

Basic Environmental Engineering and Pollution Abatement
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Lecture – 55
Tutorial 11

Hello everyone. Now, we will have a tutorial session and, in this class, will solve some numerical problems based on our discussion made in the last four classes.

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Problem 1

A country discards roughly 158 million tons of MSW. The High Heating Value of those discards is about 6,000 Btu/lb . A mass-burn waste-to-energy facility can convert those wastes to electricity with a heat rate of 17,000 Btu of thermal input per kWh of electrical output (roughly 20 percent efficiency). Estimate the electrical energy that could be produced per year if all of the discards were used in this type of WTE system. Compare it with the total energy generated, which is about $4,500 * 10^9$ kWh/yr.

Solution:

$$\text{Electrical output} = \frac{158 * 10^6 \text{ ton/yr} * 2,000 \text{ lb/ton} * 6,000 \text{ Btu/lb}}{17,000 \text{ Btu/kWh}} = 111.5 * 10^9 \text{ kWh/yr}$$

$$\text{Fraction from MSW} = \frac{111.5 * 10^9 \text{ kWh/yr}}{4,500 * 10^9 \text{ kWh/yr}} = 0.024 = 2.4\%$$



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Problem number one, the statement is a country discards roughly 158 million tons of MSW. The high heating value of those discards is about 6000 Btu/lb. A mass burn waste-to-energy facility can convert those wastes to electricity with a heat rate of 17000 Btu of thermal input per kilowatt hour of electrical output; roughly 20 % efficiency. Estimate the electrical energy that could be produced per year if all the discards were used in this type of WTE system. Compare it with the total energy generated which is about $4500 * 10^9$ kWh/yr.

So, this is the problem statement; now we have to solve. So, what we will do? We will see that what is the electrical output we can get from this waste and then total electricity production which is provided here? So, we will be take the ratio of that.

$$\text{Electrical output} = \frac{158 * 10^6 \text{ ton/yr} * 2,000 \text{ lb/ton} * 6,000 \text{ Btu/lb}}{17,000 \text{ Btu/kWh}} = 111.5 * 10^9 \text{ kWh/yr}$$

$$\text{Fraction from MSW} = \frac{111.5 * 10^9 \text{ kWh/yr}}{4,500 * 10^9 \text{ kWh/yr}} = 0.024 = 2.4\%$$

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Problem 2



Estimate the landfill area needed to handle one year's MSW for a town of 200,000 people. Assume per capita national average discards of 5 lbs per day, no combustion, a landfill density of 1,000 lb/yd³, and one 10-foot lift per year. Assume 20 percent of the cell volume is soil used for cover.

Solution:
From the data given, the landfill volume of refuse for 100,000 people would be

$$V_{MSW} = \frac{5 \text{ lbs/day-person} * 365 \text{ day/yr} * 200,000 \text{ people}}{1,000 \text{ lb/yd}^3} = 365,000 \text{ yd}^3/\text{yr}$$

Since only 80 percent of a cell is landfill, the volume of cell needed is

$$V_{cells} = \frac{365,000 \text{ yd}^3}{0.8} = 456,250 \text{ yd}^3/\text{yr}$$



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The area of lift per year at 10-ft/yr of depth is $A \times \text{lift} = V$.

$$A \text{ lift} = \frac{456,250 \text{ yd}^3/\text{yr} * 27 \text{ ft}^3/\text{yd}^3}{10 \text{ ft/yr}} = 12,31,875 \text{ ft}^2$$

The actual sizing of a landfill would include a number of additional factors, such as additional area requirements for access roads and auxiliary facilities, reduction in landfill volume as biological decomposition takes place, and increases in compaction as additional lifts are included.

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So, now we will move to problem number 2 and the statement is, estimate the landfill area needed to handle one year's MSW for a town of 2 lakhs people. Assume per capita national average discards of 5 lbs/day, no conversion. A landfill density of 1000 lb/yd³ and one 10 feet lift per year. Assume 20 % of the cell volume is soil used for cover; so this is the problem statement. So, now we have to find out the area requirement for this landfilling. So, at first we will calculate the volume of the MSW, then we will see the volume of the cells, then lift is given. So, from that we will get the value of the area requirement.

