

Soil Dynamic
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Lecture 24

Determination of Dynamic Properties of Soils (Laboratory Tests - Part 4)

Hello friends today I will continue the lecture on determination of dynamic properties of soils using laboratory test already we have seen how to find out the different dynamic properties of soil by conducting resonant column test by conducting cyclic triaxial test.

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Cyclic Torsional Shear Test

- Cyclic torsional shear test is commonly used to determine the stiffness and damping characteristics of soils over a wide range of strain levels. (Min. amp. of cyclic shear strain $> 10^{-4}$)
- The main feature of the cyclic torsional shear test is that it allows isotropic or anisotropic initial stress condition and imposes shear stresses on horizontal planes
- Ishihara and Li (1972) designed the torsional triaxial test by modifying the triaxial apparatus to provide torsional strains on solid cylindrical specimen.
- The major disadvantage of this device designed by Ishihara and Li (1972) was that the shear strain varies from maximum at the outer surface to zero at the centre.

The slide includes a video inset of a woman speaking and a red circled number '4' in the bottom right corner. Logos for IIT Kharagpur and NPTEL are visible at the bottom left.

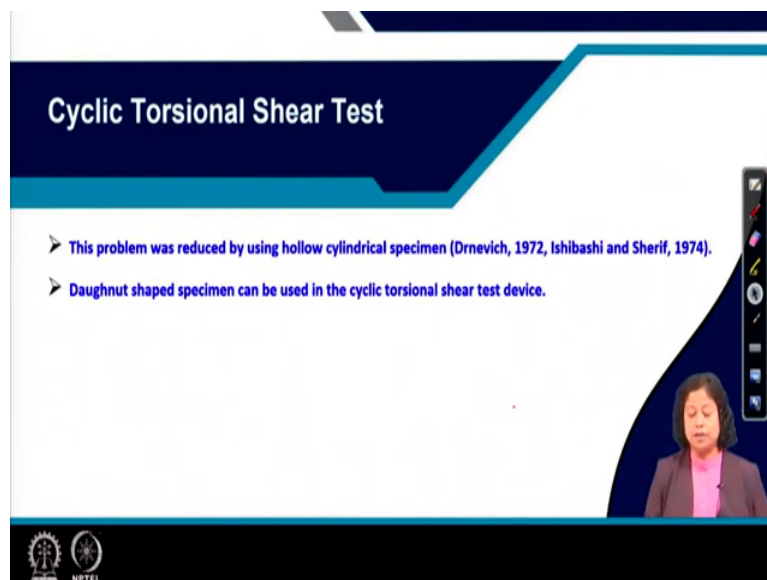
So today we will see how we can find out the dynamic properties of soil by conducting cyclic torsional shear test. Cyclic torsional shear test is one of the high strain laboratory tests conducting which we can determine the dynamic properties of soil. In this context I would like to mention here once again what is high strain test when the cyclic shear strain amplitude is more than 10 to the power minus 4 or I can say the amplitude of the cyclic shear strain is more than 10 to the power minus 2 in percentage then the test is considered as high strain test.

So cyclic torsional shear test is one of such high strain test, this test is commonly used to determine the stiffness and damping ratio of soils over a wide range of strain levels. However, the minimum strain level should be 10 to the power let me write here the minimum strain level that is 10 to the power minus 4, minimum better I just write it as minimum amplitude of cyclic shear strain that is always more than 10 to the power minus 4.

The main feature of the cyclic torsional shear test is that it allows isotropic or anisotropic initial stress condition and imposes shear stresses on the horizontal plane. Ishihara and Li in the year of 1972 design the torsional triaxial test by modifying the triaxial apparatus to provide torsional strains on solid cylindrical soil specimen, the major disadvantage of these device designed by Ishihara and Li was that the shear strain varies from maximum at the outer surface to the zero at the center.

So if I draw the cross sectional area of the cylindrical specimen then in the device which was designed by Ishihara and Li in that device what was happened maximum shear strain was developed at the surface and 0 at the center. So this is the kind of shear strain distribution over the cross sectional area.

