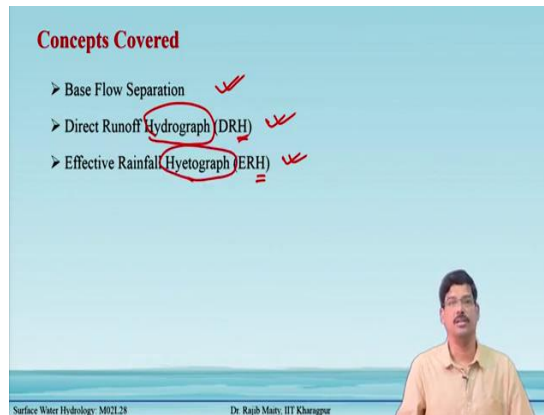


**Surface Water Hydrology**  
**Professor Rajib Maity**  
**Department of Civil Engineering**  
**Indian Institute of Technology, Kharagpur**  
**Lecture – 28**  
**Base Flow Separation, DRH and ERH**

In today's particular lecture we are considering the base flow separation DRH and ERH.

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The three major things we will learn in this first one is base flow separation second one is direct runoff hydrograph which is abbreviated as DRH and the last one is effective rainfall hydrograph which is ERH.

(Refer Slide Time: 01:27)



The outline of this lecture goes like this the introduction to the base flow and there are different methods of the base floor separation will be discussed three methods, straight-line method, two

lines method and curve extension method. Then we will discuss the direct runoff hydrograph and its properties and its relation with this effective rainfall hyetograph there are some examples of problems that will be taken up and then a summary.

(Refer Slide Time: 01:56)

**Introduction to Base Flow**

- The runoff resulting from a rainfall comprises of different components, such as surface runoff, subsurface runoff, base flow etc.
- In general, the runoff is contributed from two major components, namely quick flow and base flow.
- The quick flow such as surface flow or interflow, responds quickly to rainfall events, whereas, in case of base flow, for which main source is ground water, a slow response is observed.
- Base flow is zero for ephemeral and intermittent rivers and non-zero for perennial rivers.
- Base flow investigation helps to estimate groundwater recharge, variation in groundwater storage and water management. It is important for maintaining environmental flow in a stream.

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## Introduction to Base Flow

Now, runoff resulting from rainfall comprises different components such as surface runoff subsurface and base flow. In general, this runoff is contributed from two major components, one is the quick flow another one is the base flow. Quick flow comes relatively faster at the outlet base flow takes a longer time.

The quick flow such as surface flow or interflow, responds quickly to rainfall events, whereas, in the case of base flow, for which the main source is groundwater, a slow response is observed. Baseflow is zero for ephemeral and intermittent rivers and non-zero for perennial rivers.

The ephemeral and intermittent rivers do not flow continuously throughout the year whereas perennial rivers flow is available throughout the year. That means the base flow is non-zero for the perennial rivers but for the ephemeral and intermittent rivers where it goes to zero sometime in the year. So, we can say that base flow is zero.

Baseflow investigation helps to estimate the groundwater recharge in the inter catchment and the variation of the groundwater storage how it varies for the different seasons and it helps for the water management also. Secondly, it also helps to maintain the environmental flow in the stream and the importance of the environmental flow in a stream.

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### Separation of Base Flow


Base flow separation is also applied to explore the hydrological processes of a catchment. For instance, it is used in hydrograph analysis, to study the excess rainfall and its corresponding runoff from a catchment.

- A separation of base flow from the flood hydrograph is needed to get the direct contribution from the surface flow/flood runoff, also known as Direct Runoff (DR).
- There are three main methods for base flow separation as follows:

Straight Line Method

Two Lines Method

Curve Extension Method



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## Separation of Base Flow

Baseflow separation is also applied to explore the hydrological processes of a catchment. For instance, it is used in hydrograph analysis, to study the excess rainfall and its corresponding runoff from a catchment.

Separation of base flow from the flood hydrograph is needed to get the direct contribution from the surface flow/flood runoff, also known as Direct Runoff (DR).

There are three main methods for baseflow separation as follows:


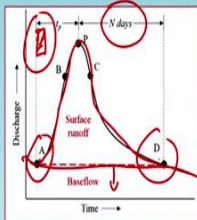
- I. Straight Line Method
- II. Two Lines Method
- III. Curve Extension Method

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### Separation of Base Flow

#### Straight Line Method

- The base flow separation is achieved by joining the starting point of the rising limb (point A) and the end point of the recession limb (point D), by a straight line.
- It is usually easy to mark point A by eye judgement, whereas marking of point D is difficult.
- The approximate position of point D is achieved by an empirical equation as follows:  $N = 0.83A^{0.2}$  where  $N$  is in days and  $A$  is the drainage area in  $km^2$ .