From the data given, the landfill volume of refuse for 100,000 people would be

$$V_{\text{MSW}} = \frac{5 \text{ lbs/day-person} * 365 \text{ day/yr} * 200,000 \text{ people}}{1,000 \text{ lb/yd}^3} = 365,000 \frac{\text{yd}^3}{\text{yr}}$$

Since only 80 percent of a cell is landfill, the volume of cell needed is

$$V_{\text{cell}} = \frac{365,000 \frac{\text{yd}^3}{\text{yr}}}{0.8} = 456,250 \frac{\text{yd}^3}{\text{yr}}$$

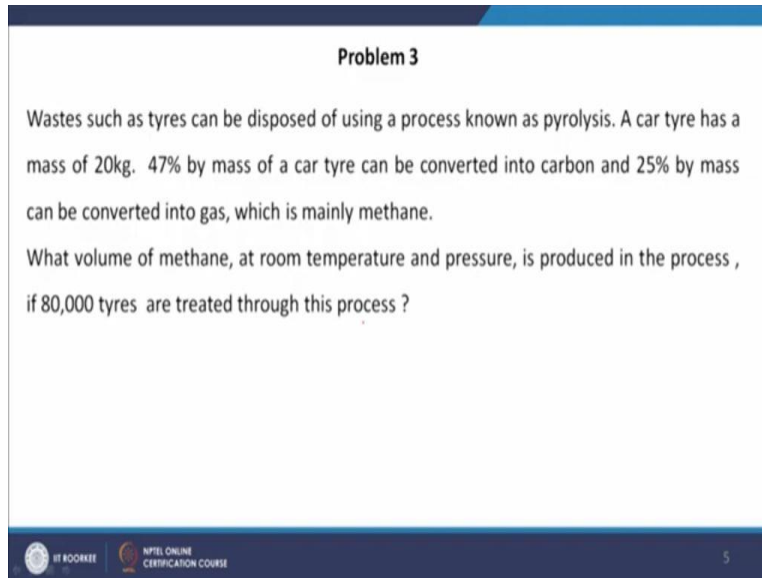
The area of lift per year at 10-ft/yr of depth is

$$A \text{ lift} = \frac{456,250 \frac{\text{yd}^3}{\text{yr}} * 27 \frac{\text{ft}^3}{\text{yd}^3}}{10 \frac{\text{ft}}{\text{yr}}} = 12,31,875 \text{ ft}^2$$

But, actually the area requirement will be more because there are some additional activities, which will be associated with the active filling.

So, the actual sizing of a landfill would include a number of additional factors such as additional area requirements for access roads and auxiliary facilities, reduction in landfill volume as biological decomposition takes place, and increases in compactions as additional lifts are included. So because of this, the actual requirement will be deferred to some extent from this one, and it will be more than this.

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Problem 3

Wastes such as tyres can be disposed of using a process known as pyrolysis. A car tyre has a mass of 20kg. 47% by mass of a car tyre can be converted into carbon and 25% by mass can be converted into gas, which is mainly methane.

What volume of methane, at room temperature and pressure, is produced in the process, if 80,000 tyres are treated through this process ?

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Now, problem number-3. The statement is, wastes such as tyres can be disposed of using a process known as pyrolysis. A car tyre has a mass of 20 kg. 47 % by mass of a car tyre can be converted into carbon and 25 % by mass can be converted into gas, which is mainly methane. What volume of methane, at room temperature and pressure is produced in the process, if 80,000 tyres are treated through this process? So, this is a problem statement of a pyrolysis process, waste tyre is converted to different pyrolysis products. And it is assumed that the gas which is produced only methane is present to make the calculation more simple.

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Solution :

Mass of 80000 tyres = $80000 * 20 * 1000 \text{ g} = 16 \times 10^8 \text{ g}$

25% of this is $25 * 16 \times 10^6 \text{ g}$ of methane

Molecular mass of methane = 16

Therefore, moles of methane = $25 * (16/16) \times 10^6 \text{ mol} = 25 \times 10^6$

1 mole occupies 22.4 dm^3 volume @ NTP


Hence volume = $22.4 * 25 \times 10^6 \text{ dm}^3 = 5.6 \times 10^8 \text{ dm}^3$

$= 5.6 \times 10^5 \text{ m}^3$

Room temperature = 30°C Volume of methane = $(303/273) * 5.6 \times 10^5 \text{ m}^3$