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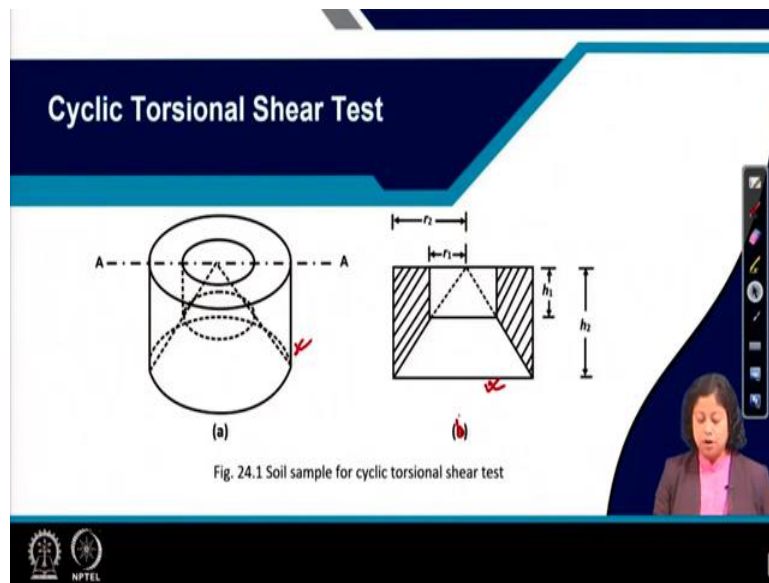
The slide features a dark blue header with the title 'Cyclic Torsional Shear Test' in white. Below the header, there are two bullet points in blue text. A video inset in the bottom right corner shows a woman speaking. The NPTEL logo is visible in the bottom left corner.

Cyclic Torsional Shear Test

- This problem was reduced by using hollow cylindrical specimen (Drnevich, 1972, Ishibashi and Sherif, 1974).
- Doughnut shaped specimen can be used in the cyclic torsional shear test device.

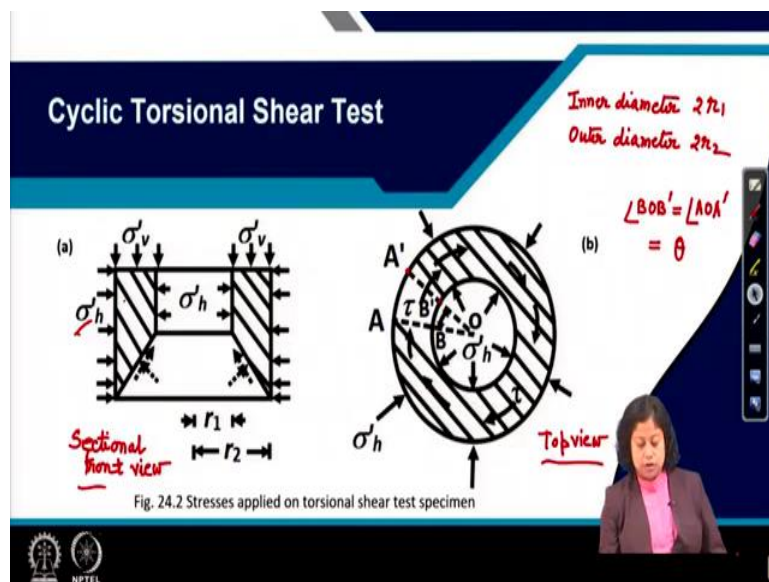
This problem is required to reduce and that was done by using hollow cylindrical specimen which was proposed by different researchers like Drnevich in 1972, then Ishibashi and Sheriff in 1974. So in this case what they have done, doughnut shaped specimen soil specimen was used in the cyclic torsional shear test device.