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## Straight Line Method

In the straight-line method, the base flow separation is achieved in this method by joining the starting point of the hydrograph or the starting point of the rising limb that points A and the ending point of the recession limb that is point D shown in fig.1. The starting point of rising limb A and ending of the recession limb that is D, which is again identification of these two points make also some difficulties.

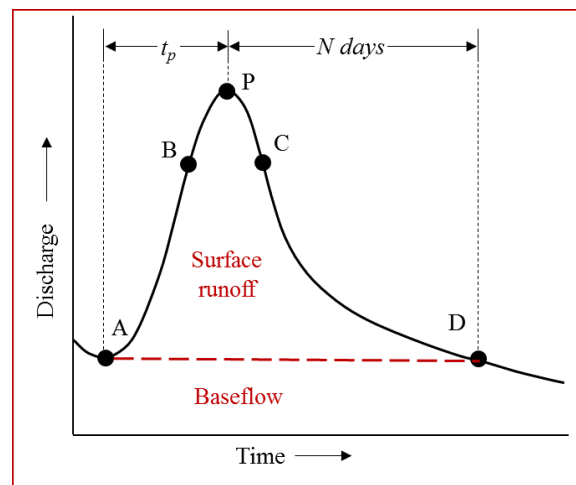


Fig.1 shows the straight-line method of base flow separation

Point A can be identified easily but sometimes it is difficult to identify where point D is and where we can say that, okay the effect of rainfall has stopped and it is now your leak coming from the groundwater contribution that is as a base flow.

The approximate position of point D is achieved by an empirical equation as follows:

$$N = 0.83A^{0.2}$$

Where N is in days and A is the drainage area in  $\text{km}^2$

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**Separation of Base Flow**

**Two Line Method**

- In this method, the separation of base flow is performed with the help of two lines AE and ED as shown in the figure.
- The line AE is obtained by extending the base flow recession curve MA (recession curve before the commencement of the surface runoff) upto the ordinate of the peak discharge (point P).
- Point D is obtained using the same formula as discussed in straight line method, and thereafter, the lines AE and ED are joined to separate the base flow.

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## Two Line Method

In this method, the separation of base flow is performed with the help of two lines AE and ED as shown in fig.2. The line AE is obtained by extending the base flow recession curve MA (recession curve before the commencement of the surface runoff) up to the ordinate of the peak discharge (point P). Point D is obtained using the same formula as discussed in the straight-line method, and thereafter, the lines AE and ED are joined to separate the base flow.

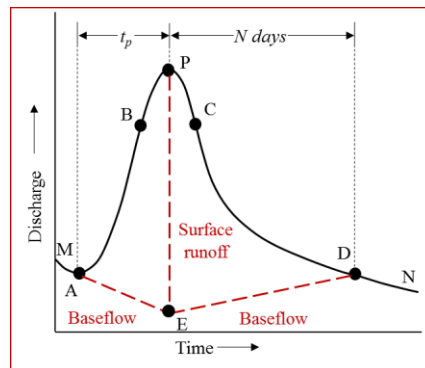


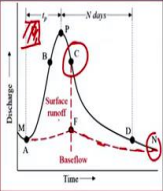
Fig.2 shows the two-line method of base flow separation

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**Separation of Base Flow**

**Curve Extension Method**

- This procedure for separation of base flow starts by drawing an arbitrary smooth curve, i.e., extension of the MA curve till it intersects the ordinate of point of inflection (C) at point F.
- Thereafter, a curve between F and N is drawn by extending it backward from N to F. Thus, the two segments marked by the curves AF and FN demarcate the base flow and surface/direct runoff.
- This method is applicable in a region where the groundwater contributions are significant and reaches the stream quickly.



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## Curve Extension Method

This procedure for separation of base flow starts by drawing an arbitrary smooth curve, i.e., an extension of the MA curve till it intersects the ordinate of point of inflection (C) at point F as shown in fig.3.

Thereafter, a curve between F and N is drawn by extending it backward from N to F. Thus, the two segments marked by the curves AF and FN demarcate the base flow and surface/direct runoff. This method is applicable in a region where the groundwater contributions are significant and reach the stream quickly.

