

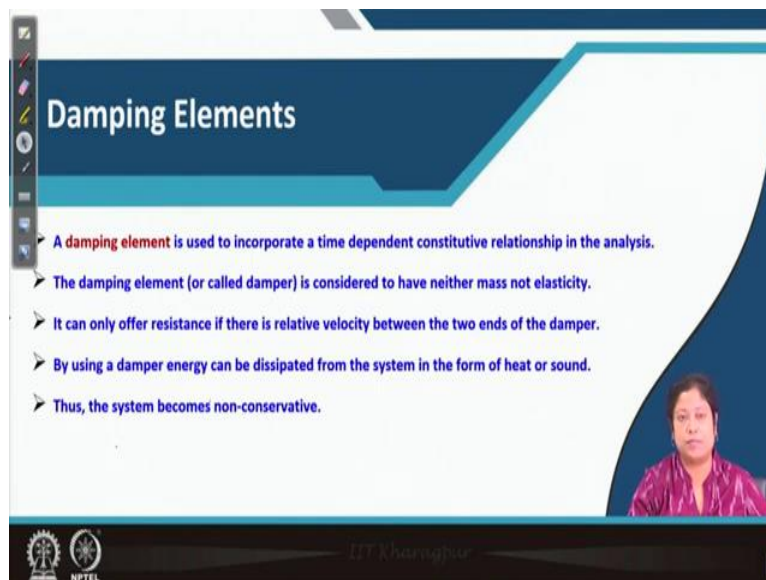
Soil Dynamics
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Lecture - 04
Single Degree of Freedom System (SDOF) - Part 2

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Hello friends. Today we will continue our discussion on single degree of freedom system.

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So, our today's topic is damping, so first we will see what is damping element. So, a damping element is generally used to incorporate a time dependent constitutive relationship in the

analysis. The damping element sometime it is called also as damper is considered to have neither mass nor elasticity.

Now, it can only offer resistance if there is relative velocity between the two ends of the damper. By using a damper energy can be dissipated from the system in the form of either heat or sound. So, in this way the system becomes non-conservative.

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Types of Damping Elements

There are different types of damping elements which are commonly used in the analysis such as:

- ✓ **Viscous Damping** (because viscous fluid flows through a slot) $F_d = c \frac{dx}{dt} = c \dot{z}$
- ✓ **Coulomb Damping** (because of sliding of dry surfaces) $F = \mu N$
- ✓ **Internal Damping** (also called material damping) due to internal friction of materials
- ✓ **Non-Viscous Damping** (due to fluid resistance when a body moving in fluid)

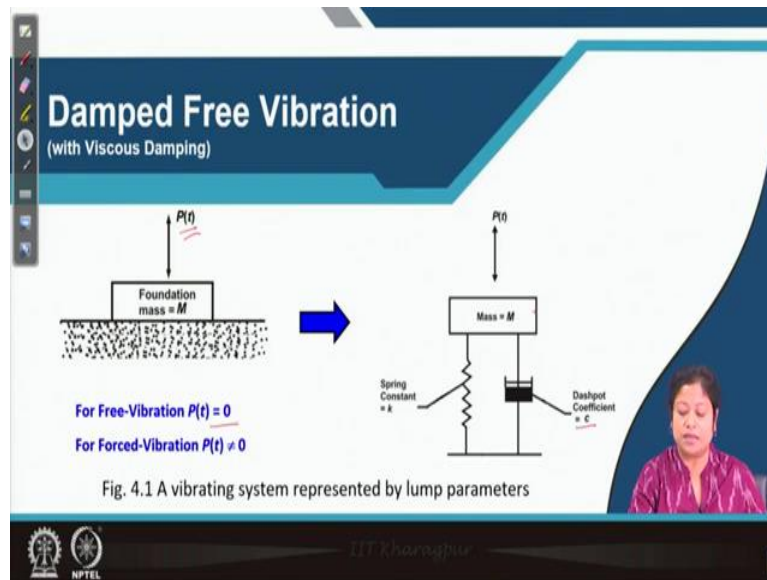
Now, let us see what are the different types of damping elements. There are different types of damping elements which are commonly used in the analysis such as, viscous damping it is present because of the flow of viscous fluid through a slot. Next is coulomb damping which is present because of sliding of dry surfaces on each other? Internal damping is also called as material damping which is due to internal friction of the materials.

