) now this is simple mathematics you can just find out up to the $\frac{\partial^4 f}{\partial x^4}$ because you will be $(())$ you already have a $x x x$ and another $(())$, so we reached up to this particular term.

So, this now also what you can do is that now that everything has been sort of linearised you can sort of subsequently work on this expression, so this now becomes γf_{xxxx} . And so, $\frac{\partial \phi}{\partial h} h_0 f_x$ into h_0^3 is equal to 0, because this is now a constant now, it is no longer a function of x because you have evaluated that at h is equal to h_0 .

So, once you have these expression so, out of these expression you will essentially be needing these three terms this one, this one and this one (Refer Slide Time: 45:50), which eventually will substitute here here and here (Refer Slide Time: 45:55). So, once you do that what you get is $\omega \sin K x e^{\omega t} - \frac{1}{3\mu} \gamma K^4 \sin K x e^{\omega t} + \frac{\pi h_0}{3\mu} \omega \sin K x e^{\omega t}$

minus **sorry** minus will come here, it is there minus $k^2 \sin Kx e$ to the power ωt h^3 is equal to 0.

So, from this step to this step it looks a little biggish, but really does not matter all what we have done we have substituted $f(t)$, we have substituted $f(x)$ and we have substituted $f(x)$. So, if you do that, what comes out is $\sin Kx e$ to the power ωt sort of you can cancel out from both the sides and what you are left with is (No audio from 47:19 to 47:39).

Therefore, now if we use the expression of π is equal to A divide by $6\pi h^3$ considering attractive Van der Waals interaction, we can calculate the πh^3 is equal to minus A divided by $2\pi h^3$ to the power 4. So, if we plug in that expression, what we are left with is ω is equal to h^3 by 3μ into A divided by $2\pi h^3$ to the power 4 K^2 minus γK to the power 4.

Now, this is what is known as the characteristic equation and this is also very interesting see, we have taken the form the functional form of the perturbation equation to be (Refer Slide Time: 48:43) $\sin Kx$ into e to the power ωt now this; so what is this? This is the surface fluctuation of the perturbation you have taken.

Now, in order for the film to become unstable as we have discussed in some of our previous classes that the what has to happen is that this interfacial fluctuations should grow and then the amplitude of the qualitatively this we have discussed. So, it becomes possible only when this interfacial fluctuations grow and sort of the amplitude of the growing fluctuations match that of the film thickness, then only one can argue that the film has ruptured.

(Refer Slide Time: 49:33) So, from this perturbation function a growth of this amplitude is only possible. So, the amplitude, the growth of the amplitude (No audio from 49:38 to 49:52), when ω is greater than 0, if ω is less than 0, then what is going to happen that with time, this term is going to tend towards 0 and the perturbation is going to die down.

In physical terms what; that means, is that we know that these fluctuations are always opposed by surface tension, so in that case physically a negative ω would mean that the strength of your attractive Van der Waals interaction or the destabilizing force to be

more general was not strong enough to overcome the stabilizing influence of surface tension.

(Refer Slide Time: 50:35)

$f(x,t) = \sin kx \cdot e^{i\omega t}$
 $f_t = \omega \sin kx \cdot e^{i\omega t}$
 $f_x = k \cos kx \cdot e^{i\omega t}$
 $f_{xx} = -k^2 \sin kx \cdot e^{i\omega t}$
 $f_{xxx} = -k^3 \cos kx \cdot e^{i\omega t}$
 $f_{xxxx} = k^4 \sin kx \cdot e^{i\omega t}$

$f_t - \frac{1}{3\mu} \left[-\gamma f_{xxxx} + \left(\frac{\partial \phi}{\partial x} \right)_{h_0} f_x \right] h_0^3 = 0$
 $f_t - \frac{1}{3\mu} \left[-\gamma f_{xxxx} + \phi_{h_0} f_x \right] h_0^3 = 0$

$\omega \sin kx \cdot e^{i\omega t} - \frac{1}{3\mu} \left[-\gamma k^4 \sin kx \cdot e^{i\omega t} + \phi_{h_0} (-k^2 \sin kx \cdot e^{i\omega t}) \right] h_0^3 = 0$
 $\omega - \frac{h_0^3}{3\mu} \left[-\gamma k^4 + \phi_{h_0} (-k^2) \right] = 0$
 $\Rightarrow \omega = \frac{h_0^3}{3\mu} \left[\frac{A}{2\pi h_0^4} k^2 - \gamma k^4 \right]$

Characteristic Eqn

Therefore, from this using this perturbation function the film can only become unstable the condition of instability of a film, now turns out to be or let us use a fresh sheet (No audio from 50:45 to 51:04), now based on the concept, we discussed here film can only become unstable (Refer Slide Time: 51:12), (No audio from 51:12 to 51:23), when omega is greater than 0 right.