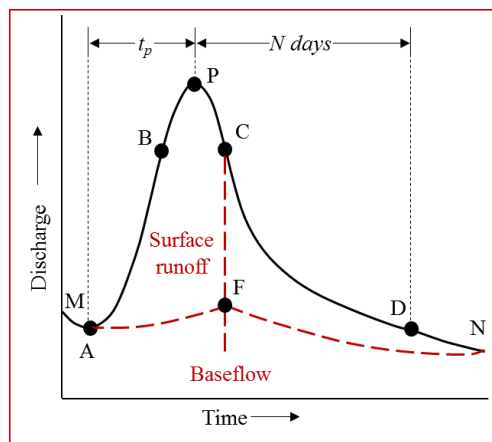


Fig.3 shows the curve extension method of base flow separation

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**Separation of Base Flow**

- The demarcations, obtained by various methods, separating the base flow and Direct Runoff (DR), i.e., either the straight line AD or the curves denoted by AED or AFN may not always represent the actual site condition.
- However, since the contribution of groundwater flow is very small as compared to the total flow volume, these methods are usually justified for obtaining Direct Runoff Hydrograph (DRH).

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The demarcations, obtained by various methods, separating the base flow and Direct Runoff (DR), i.e., either the straight line AD or the curves denoted by AED or AFN may not always represent the actual site condition.

However, since the contribution of groundwater flow is very small as compared to the total flow volume, these methods are usually justified for obtaining a Direct Runoff Hydrograph (DRH).

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**Direct Runoff Hydrograph (DRH)**

- After the separation of base flow from the storm hydrograph, the resulting hydrograph is known as a **Direct Runoff Hydrograph (DRH)**.
- The area under the DRH is known as **direct runoff volume**.
- By knowing the catchment area, direct runoff can also be expressed in terms of depth.

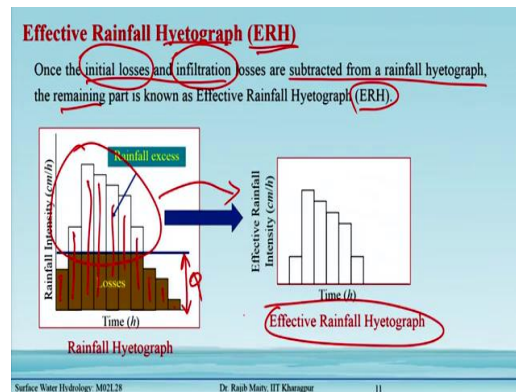
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## Direct Runoff Hydrograph (DRH)

After the separation of base flow from the storm hydrograph, the resulting hydrograph is known as a Direct Runoff Hydrograph (DRH). So, the total area under the DRH is indicating that how much total volume of the runoff has come out from the basin due to a storm that is what is called the direct runoff volume.

The direct runoff can also be expressed in terms of depth. If the volume is divided by the area that gets in terms of the depth also. So, runoff sometime is expressed in terms of depth as the rainfall is also expressed in terms of depth.

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## Effective Rainfall Hyetograph (ERH)

There are two such losses with respect to the runoff one is the initial loss other one is the infiltration loss. If these two things are subtracted from the rainfall hyetograph then the remaining part is known as the ERH is an effective rainfall hyetograph.

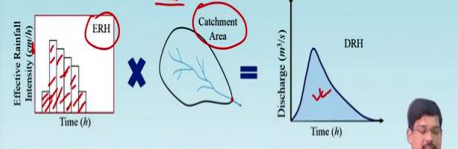
Sometimes we considered there is a constant loss in terms of the phi index or W index. So, once this rainfall hyetograph is obtained, separate the initial loss and infiltration loss which is through this sometimes the phi index, and then this remaining part is called the effective rainfall hyetograph.



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**DRH vs ERH**

- Total volume of DRH and ERH are same. However, these are expressed in different units. Hence, proper care is to be taken during calculation (example follows).
- Generally, the ordinate of DRH (instantaneous values) are in  $m^3/s$  and the ordinates of ERH (height of bars) are in  $cm/h$ .



Area of ERH multiplied by the catchment area is equal to the total area of DRH (area below the curve).

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## DRH vs ERH

The total volume of DRH and ERH are the same. However, these are expressed in different units. Hence, proper care is to be taken during calculation (example follows).

Generally, the ordinate of DRH (instantaneous values) are in  $m^3/s$  and the ordinates of ERH (height of bars) are in  $cm/h$ . The area of ERH multiplied by the catchment area is equal to the total area of DRH (area below the curve).

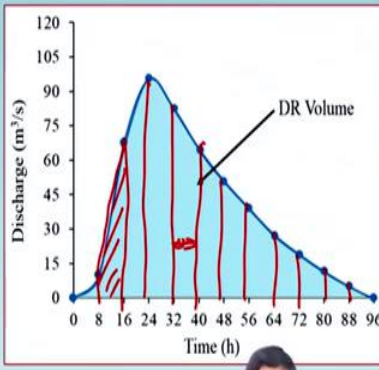
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**DRH vs ERH**

- Direct Runoff (DR) volume can be calculated with the help of the following expression

$$\text{DR Volume} = \text{Total Area under the DRH} \times \text{Area of the basin}$$

- We usually follow trapezoidal rule to compute the total area under the DRH.