Another damping is present in nature which is non viscous damping, this is mainly because of fluid resistance when a body moving in fluid. Now, we, in this subject we will discuss the viscous damping, then we will study coulomb damping also and at the end we will see what is, we will discuss internal damping.

Now, viscous damping, so the damping force for this case if I will take it as F_d this is equal to the C times velocity, so velocity I can write it as $\frac{dz}{dt}$ or I can write it as C times \dot{z} , I am assuming the displacement of the mass in the vertical direction. So, what we can see viscous damping is proportional to the velocity. Now, what is C ? C is coefficient of damping.

Next is coulomb damping, so coulomb damping we can see it is equal to μ times N where N is the normal force acting between the two sliding surfaces and μ is the frictional coefficient between these two sliding surfaces.

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Now, let us see what will be the equation of motion for damped free vibration condition. So, in this figure we can see a foundation which is a block foundation, its mass is capital M is resting on the ground surface. Now, under free vibration condition the load $P(t)$ will be equal to 0, in case of forced vibration $P(t)$ will be non-zero. So, just for the sake of completeness I am just repeating what is free vibration which we have already studied.

So, free vibration system is possible when any system vibrated due to the inherent forces and in absent of the external forces that is the reason in this problem which we have taken here $P(t)$ is equal to 0. Now, the problem can be represented by lump parameters K which is spring constant and dashboard coefficient C . That means the soil is represented by a spring and a dashboard coefficient, dashboard and M is mass of the foundation.

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Damped Free Vibration
(with Viscous Damping)

Equation of motion of a system subjected to free vibration with viscous damping is:

$$M\ddot{z} + c\dot{z} + kz = 0$$

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Free body diagram showing mass M with forces Mg (down) and KZ_s (up). Displacement z is shown from the equilibrium position. \dot{z} is relative velocity.

Unbalanced force = $(-Kz - c\dot{z}) = (Mass)(Acceleration)$

$$M\ddot{z} = -Kz - c\dot{z} \Rightarrow M\ddot{z} + c\dot{z} + Kz = 0$$

So, in this case we can derive the equation of motion of this system which is subjected to free vibration and connect it to viscous damping, let us see. So, first thing what we need to do is to draw the free body diagram of the mass M . So, this is our mass M , we have already seen that when external forces are not present, we can write Mg is equal to K times of Z_s , where Z_s is the static displacement of the mass M under the action of the load Mg .

Now, that is the reason in the free body diagram I will neither show Mg nor KZ_s , since this mass is moving in downward direction so I am taking the current position of the mass is at a distance Z from the equilibrium position under static condition. Now, what are the different forces other than this Mg and KZ_s are acting on this mass M .

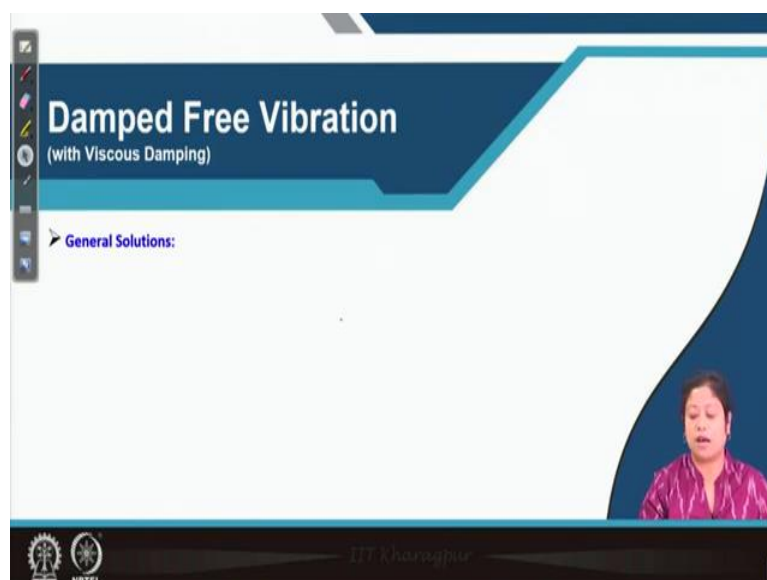
When it is connected to the spring, spring exerts a force which is equal to K times Z , when it is connected to the dashpot also what will be happened at the two ends of the dashpot, it will be subjected to a kind of relative velocity which is equal to \dot{Z} , so \dot{Z} is the relative velocity in this case for the dashpot, two ends of the dashpot.