$= 6.215 \times 10^5 \text{ m}^3$

$\frac{P_1 V_1}{T_1} = \frac{P_2 V_2}{T_2}$



So, here we will have to do some mass balance.

$$\text{Mass of 80000 tyres} = 80000 * 20 * 1000 \text{ g} = 16 \times 10^8 \text{ g}$$

$$25\% \text{ of this is } 25 * 16 \times 10^6 \text{ g of methane}$$

$$\text{Molecular mass of methane} = 16$$

$$\text{Therefore, moles of methane} = 25 * (16/16) \times 10^6 \text{ mol} = 25 \times 10^6$$

$$1 \text{ mole occupies } 22.4 \text{ dm}^3 \text{ volume @ NTP}$$

$$\text{Hence volume} = 22.4 * 25 \times 10^6 \text{ dm}^3 = 5.6 \times 10^8 \text{ dm}^3$$

$$= 5.6 \times 10^5 \text{ m}^3$$

$$\text{Room temperature} = 30^\circ\text{C}$$

$$\text{Volume of methane} = (303/273) * 5.6 \times 10^5 \text{ m}^3$$

$$= 6.215 \times 10^5 \text{ m}^3$$

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Problem 4

In an MSW gasifier air flowrate and feed flow rate are $10\text{Nm}^3/\text{s}$ and 8 kg per second respectively. The MSW does not contain any sulphur, nitrogen and chloride. The syngas contains CO (40%) , CO_2 (2 %), H_2 (30%), CH_4 (5%) and C_2H_2 (2%). Calculate the rate of production of syngas in Nm^3/kg of MSW.

Solution

We know that under the above condition the rate of syngas production can be computed by the following equation

$$\text{Fuel gas production}(\text{Nm}^3.\text{kg}^{-1}) = \frac{\text{air flow rate} (\text{Nm}^3.\text{s}^{-1}) \times 0.79}{\left[1 - \frac{\text{CO} + \text{CO}_2 + \text{H}_2 + \text{CH}_4 + \text{C}_2\text{H}_2}{100}\right] \times \text{feeding rate}(\text{kg}.\text{s}^{-1})}$$



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Now, problem number 4. The statement is, in an MSW gasifier air flow rate and feed flow rate are $10\text{ Nm}^3/\text{s}$ and 8 kg/s respectively. The MSW does not contain any sulphur, nitrogen and chloride. The syngas contains carbon monoxide 40 %, CO_2 2 %, H_2O 30 %, CH_4 5 % and C_2H_2 2 %. Calculate the rate of production of syngas in Nm^3/kg of MSW. So again, this is another problem related to the handling of MSW through gasifier. And through the gasifier, we know that producer gas or syngas, when we use the oxygen, we get syngas; and when we use the air, we get producer gas. So this is a case of producer gas production.

Now, what we will see? This is also again, can be solved on the basis of mass balance of nitrogen.

We know that under the above condition the rate of syngas production can be computed by the following equation

$$\text{Fuel gas production} \left(\frac{\text{Nm}^3}{\text{kg}} \right) = \frac{\text{Air flow rate} \left(\frac{\text{Nm}^3}{\text{s}} \right)}{[1 - (\text{CO} + \text{CO}_2 + \text{H}_2 + \text{CH}_4 + \text{C}_2\text{H}_2)/100] \times \text{Feeding rate} \left(\frac{\text{kg}}{\text{s}} \right)}$$

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Therefore,

$$\text{Syn gas production} = \frac{[(10 \times 0.79)]}{[1 - (0.4 + 0.02 + 0.3 + 0.05 + 0.02)]} \times 8$$
$$= 7.9 / (0.21 \times 8) = 4.702 \text{ Nm}^3/\text{kg MSW}$$

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Problem 4

In an MSW gasifier air flowrate and feed flow rate are $10 \text{ Nm}^3/\text{s}$ and 8 kg per second respectively. The MSW does not contain any sulphur, nitrogen and chloride. The syngas contains CO (40%), CO_2 (2%), H_2 (30%), CH_4 (5%) and C_2H_2 (2%). Calculate the rate of production of syngas in Nm^3/kg of MSW.