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So here you can see that doughnut shape cylindrical soil specimen if we will cut these cylindrical sorry I should not use the word cylindrical hollow specimen then. So this is the portion where we can expect soil material was there I am just erasing. So in this specimen if we will cut it by section A, A then it will look like this one it should be figure b not a. So a gives the full 3D view of the hollow specimen whereas figure b gives the sectional view of the hollow specimen.

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Shear strain at A, $\gamma_A = \frac{r_2 \theta}{h_2}$
 Shear strain at B, $\gamma_B = \frac{r_1 \theta}{h_1}$
 $\gamma_A = \gamma_B \Rightarrow \frac{r_2 \theta}{h_2} = \frac{r_1 \theta}{h_1}$
 $\Rightarrow \frac{r_1}{h_2} = \frac{r_2}{h_1}$

So in this next figure you can see the stresses acting on the specimen. So here you can see vertical stress is σ_v vertical effective stress whereas horizontal effective stresses σ_h . The dimension of the hollow specimen if you see r_1 is the inner radius whereas r_2 is the outer radius that means it is inner diameter if I will write it here inner diameter that is how much this is $2r_1$ likewise outer diameter this is $2r_2$ for the specimen which is shown in this figure.

Now you can see here when τ is applied we can see how shear stresses developed τ is the shear stress on the specimen from the top. So this is the top view and this is the sectional front view. So I can write it here sectional front view, top view and sectional front view.

So now the main features for the main reason I can say for which we have taken or I can say Ishibashi and Sheriff choose these kinds of specimen was that to develop uniform shear strain to the sample that means if you see the point A and B in original position after applying τ when these A B shifted, A B shifted to A dashed B dashed position. So this is B dashed this is A dashed. So originally it was at A and B. Now how much shear strain is developed at A and B if I will go to the board then I can right here as just give me one minute time.

So at A if I will write the shear strain is γ_A then I can write shear strain at A just going back to the original figure that means here shear strain is how much shear strain is here if you think this angle BOB dashed or I can also write it as AOA dashed, if this angle is equal to θ then we can find out the magnitude of γ_A here. So γ_A will be how much? It will be r_2 times θ divided by h_2 this is the shear strain at A likewise, we can get the shear strain at B also which is γ_B and that is nothing but r_1 times θ divided by h_1 .

Now in order to allow uniform shear strain on the soils specimen what we need to do gamma A is equal to gamma B, if so what we can write here $r_2 \theta$ divided by h_2 which is equal to gamma B. So in place of gamma B I can write $r_1 \theta$ divided by h_1 .

So from this what we can see r_1 by r_2 is equal to h_1 divided by h_2 that means the ratio of the inner diameter to outer diameter or I can say the ratio of the inner radius to outer radius is equal to the ratio of the height h_1 to height h_2 that means, for the doughnut shape sample the height at the inner phase is h_1 and outer phase it is h_2 . So that ratio of these two height should be equal to the ratio of the inner to outer radii.

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Cyclic Triaxial Test Method

- Due to application of shear stress τ to the sample, the line AB shifts to new position A'B'.
- The shear strain at A: $\gamma_A = \frac{r_2 \theta}{h_2}$... (1a)
- The shear strain at B: $\gamma_B = \frac{r_1 \theta}{h_1}$... (1b)
- If uniformly shear strain is developed from the inner surface to outer surface of the specimen, then,

$$\gamma_A = \gamma_B \quad \dots (2)$$
- So, $\frac{r_2 \theta}{h_2} = \frac{r_1 \theta}{h_1}$
- Finally,

$$\frac{r_1}{r_2} = \frac{h_1}{h_2} \quad \dots (3)$$


So here you can see the same way I have written that because we are interested to develop the uniform shear strain in the soil specimen. So here gamma A is equal to gamma B that I have already explained. So the same thing is written here and thus finally what we get is r_1 by r_2 is equal to h_1 by h_2 . Let us give number to all these equations.