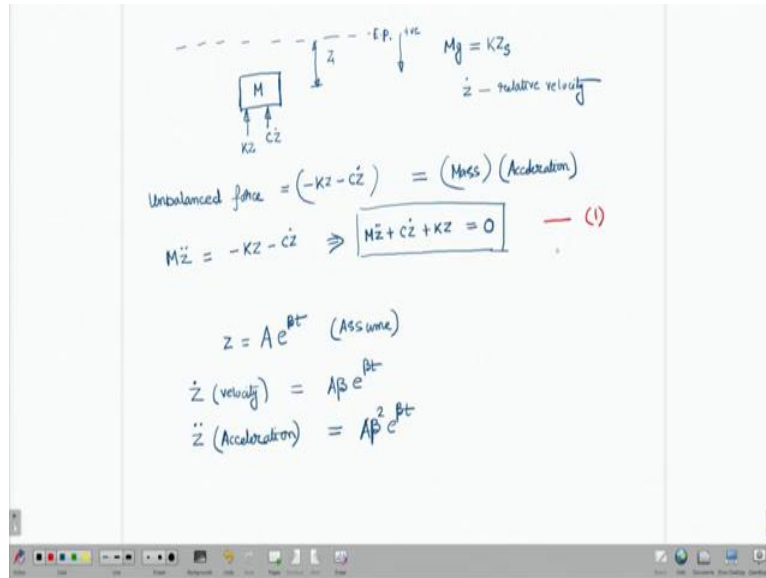
So, the force, damping force which is exerted by the dashpot is equal to C times \dot{Z} . Then under, then what is the amount of the unbalanced force present in this system? Minus KZ which is the spring force minus $C\dot{Z}$ which is damping force. Why minus? Because in this case sign convention is Z is positive in downward direction and this unbalanced force should be equal to the mass times acceleration which is the inertia force.

So, we can write then $M\ddot{Z}$ which is inertia force is equal to minus of KZ minus of $C\dot{Z}$, if we take all the parameters, all the forces on the left hand side then it will become $M\ddot{Z} + C\dot{Z} + KZ = 0$. Why 0? Because we are considering freely vibrating system in this analysis.

Now, we can go back to the slide. So, here the final form you can see once $M\ddot{Z} + C\dot{Z} + KZ = 0$ where $C\dot{Z}$ is damping force because of the viscous damping, KZ is the spring force because of the spring.

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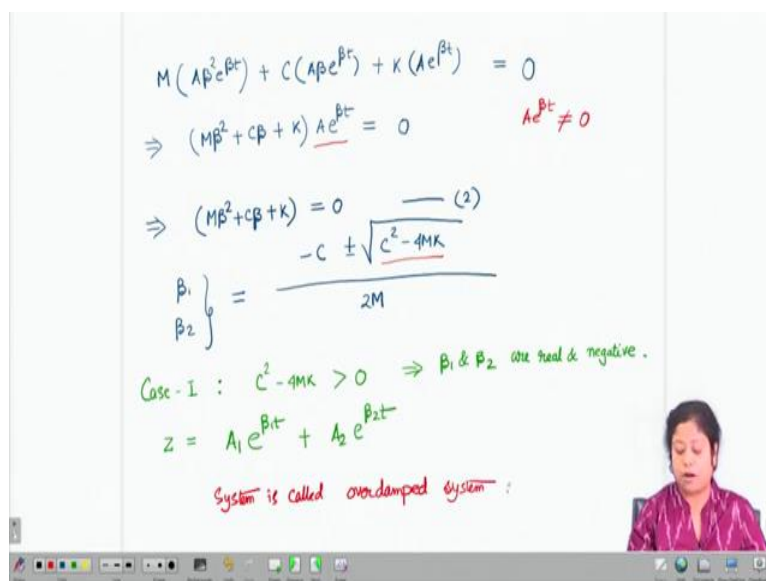




Now, we are interested to find out the general solution for this equation. For this purpose what do we do? We will assume that Z, it is better to write it as small z, z is equal to A times e to the power beta t, this is solution which we assume right now and this kind of trial solution we can take for differential, homogeneous differential equation having form this.

Now, from these trial solution what will be the value of the Z dot which is the velocity? Velocity will be A times beta times e to the power beta, likewise we can write Z two dot which is acceleration in this case will be equal to A times beta square e to the power beta t. Now, let us give this equation one number. Now, if we will write the value of Z, Z Dot and Z double dot to this equation 1 what we will get?