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Direct Runoff (DR) volume can be calculated with the help of the following expression

$$\text{DR Volume} = \text{Total Area under the DRH} \times \text{Area of the basin}$$

We usually follow the trapezoidal rule to compute the total area under the DRH. And for that one calculation, it becomes much simpler that we can just take the ordinates at different time instances and we only add them up and then we can multiply with the time gap between two successive ordinates.

(Refer Slide Time: 19:02)

**Example 28.1:**

Rainfall hyetograph for a 3-h storm over a catchment of  $46 \text{ km}^2$  area is provided below. Area under the resulting DRH, i.e., total volume of direct runoff, is  $1.5 \text{ Mm}^3$ .

| Time spell (h) | 1 <sup>st</sup> hour | 2 <sup>nd</sup> hour | 3 <sup>rd</sup> hour |
|----------------|----------------------|----------------------|----------------------|
| Rainfall (mm)  | 20                   | 17                   | 10                   |

Find out the Effective Rainfall Hyetograph (ERH).

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**Example 28.1:**

Rainfall hyetograph for a 3-h storm over a catchment of  $46 \text{ km}^2$  area is provided below. The area under the resulting DRH, i.e., the total volume of direct runoff, is  $1.5 \text{ Mm}^3$ .

| Time spell (h) | 1 <sup>st</sup> hour | 2 <sup>nd</sup> hour | 3 <sup>rd</sup> hour |
|----------------|----------------------|----------------------|----------------------|
| Rainfall (mm)  | 20                   | 17                   | 10                   |

Find out the Effective Rainfall Hyetograph (ERH).

(Refer Slide Time: 19:53)

**Solution**

- First, we need to calculate the  $\phi$ -index.

Given:

Total volume of direct runoff =  $1.5 \text{ Mm}^3 = 1.5 \times 10^6 \text{ m}^3$

Area of the catchment =  $46 \text{ km}^2 = 46 \times 10^6 \text{ m}^2$


Rainfall duration =  $3 \text{ h}$

Total rainfall in  $3 \text{ h} = (20 + 17 + 10) = 47 \text{ mm} = 4.7 \text{ cm}$

So,

Runoff depth =  $\frac{1.5 \times 10^6}{46 \times 10^6} = 0.033 \text{ m} = 3.3 \text{ cm}$

$\phi$ -index =  $\frac{4.7 - 3.3}{3} = 0.47 \text{ cm/h}$



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## Solution

First, we need to calculate the  $\phi$ -index.

Given:

$$\text{Total volume of direct runoff} = 1.5 \text{ Mm}^3 = 1.5 \times 10^6 \text{ m}^3$$

$$\text{Area of the catchment} = 46 \text{ km}^2 = 46 \times 10^6 \text{ m}^2$$

$$\text{Rainfall duration} = 3 \text{ h}$$

$$\text{Total rainfall in } 3 \text{ h} = (20 + 17 + 10) = 47 \text{ mm} = 4.7 \text{ cm}$$

So,

$$\text{Runoff depth} = \frac{1.5 \times 10^6}{46 \times 10^6} = 0.033 \text{ m} = 3.3 \text{ cm}$$

$$\phi\text{-index} = \frac{4.7 - 3.3}{3} = 0.47 \text{ cm/h}$$

(Refer Slide Time: 21:10)

**Solution**

- The effective rainfall hyetograph for each time spell is calculated as shown in the table.

| Time spell (h)       | Rainfall (cm) | $\phi$ -index (cm/h) | Effective rainfall [C2-C3] (cm) | Effective rainfall intensity [C4/C1] (cm/h) |
|----------------------|---------------|----------------------|---------------------------------|---|
| C1                   | C2            | C3                   | C4                              | C5  |
| 1 <sup>st</sup> hour | 2.0           | 0.47                 | 1.53                            | 1.53  |
| 2 <sup>nd</sup> hour | 1.7           | 0.47                 | 1.23                            | 1.23  |
| 3 <sup>rd</sup> hour | 1.0           | 0.47                 | 0.53                            | 0.53  |

**Effective Rainfall Hyetograph**

- The corresponding effective rainfall hyetograph is also drawn and is shown in the figure.