(Refer Slide Time: 50:50)

$\omega = \frac{h_0^3}{3\mu} \left[\frac{A}{2\pi h_0^4} k^2 - \gamma k^4 \right]$

$h_0 = \text{Film thickness}$
 $\mu = \text{viscosity}$
 $k = k^2, k^4 \Rightarrow \text{Potl Positive}$

$\gamma = \text{Surface Tension}$
 Positive Qty.

$\gamma = \text{Negative}$

$\frac{A}{2\pi h_0^4} k^2 = \text{Destabilizing term}$
 Are always positive.

Only way ω can be Positive. \Rightarrow 1st term has to be positive $\Rightarrow \omega$ can be positive.

Condition of film instability based on attractive VdW interaction is $A > 0$.

$A < 0$ | Film is unconditionally Stable.

\Rightarrow Viscosity only can influence the dynamics but cannot influence the stability of the system.

Therefore here also let us now examine the expression of ω carefully you see, h_0 is a film thickness μ is the viscosity, so these two are always positive; so therefore, this prefactor $h_0^3 / 3\mu$ is always positive.

Now, there is also another interesting thing that is hidden here, which we will discuss later K we know is any real number or K is any integer, so irrespective of whether K is positive or negative both the terms are positive. Γ is surface tension it is again a positive quantity, we are talking about a film that is exposed to air, we are not talking about any interfacial tension and we have always argued that the surface tension is always positive.

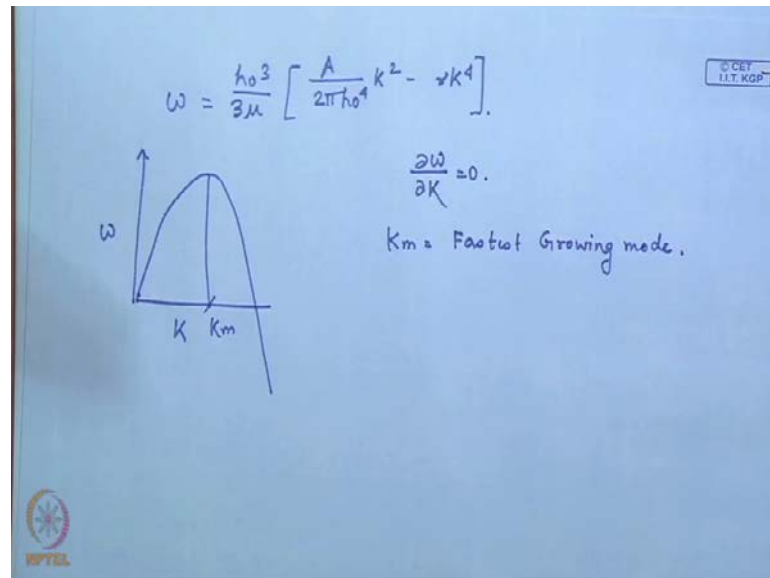
Therefore this term, since it has a negative sign is always going to be negative, this multiplied by a positive number, so this is always going to be negative K^2 is positive h_0^4 is also positive. So, the only way ω can be positive is this first term has to be positive only then this term is positive and this term is negative. So, if the magnitude of this particular term is now higher than the magnitude of this particular this the second term, then only ω can be positive

Therefore now we clearly understand the condition of film instability based on attractive Van der Waals interaction is $A > 0$, so A has to be higher than 0, this is number 1.

So, for any system where effective Hamaker constant is negative, then this term is negative this term is also negative (Refer Slide Time: 54:29) therefore, the film is unconditionally stable, further you see; so in this expression this is the potential destabilizing term, which arises from van der Waals interaction this is the stabilizing term and we have always argued that whenever you have the surface fluctuation surface tension opposes the growth.

So, here it is you can see that the term to which the surface tension is associated it is the stabilizing term, other thing is you see that the in the prefactor, viscosity is at the denominator, which means that higher is the magnitude of μ , lower will be the value of ω . But, μ **can not** influence the sign of ω that is the rheology of the system or the viscosity of the system only can influence the dynamics but, cannot influence the stability of the system, these are important findings that comes out from linear stability analysis.

(Refer Slide Time: 56:05)



The other, the only other remaining important thing is that if you now look at the expression for the characteristic equation again, you can find out the mode at which the growth is fastest by setting $\frac{\partial \omega}{\partial k} = 0$ and which gives you the fastest growing mode (No audio from 56:33 to 56:42).

So, in this class we will stop here and we will pick up from the fastest growing mode in the next class and get an expression for the instability wave length as well as the number density of the features that comes from the linear stability analysis. And then move on to some real experimental **evil** sequence of thin film dewetting, polymer thin film dewetting thank you.