Solution

We know that under the above condition the rate of syngas production can be computed by the following equation

$$\text{Fuel gas production} (\text{Nm}^3 \cdot \text{kg}^{-1}) = \frac{\text{air flow rate} (\text{Nm}^3 \cdot \text{s}^{-1}) \times 0.79}{\left[1 - \frac{\text{CO} + \text{CO}_2 + \text{H}_2 + \text{CH}_4 + \text{C}_2\text{H}_2}{100}\right] \times \text{feeding rate} (\text{kg} \cdot \text{s}^{-1})}$$


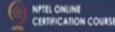
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$$\text{Syn gas production} = \frac{[(10 \times 0.79)]}{[1 - (0.4 + 0.02 + 0.3 + 0.05 + 0.02)]} \times 8$$
$$= 7.9 / (0.21 \times 8) = 4.702 \text{ Nm}^3/\text{kg MSW}$$

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Problem 5

A pyrolysis plant handles 0.5 TPD MSW and produces gas, char and liquor. Operating temperature is 788°C and pressure of the reactor is 1 atm., respectively. The gas composition (vol %) is H₂(39.10), CO(33.50), CH₄(13.10), CO₂ (14.3). The mass % of production of gas, char and oil are 35, 20 and 45 respectively. Determine the no. of moles of each component of gas produced per day.

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Next problem, statement number 5. A pyrolysis plant handles 0.5 TPD MSW and produces gas, char and liquor. Operating temperature is 788 °C and pressure of the reactor is 1 atmosphere respectively. The gas composition volume percent is H₂ (39.10), CO (33.50), CH₄ (13.10), CO₂ (14.3). The mass % of production of gas, char and oil are 35, 20 and 45 respectively. Determine the number of moles of each component of gas produced per day. So, we have to calculate the number of moles of each component of gas produced per day. So, this is a problem related to pyrolysis of MSW.

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Solution

Basis: 500 kg MSW per day



Mass of gas produced = $500 \times 0.35 = 175$ kg per day

Mass of char produced = $500 \times 0.20 = 100$ kg per day

Mass of oil produced = $500 \times 0.45 = 225$ kg per day

Avg. mol. Wt. of gas produced = $0.3910 \times 2 + 0.335 \times 28 + 0.131 \times 16 + 0.143 \times 44$
 $= 18.55$ kg per kmole

Gas produced in kmole per day = $175 \times 1 / 18.55 = 9.43$ k mole per day

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Mass of gas produced = $500 \times 0.35 = 175$ kg per day

Mass of char produced = $500 \times 0.20 = 100$ kg per day

Mass of oil produced = $500 \times 0.45 = 225$ kg per day

Avg. mol. Wt. of gas produced = $0.3910 \times 2 + 0.335 \times 28 + 0.131 \times 16 + 0.143 \times 44$
= 18.55 kg per kmole

Gas produced in kmole per day = $175 \times 1 / 18.55 = 9.43$ k mole per day

So, this is the gas production per day.

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On mole basis
Hydrogen produced = $9.43 \times 39.10 / 100 = 3.69$ k mole per day
CO produced = $9.43 \times 33.50 / 100 = 3.16$ k mole per day
Methane produced = $9.43 \times 13.10 / 100 = 1.24$ k mole per day
CO₂ produced = $9.43 \times 14.3 / 100 = 1.35$ k mole per day

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Now, we have to calculate individual gas molecules production per day.

On mole basis

Hydrogen produced = $9.43 \times 39.10 / 100 = 3.69$ k mole per day

CO produced = $9.43 \times 33.50 / 100 = 3.16$ k mole per day

Methane produced = $9.43 \times 13.10 / 100 = 1.24$ k mole per day



CO₂ produced = $9.43 \times 14.3 / 100 = 1.35$ k mole per day

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Problem 6

A dry MSW has the following composition on mass basis:

C: 40 (%), H: 5 %, O: 30 % and Ash:25 %. Determine the stoichiometric oxygen requirement for the combustion of the MSW. Assume the ash as inert and average molecular weight of ash is 56. If the ratio of nitrogen to oxygen in air is 4:1 (v/v), determine the stoichiometric requirement of air.