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The effective rainfall hyetograph for each time spell is calculated as shown in the table.

| Time spell (h)       | Rainfall (cm) | $\phi$ -index (cm/h) | Effective rainfall [C2-C3] (cm) | Effective rainfall intensity [C4/C1] (cm/h) |
|----------------------|---------------|----------------------|---------------------------------|---|
| C1                   | C2            | C3                   | C4                              | C5  |
| 1 <sup>st</sup> hour | 2.0           | 0.47                 | 1.53                            | 1.53  |
| 2 <sup>nd</sup> hour | 1.7           | 0.47                 | 1.23                            | 1.23  |
| 3 <sup>rd</sup> hour | 1.0           | 0.47                 | 0.53                            | 0.53  |

The corresponding effective rainfall hyetograph is also drawn and is shown in figure 4.

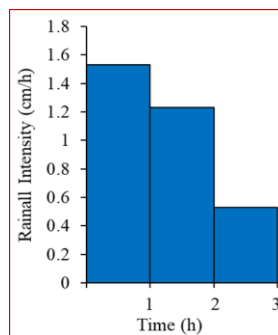


Fig.4 shows the ERH of example 28.1

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**Example 28.2:**

Rainfall magnitudes of 4.2 cm and 2.2 cm have occurred in two successive 3-h durations on a watershed of area 32 km<sup>2</sup>. The following hydrograph is produced at the outlet of the basin.

|                                   |    |   |    |    |    |    |    |    |    |    |    |     |     |
|-----------------------------------|----|---|----|----|----|----|----|----|----|----|----|-----|-----|
| Time from start of rainfall (h)   | -5 | 0 | 5  | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50  | 55  |
| Observed flow (m <sup>3</sup> /s) | 8  | 7 | 15 | 28 | 23 | 18 | 14 | 11 | 9  | 7  | 6  | 5.5 | 5.5 |

Estimate the Effective Rainfall Hyetograph (ERH) and  $\phi$ -index.

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### Example 28.2:

Rainfall magnitudes of 4.2 cm and 2.2 cm have occurred in two successive 3-h durations on a watershed of area 32 km<sup>2</sup>. The following hydrograph is produced at the outlet of the basin.

|                                   |    |   |    |    |    |    |    |    |    |    |    |     |     |
|-----------------------------------|----|---|----|----|----|----|----|----|----|----|----|-----|-----|
| Time from start of rainfall (h)   | -5 | 0 | 5  | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50  | 55  |
| Observed flow (m <sup>3</sup> /s) | 8  | 7 | 15 | 28 | 23 | 18 | 14 | 11 | 9  | 7  | 6  | 5.5 | 5.5 |

Estimate the Effective Rainfall Hyetograph (ERH) and  $\phi$ -index.

(Refer Slide Time: 23:27)

**Solution**

- The flood hydrograph is drawn as per the given ordinates.
- The base flow is separated by straight line method, joining starting and ending points. Starting point is identified by eye estimation and the end point is identified using the equation  $N = 0.83 A^{0.2}$  as explained before.
- The ordinates of base flow are obtained at the same time intervals.

Discharge (m<sup>3</sup>/s)

Time (h)

$N = 0.83 A^{0.2}$   
 $= 0.83 \times (32)^{0.2}$   
 $= 1.66 \text{ days} \cong 40 \text{ h}$

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### Solution

The flood hydrograph is drawn as per the given ordinates shown in fig.5.

The base flow is separated by the straight-line method, joining starting and ending points. The starting point is identified by eye estimation and the endpoint is identified using the equation  $N=0.8 A^{0.2}$  as explained before.

The ordinates of baseflow are obtained at the same time intervals.

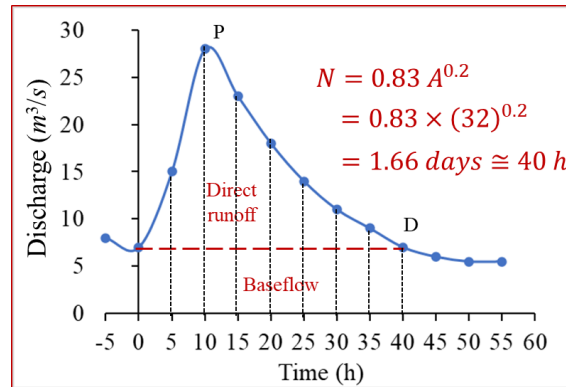


Fig.5 shows the flood hydrograph of example 28.2

(Refer Slide Time: 24:12)

**Solution**

| Time (h) | Observed flow (m <sup>3</sup> /s) | Base flow (m <sup>3</sup> /s) | Direct Runoff Hydrograph (m <sup>3</sup> /s) |
|----------|-----------------------------------|-------------------------------|--|
| -5       | 8                                 | --                            | --   |
| 0        | 7                                 | 7                             | 0  |
| 5        | 15                                | 7                             | 8  |
| 10       | 28                                | 7                             | 21   |
| 15       | 23                                | 7                             | 16   |
| 20       | 18                                | 7                             | 11   |
| 25       | 14                                | 7                             | 7  |
| 30       | 11                                | 7                             | 4  |
| 35       | 9                                 | 7                             | 2  |
| 40       | 7                                 | 7                             | 0  |
| 45       | 6                                 | → 6 →                         | --   |
| 50       | 5.5                               | 5.5                           | --   |
| 55       | 5.5                               | 5.5                           | --   |