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Case II : $\underline{C^2 - 4MK} = 0$

$$\beta_1 = \beta_2 = -\frac{C}{2M}$$

$$z = (A_1 + A_2 t) e^{\beta t}$$

$$C_c \text{ (critical damping)} = 2\sqrt{MK}$$

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$$\beta_1 = \beta_2 = -\frac{C}{2M}$$

$$z = (A_1 + A_2 t) e^{\beta t}$$

$$C_c \text{ (critical damping)} = 2\sqrt{MK}$$

System is called critically damped system

Case III : $C^2 - 4MK < 0$

$$\beta_1 = \frac{-C + \sqrt{C^2 - 4MK}}{2M}$$

$$\beta_2 = \frac{-C - \sqrt{C^2 - 4MK}}{2M}$$

$$\omega_n = \sqrt{\frac{K}{M}}$$

$$C_c = 2\sqrt{MK}$$

$$\beta_1 = -\frac{C}{2M} + \sqrt{\left(\frac{C}{2M}\right)^2 - \left(\frac{K}{M}\right)}$$

$$\frac{C}{C_c} = \text{Damping ratio } (D)$$

$$D = \frac{C}{2\sqrt{MK}}$$

$$\frac{C}{2M} = D \sqrt{\frac{K}{M}}$$

$$= D \omega_n$$

We will get $M \ddot{z} + C \dot{z} + Kz = 0$ which is nothing but $M \ddot{z} + C \dot{z} + Kz = 0$. Now, it can be rewritten as $M \beta^2 + C \beta + K = 0$, plus K whole thing can be multiplied by $A e^{\beta t}$ and that should be equal to 0.

Now, this $A e^{\beta t}$ is non zero quantity. So, which implies that whatever is written within the bracket z should be 0. So, in this way now we can find out the two roots of the equation 2, it is a second order differential, it is a second order equation of β , so β has two roots. What are these two roots? β_1 and β_2 together I am writing, this is $\frac{-C \pm \sqrt{C^2 - 4MK}}{2M}$.

Now, you can see here depending upon the value of $C^2 - 4MK$ the nature of the roots of equation 2 may change. There are three possibilities in this case. So, let me write all these three cases. So, our case 1, which is first possibility is $C^2 - 4MK$ is greater than 0 that means the quantity under square root is positive quantity.

Then what will be, what can we say about the two roots β_1 and β_2 ? Obviously then we can say β_1 and β_2 both are real and negative because there is a negative sign with C and obviously whatever we will get under this square root of $C^2 - 4MK$ that will always be less than C . So, we can write from here that the two roots β_1 and β_2 are real and negative. Now, then what will be the form of this solution for case 1?

Then we can write Z is equal to $A_1 e^{-\beta_1 t} + A_2 e^{-\beta_2 t}$. Now, come to the next condition which is our case 2. What is case 2? There is second possibility that $C^2 - 4MK$ is equal to 0. Then what will be happened? The quantity I can go back to the previous page, the quantity under square root will be 0 in this case.

As a consequence the two roots β_1 and β_2 will be same $2 - C$ divided by $2M$. Therefore what will be the general solution for this case? Z is equal to $A_1 + A_2 t$ times $e^{-\beta t}$ or you can write βt . Now, in this case we can introduce a new thing, what is that?

See in this case we have seen that see, if I will draw the response of the system let us take this is t or I can write ωt also and this is Z , then the response will look like something like this. So, what we can note here the damping finally because of this damping the system will not be subjected to periodic motion. So, finally we can say this damping is something which is maximum in magnitude, so this damping at this stage is called as critical damping which is represented by C_c critical damping.

And that is equal to if you see here $2 \sqrt{MK}$ which we can get from this or I can show it other way. So we are getting this from actually this relationship, so this damping is called critical damping. And the system is called critically damped system. I have forgot to mention one thing the previous case when C^2 is greater than $4MK$ under that condition the system is called over damped.

Now there is the next case third case when we can see C^2 minus four times of $M K$ will be less than 0. If C^2 minus 4 times of $M K$ that means the quantity under root is less than 0 then what will be happened? The quantity will be a negative quantity under this square root.

So, we can write it as I am writing the general solution, sorry the roots of the equation 2, these are β_1 and β_2 , so β_1 will be equal to, here I will not write plus minus but I will write it as only plus or only minus, so let us take only plus, likewise for β_2 I can write minus C minus square root of C^2 minus 4 $M K$ divided by 2 M .