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Now, we will move to the next problem, problem number 6. The statement is a dry MSW has the following composition on mass basis; carbon 40 %, hydrogen 5 %, oxygen 30 %, ash 25 %. Determine the stoichiometric oxygen requirement for the combustion of the MSW. Assume the ash as inert and average molecular weight of ash is 56. If the ratio of nitrogen to oxygen in air is 4:1 volume by volume ratio; determine the stoichiometric requirement of air. So, this problem is basically related to the incineration of MSW; so we have to calculate the stoichiometric requirement of air.

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Basis : 100 g dry MSW ✓

C = 40 g = $40/12 = 3.33$ moles
H = 5 g = $5/1 = 5$ moles
O = 30 g = $30/16 = 1.875$ moles
Ash = 25 g = $25/56 = 0.4464$ moles

Average Molecular formula of the MSW
 $C_{3.33}H_5O_{1.875}Ash_{0.4464}$

Since the ash is inert the combustion reaction will be as follows:

$C_aH_bO_cAsh_g + d O_2 = e H_2O + f CO_2 + g Ash$ Where a = 3.33, b = 5, c = 1.875

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Basis : 100 g dry MSW

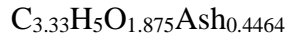
$$C = 40 \text{ g} = 40/12 = 3.33 \text{ moles}$$

$$H = 5 \text{ g} = 5/1 = 5 \text{ moles}$$

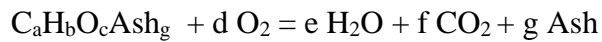
$$O = 30 \text{ g} = 30/16 = 1.875 \text{ moles}$$

$$\text{Ash} = 25 \text{ g} = 25/56 = 0.4464 \text{ moles}$$

Average Molecular formula of the MSW



Since the ash is inert the combustion reaction will be as follows:



Where $a = 3.33$, $b = 5$, $c = 1.875$

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By mass balance of the components $C_aH_bO_c + d O_2 = e H_2O + f CO_2$

$C_{3.33}H_5O_{1.875}\text{Ash}_{0.4464}$

$a=f$ (C balance)
 $b = 2e$ (H balance)
 $c + 2d = e + 2f$ (O balance)

Therefore
 $a = f = 3.33$,
 $b = 5$
 $e = b/2 = 5/2 = 2.5$
 $c = 1.875$

Therefore for 100 g of MSW O_2 requirement =
 $3.6425 * 32 = 116.56 \text{ g}$

Stoichiometric requirement of O_2 is 116.56 g per
100 g of MSW Or 1.1656 g O_2 per g of MSW

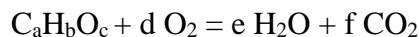
N_2 in the air containing 3.6425 mole $O_2 = 4 * 3.6425 =$
14.57 mole; Mass of $N_2 = 14.57 * 28 = 407.96 \text{ g}$

Or $2d = 2.5 + 6.66 - 1.875$
 $= 7.285$
 $d = 3.6425$

Therefore mass of air = $407.96 + 116.56 = 524.52 \text{ g}$

Stoichiometric requirement of air = 524.52 g per 100 g of MSW

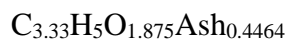
By mass balance of the components



$$a=f \text{ (C balance)}$$

$$b = 2e \text{ (H balance)}$$

$$c + 2d = e + 2f \text{ (O balance)}$$



Therefore

$$a = f = 3.33,$$

$$b = 5$$

$$e = b/2 = 5/2 = 2.5$$

$$c = 1.875$$

$$1.875 + 2d = 2.5 + 2 \times 3.33$$

$$\text{Or } 2d = 2.5 + 6.66 - 1.875$$

$$= 7.285$$

$$d = 3.6425$$

Therefore for 100 g of MSW O_2 requirement = $3.6425 \times 32 = 116.56$ g

Stoichiometric requirement of O_2 is 116.56 g per 100 g of MSW

Or 1.1656 g O_2 per g of MSW

N_2 in the air containing 3.6425 mole $O_2 = 4 \times 3.6425 = 14.57$ mole;

Mass of $N_2 = 14.57 \times 28 = 407.96$ g

Therefore mass of air = $407.96 + 116.56 = 524.52$ g

Stoichiometric requirement of air = 524.52 g per 100 g of MSW

So, now we are able to solve the problem and we have seen the stoichiometric requirement of air.

So, now we have solved all our problems and thank you for your patience.