Summation of all the ordinates of Direct Runoff Hydrograph ( $\sum Q$ ) = 69

- From the Table we can calculate the ordinates of Direct Runoff Hydrograph (DRH).  
 $DR = \text{Observed flow} - \text{Base flow}$
- With the help of the formula  

$$\text{Depth of DR} = \frac{(\sum Q) \times t \times 60 \times 60}{A \times 10^6}$$

$$= \frac{(69) \times 5 \times 60 \times 60}{32 \times 10^6}$$

$$= 0.0388 \text{ m} = 3.88 \text{ cm}$$

| Time (h)  | Observed flow (m <sup>3</sup> /s) | Base flow (m <sup>3</sup> /s) | Direct Runoff Hydrograph (m <sup>3</sup> /s) |
|---|-----------------------------------|-------------------------------|--|
| -5  | 8                                 | --                            | --   |
| 0   | 7                                 | 7                             | 0  |
| 5   | 15                                | 7                             | 8  |
| 10  | 28                                | 7                             | 21   |
| 15  | 23                                | 7                             | 16   |
| 20  | 18                                | 7                             | 11   |
| 25  | 14                                | 7                             | 7  |
| 30  | 11                                | 7                             | 4  |
| 35  | 9                                 | 7                             | 2  |
| 40  | 7                                 | 7                             | 0  |
| 45  | 6                                 | 7                             | --   |
| 50  | 5.5                               | 7                             | --   |
| 55  | 5.5                               | 7                             | --   |
| Summation of all the ordinates of Direct Runoff Hydrograph ( $\sum Q$ ) |                                   |                               | 69   |

- From the Table we can calculate the ordinates of Direct Runoff Hydrograph (DRH).

DR = Observed flow – Base flow

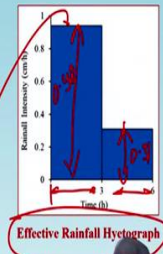
- With the help of the formula

$$\begin{aligned}
 \text{Depth of DR} &= \left[ \frac{(\sum Q) \times t \times 60 \times 60}{A \times 10^6} \right] \\
 &= \left[ \frac{(69) \times 5 \times 60 \times 60}{32 \times 10^6} \right] \\
 &= 0.0388 \text{ m} = 3.88 \text{ cm}
 \end{aligned}$$

(Refer Slide Time: 26:06)

**Solution**

- Now we have, runoff depth in the catchment = 3.88 cm
- Total rainfall in the catchment = 4.2 + 2.2 = 6.4 cm
- Total duration of rainfall = 6 h
- Therefore,
  - $\phi$ -index =  $\frac{6.4 - 3.88}{6} = 0.42 \text{ cm/h}$
  - Effective rain in the 1<sup>st</sup> spell of 3-h of rainfall =  $4.2 - (0.42 \times 3) = 2.94 \text{ cm}$
  - Effective rainfall intensity in 1<sup>st</sup> spell =  $\frac{2.94}{3} = 0.98 \text{ cm/h}$
  - Effective rain in the 2<sup>nd</sup> spell of 3-h of rainfall =  $2.2 - (0.42 \times 3) = 0.94 \text{ cm}$
  - Effective rainfall intensity in 2<sup>nd</sup> spell =  $\frac{0.94}{3} = 0.31 \text{ cm/h}$



Effective Rainfall Hyetograph

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- Now we have, runoff depth in the catchment = 3.88 cm

Total rainfall in the catchment = 4.2 + 2.2 = 6.4 cm

Total duration of rainfall = 6 h

- Therefore,

$$\phi\text{-index} = \frac{6.4 - 3.88}{6} = 0.42 \text{ cm/h}$$

Effective rain in the 1<sup>st</sup> spell of 3-h of rainfall

$$= 4.2 - (0.42 \times 3) = 2.94 \text{ cm}$$

Effective rainfall intensity in 1<sup>st</sup> spell =  $\frac{2.94}{3} = 0.98 \text{ cm/h}$

Effective rain in the 2<sup>nd</sup> spell of 3-h of rainfall

$$= 2.2 - (0.42 \times 3) = 0.94 \text{ cm}$$

Effective rainfall intensity in 2<sup>nd</sup> spell =  $\frac{0.94}{3} = 0.31 \text{ cm/h}$