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Cyclic Torsional Shear Test

$$\frac{h_1}{h_2} = \frac{r_1}{r_2}$$

- With proper designing of cyclic torsional shear test device as stated in Equation (3) uniform shear strain can be applied to soil specimen.
- This specimen has inner and outer diameters of 50.8 mm (i.e. 1 in.) and 101.6 mm (2 in.), respectively.
- The inner and outer heights of the specimen are generally 25.4 mm (i.e. 0.5 in.) and 50.8 mm (i.e. 1 in.), respectively.
- Generally, up to 1% shear strain can be applied to the specimen.



Cyclic Torsional Shear Test


$$\frac{h_1}{h_2} = \frac{r_1}{r_2}$$

- Drnevich (1972) used long hollow cylinder to obtain uniform conditions at the test specimen.
- Ishibashi and Sherif (1974) used a short hollow cylinder specimen.
- The selection of r_1 and r_2 are done by minimizing the difference in average stresses obtained from the following two extreme conditions:
 - ✓ Shear stress shown in Equation (4) varies linearly with radius as for an elastic material.
 - ✓ Shear stress shown in Equation (5) is constant as for pure plastic deformation.

$$\tau_{avg,e} = \frac{4T}{3\pi} \left[\frac{r_2^3 - r_1^3}{(r_2^2 - r_1^2)(r_2 - r_1)} \right] \quad \dots (4)$$

$$\tau_{avg,p} = \frac{3T}{2\pi} \left[\frac{1}{(r_2^2 - r_1^2)} \right] \quad \dots (5)$$

where, T is the applied torque



So now we proper designing of cyclic torsional shear test device as stated in equation 3 what is that? That means r_1 by r_2 is equal to h_1 by h_2 . So satisfying these condition uniform shear strain can be developed or applied to the soil specimen.

Now this specimen has generally inner and outer diameters equal to 50.8 millimeter and 101.6 millimeter respectively. That means inner diameter is 50.8 millimeter and the outer diameter of the specimen is 101.6 millimeter and accordingly the inner and outer height of the specimen can be selected keeping it in mind that the ratio of h_1 to h_2 should be equal to r_1 by r_2 .

So if you see when inner diameter is 50.8 millimeter and outer diameter is 101.6 millimeter that time r_1 by r_2 is 1 by 2, then we need to maintain the same ratio for h_1 by h_2 . Now if h_1

is 25.4 millimeter the h_2 will be two times of 25.4 millimeter which is 50.8 millimeter. In this case there is another thing that generally up to 1 percent shear strain can be applied to the soil specimen.

Next here we can see the difference in the soil sample used by Drnevich in 1972 and Ishibashi and Sheriff in 1974 Drnevich 1972 used long hollow cylinder to obtain the uniform conditions at the test specimen. So here are the main feature is long hollow cylinder whereas Ishibashi and Sheriff 1974 used short hollow cylinder soil specimen. So what is the difference now these long and short hollow?

So in long hollow in both the cases actually the ratio of r_1 by r_2 is equal to h_1 by h_2 . But when it is long that time the radius of the specimen may not be I am talking about the r_2 to may not be equal to h_2 . However, for short hollow cylinder you can take r_2 is equal to h_2 . So if this way you can make the difference between long hollow cylinder and the short hollow cylinder.

Now how you will select r_1 and r_2 there is some guideline the selection of r_1 and r_2 can be done by minimizing the difference in average stress obtained from the following to extreme conditions what are these conditions, first condition saying shear stress shown in equation 4 varies linearly with radius as for an elastic material. So let us see equation 4 and 5 this is equation 4.

Second criteria saying shears stress that means, this one shown in equation 5 is constant for pure plastic deformation. So we have two equations one for the elastic shear stress another for plastic shear stress we can call, now in this equation capital T is the tau applied to the specimen. Now if the difference between the 2 shear stresses mentioned in equation 4 and 5 if this difference will be minimized then we can get that value for the outer radius and inner radius. So one I am repeating once again the selection of r_1 and r_2 are done by minimizing the difference in average stresses obtained from equation 4 and from equation 5.