(Refer Slide Time: 28:19)

**Example 28.3:**

A 4-h storm occurs over a watershed having an area of 70 km<sup>2</sup>. The details of the sub-area of the catchment and hourly distribution of rainfall are as follows:

| Sub Area (km <sup>2</sup> ) | $\phi$ -index (mm/hr) | Hourly Rain (mm)     |                      |                      |                      |
|-----------------------------|-----------------------|----------------------|----------------------|----------------------|----------------------|
|                             |                       | 1 <sup>st</sup> hour | 2 <sup>nd</sup> hour | 3 <sup>rd</sup> hour | 4 <sup>th</sup> hour |
| 10                          | 8                     | 15                   | 65                   | 45                   | 22                   |
| 20                          | 12                    | 17                   | 40                   | 38                   | 16                   |
| 25                          | 20                    | 11                   | 35                   | 25                   | 18                   |
| 15                          | 20                    | 10                   | 62                   | 32                   | 14                   |

Estimate the direct runoff (both in volume and depth unit) from the catchment and the hourly distribution of the average ERH from the entire catchment.

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**Example 28.3:**

A 4-h storm occurs over a watershed having an area of 70 km<sup>2</sup>. The details of the sub-area of the catchment and hourly distribution of rainfall are as follows:

| Sub Area (km <sup>2</sup> ) | $\phi$ -index (mm/hr) | Hourly Rain (mm)     |                      |                      |                      |
|-----------------------------|-----------------------|----------------------|----------------------|----------------------|----------------------|
|                             |                       | 1 <sup>st</sup> hour | 2 <sup>nd</sup> hour | 3 <sup>rd</sup> hour | 4 <sup>th</sup> hour |
| 10                          | 8                     | 15                   | 65                   | 45                   | 22                   |
| 20                          | 12                    | 17                   | 40                   | 38                   | 16                   |
| 25                          | 20                    | 11                   | 35                   | 25                   | 18                   |
| 15                          | 20                    | 10                   | 62                   | 32                   | 14                   |



Estimate the direct runoff (both in volume and depth unit) from the catchment and the hourly distribution of the average ERH from the entire catchment.

(Refer Slide Time: 30:09)

**Solution**

- Calculate the hourly Excess Rainfall (ER) for each sub-area.

$$\text{hourly ER} = \text{hourly Rainfall} - \phi\text{-index}$$

| Sub-area (km <sup>2</sup> ) | $\phi$ -index (mm/hr) | Hourly Excess Rainfall (mm) |                      |                      |                      |
|-----------------------------|-----------------------|-----------------------------|----------------------|----------------------|----------------------|
|                             |                       | 1 <sup>st</sup> hour        | 2 <sup>nd</sup> hour | 3 <sup>rd</sup> hour | 4 <sup>th</sup> hour |
| 10                          | 8                     | 7                           | 57                   | 37                   | 14                   |
| 20                          | 12                    | 5                           | 28                   | 26                   | 4                    |
| 25                          | 20                    | 0                           | 15                   | 5                    | 0                    |
| 15                          | 20                    | 0                           | 42                   | 12                   | 0                    |

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**Example 28.3:**

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| 15                          | 20                    | 10                   | 62                   | 32                   | 14                   |

Estimate the direct runoff (both in volume and depth unit) from the catchment and the hourly distribution of the average ERH from the entire catchment.

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## Solution

- Calculate the hourly Excess Rainfall (ER) for each sub-area,

$$\text{hourly ER} = \text{hourly Rainfall} - \phi\text{-index}$$

| Sub-area (km <sup>2</sup> ) | $\phi$ -index (mm/hr) | Hourly Excess Rainfall (mm) |                      |                      |                      |
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|                             |                       | 1 <sup>st</sup> hour        | 2 <sup>nd</sup> hour | 3 <sup>rd</sup> hour | 4 <sup>th</sup> hour |
| 10                          | 8                     | 7                           | 57                   | 37                   | 14                   |
| 20                          | 12                    | 5                           | 28                   | 26                   | 4                    |
| 25                          | 20                    | 0                           | 15                   | 5                    | 0                    |
| 15                          | 20                    | 0                           | 42                   | 12                   | 0                    |

(Refer Slide Time: 31:22)

**Solution**

- The average ERH for the entire basin is obtained by giving weightages to each sub-area as  $(\text{Sub-area}/\text{Total Area})$ .

$$1^{\text{st}} \text{ hour} = 1/70 \times [(7 \times 10) + (5 \times 20)] = 2.43 \text{ mm}$$

$$2^{\text{nd}} \text{ hour} = 1/70 \times [(57 \times 10) + (28 \times 20) + (15 \times 25) + (42 \times 15)] = 30.50 \text{ mm}$$

$$3^{\text{rd}} \text{ hour} = 1/70 \times [(37 \times 10) + (26 \times 20) + (5 \times 25) + (12 \times 15)] = 17.07 \text{ mm}$$

$$4^{\text{th}} \text{ hour} = 1/70 \times [(14 \times 10) + (4 \times 20)] = 3.14 \text{ mm}$$

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The average ERH for the entire basin is obtained by giving weightages to each sub-area as  $(\text{Sub-area}/\text{Total Area})$ .

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**Solution**

- The hourly runoff and runoff volume from each sub-area are calculated as

$$\text{Runoff from sub-area} = (1^{\text{st}} + 2^{\text{nd}} + 3^{\text{rd}} + 4^{\text{th}}) \text{ hourly ER}$$

$$\text{Runoff volume from sub-area (in Mm}^3\text{)} = (\text{Runoff from sub-area} \times \text{subarea}/1000)$$

| Sub-area (km <sup>2</sup> )                        | Hourly Excess Rainfall (mm) |                      |                      |                      | Runoff Depth from sub-area (mm) | Runoff volume from sub-area (Mm <sup>3</sup> ) |
|--|-----------------------------|----------------------|----------------------|----------------------|---------------------------------|--|
|  | 1 <sup>st</sup> hour        | 2 <sup>nd</sup> hour | 3 <sup>rd</sup> hour | 4 <sup>th</sup> hour |                                 |  |
| 10   | 7                           | 57                   | 37                   | 14                   | 115                             | 1.15   |
| 20   | 5                           | 28                   | 26                   | 4                    | 63                              | 1.26   |
| 25   | 0                           | 15                   | 5                    | 0                    | 20                              | 0.5  |
| 15   | 0                           | 42                   | 12                   | 0                    | 54                              | 0.81   |
| Area averaged calculation for the entire catchment |                             |                      |                      |                      |                                 |  |
| 70   | 2.43                        | 30.50                | 17.07                | 3.14                 | 53.14                           | 3.72   |

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The hourly runoff and runoff volume from each sub-area are calculated as

$$\text{Runoff from sub-area} = (1^{\text{st}} + 2^{\text{nd}} + 3^{\text{rd}} + 4^{\text{th}}) \text{ hourly ER}$$


$$\text{Runoff volume from sub-area (in Mm}^3\text{)} = (\text{Runoff from sub-area} \times \text{subarea}/1000)$$

| Sub-area<br>(km <sup>2</sup> )                     | Hourly Excess Rainfall (mm) |                         |                         |                         | Runoff Depth from sub-area<br>(mm) | Runoff volume<br>from<br>sub-area (Mm <sup>3</sup> ) |
|--|-----------------------------|-------------------------|-------------------------|-------------------------|------------------------------------|--|
|  | 1 <sup>st</sup><br>hour     | 2 <sup>nd</sup><br>hour | 3 <sup>rd</sup><br>hour | 4 <sup>th</sup><br>hour |                                    |  |
| 10   | 7                           | 57                      | 37                      | 14                      | 115                                | 1.15   |
| 20   | 5                           | 28                      | 26                      | 4                       | 63                                 | 1.26   |
| 25   | 0                           | 15                      | 5                       | 0                       | 20                                 | 0.5  |
| 15   | 0                           | 42                      | 12                      | 0                       | 54                                 | 0.81   |
| Area averaged calculation for the entire catchment |                             |                         |                         |                         |                                    |  |
| 70   | 2.43                        | 30.50                   | 17.07                   | 3.14                    | 53.14                              | 3.72   |

(Refer Slide Time: 33:56)

**Summary**

- A general introduction to base flow and its importance in hydrology is discussed.
- Theoretical methods of separating base flow namely straight line method, two lines method and curve extension method are discussed.
- An introduction to the term Direct Runoff Hydrograph (DRH) and Effective Rainfall Hyetograph (ERH), difference between them and their application in hydrograph analysis is covered.
- Example problems to construct DRH, ERH and to separate base flow is covered.
- In the next lecture, concept of unit hydrograph will be discussed.



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## Summary

In summary, we learned the following points from this lecture:

- A general introduction to base flow and its importance in hydrology is discussed.
- Theoretical methods of separating base flow namely the straight-line method, two lines method, and curve extension method are discussed.
- An introduction to the term Direct Runoff Hydrograph (DRH) and Effective Rainfall Hyetograph (ERH), the difference between them and their application in hydrograph analysis is covered.
- Example problems to construct DRH, ERH, and separate base flow are covered.
- In the next lecture, the concept of unit hydrograph will be discussed.