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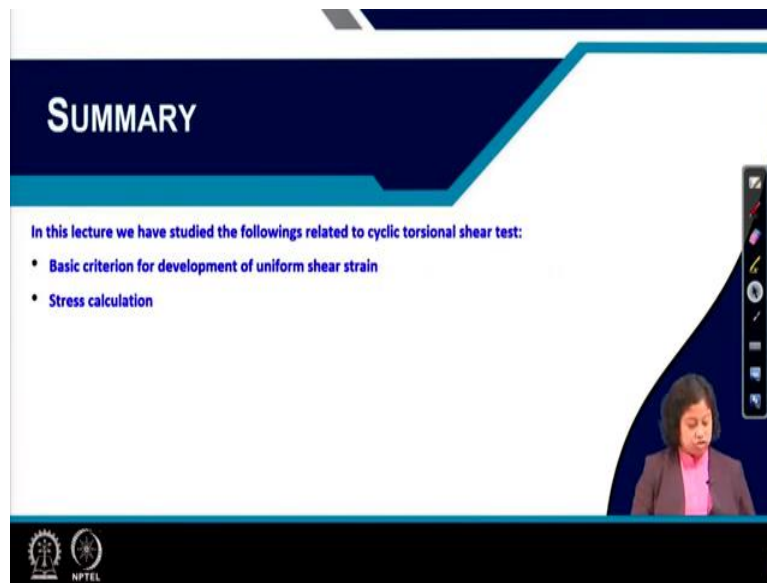
Cyclic Torsional Shear Test
(Calculation of Stresses)

- Major effective principal stress:
$$\sigma_1' = \frac{\sigma_v' + \sigma_h'}{2} + \sqrt{\tau_h'^2 + \left(\frac{\sigma_v' - \sigma_h'}{2}\right)^2} \quad \dots (6)$$
- Intermediate effective principal stress:
$$\sigma_2' = \sigma_h' \quad \dots (7)$$
- Minor effective principal stress:
$$\sigma_3' = \frac{\sigma_v' + \sigma_h'}{2} - \sqrt{\tau_h'^2 + \left(\frac{\sigma_v' - \sigma_h'}{2}\right)^2} \quad \dots (8)$$

Now with this now we know the amount of the vertical effective stress, horizontal effective stress and shear stress applied or developed in the soil sample. So from that we can calculate the major effective principal stress using this equation. So σ_v' is vertical effective stress and σ_h' is horizontal effective stress τ_h' is the shear stress, intermediate effective principal stress that is σ_2' should be equal to σ_h' .

And minor effective principal stress which is σ_3' is equal to $\frac{\sigma_v' + \sigma_h'}{2} - \sqrt{\tau_h'^2 + \left(\frac{\sigma_v' - \sigma_h'}{2}\right)^2}$. So using these 3 equations, we can find out major effective principal stress, intermediate effective principal stress and minor effective principal stress.

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SUMMARY

In this lecture we have studied the followings related to cyclic torsional shear test:

- Basic criterion for development of uniform shear strain
- Stress calculation

Come to the summary of today's lecture. Today we have discussed the basic criteria for development of uniform shear strain on the soil specimen that is r_1 divided by r_2 is equal to h_1 divided by h_2 , then we have started the stress calculation, stress calculation means how to calculate major effective principal stress, intermediate effective principal stress and minor effective principal stress.

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REFERENCES

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2. Soil Dynamics by Shamsheer Prakash, McGraw Hill Higher Education

Journal Papers

3. Drnevich, V.P. (1972). "Undrained cyclic shear of saturated sand." *Journal of Soil Mechanics and Foundation Division, ASCE*, 98 (SM-8), 807-825.
4. Ishibashi, I., and Sherif, M.A. (1974), "Soil liquefaction by torsional simple shear device." *Journal of the Geotechnical Engineering Division, ASCE*. 100(GT-8), 871-888.

Here in this slide you can see the references which I have used for today's class. You can see there are 2 references reference number 3 and 4 are taken from general papers thank you.