Now, we can rewrite these two roots in other form also, how, let me do that. So, for β_1 what we can write? Minus C divided by 2 M plus square root of C^2 by 2 M whole square minus K by M , we are already introduced to the term K by M , we are familiar with the term natural damping of the undamped system which is equal to square root of K by M . So, in this case K by M is ω_n^2 .

Now, how we can write C divided by 2 M ? We have already introduced, we have, we are already introduced to the term critical damping which is C_c and that can be expressed as 2 times square root of capital M times K . Now, if we will find out the ratio of the damping of any system to the critical damping, this ratio is called damping ratio, damping ratio and symbolically it is represented by D .

So, now I can write then D is equal to C divided by C_c , C_c means 2 times of square root of $M K$. So, finally with this if capital D is equal to C divided by 2 times square root of $M K$ then what I can write for C divided by 2 M ? C divided by 2 M means we can write D times K , square root of K by M which is equal to D times ω_n .

So, in the expression of β_1 and β_2 now we can write in place of C divided by 2 M the term D times ω_n where D is the damping ratio and ω_n is the natural frequency of undamped system. So, let us do this work.

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The first screenshot shows the derivation of the roots β_1 and β_2 for an underdamped system where $c^2 - 4mK < 0$. The roots are complex conjugates: $\beta_1 = -D\omega_n + \omega_n \sqrt{D^2 - 1}$ and $\beta_2 = -D\omega_n - \omega_n \sqrt{D^2 - 1}$. The general solution is given as $z = [A_1 \sin(\omega_n \sqrt{1-D^2} t) + A_2 \cos(\omega_n \sqrt{1-D^2} t)] e^{-D\omega_n t}$.

The second screenshot shows three cases for the characteristic equation $c^2 - 4mK = 0$:
 - Case II (Critical Damping): $c^2 - 4mK = 0$, $\beta_1 = \beta_2 = -\frac{c}{2m}$. The general solution is $z = (A_1 + A_2 t) e^{\beta t}$. A graph shows a smooth curve decaying to zero. $c_c = 2\sqrt{mK}$ is defined as critical damping. The system is called a critically damped system.
 - Case III (Overdamped): $c^2 - 4mK > 0$. The roots are $\beta_1 = \frac{-c + \sqrt{c^2 - 4mK}}{2m}$ and $\beta_2 = \frac{-c - \sqrt{c^2 - 4mK}}{2m}$.
 - Damping Ratio: $\frac{c}{c_c} = \text{Damping Ratio } (D)$, $D = \frac{c}{2\sqrt{mK}}$, $\frac{c}{2m} = D\sqrt{\frac{K}{m}} = D\omega_n$.

Then beta 1 is equal to, sorry beta 1 is equal to minus D omega n plus square root of D square omega n square minus omega n square or I can write it as D times omega n plus I can take omega n outside the square root and it will be D square minus 1. Now, under underdamped condition when C square minus 4 M K this is less than 0 that means negative that time obviously D is less than 1.

So, because of that reason I can write beta 1 once again as 1 minus D square times minus 1 or minus D omega n plus i omega n times square root of 1 minus D square likewise beta 2 will be minus D times omega n minus i times omega n times square root of 1 minus D square. So, then what will be the general solution for this type of problem?

Z is in this case I can write it as $A_1 \sin$ of this imaginary, coefficient of imaginary part I need to write here, so \sin of ω_n times $1 - D^2$ plus A_2 times \cos of ω_n times $1 - D^2$ and the thing which is written within bracket should be multiplied by e to the power minus $D \omega_n t$.

So, here we have studied, in today's lecture what we have studied? We have studied how to get the general equation for free vibrating system with viscous damping then what are the, what are the possible solutions for that kind of system.

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Damped Free Vibration
(with Viscous Damping)

General Solutions:

- ✓ For Over-damped system: $z = A_1 e^{\beta_1 t} + A_2 e^{\beta_2 t}$ ✓
where, $\beta_1 = -D\omega_n + \omega_n\sqrt{D^2 - 1}$ and $\beta_2 = -D\omega_n - \omega_n\sqrt{D^2 - 1}$ for $D > 1$ ✓
- ✓ For Critically-damped system: $z = (A_1 + A_2 t)e^{-\omega_n t}$ for $D = 1$
- ✓ For under-damped system: $z = e^{-\omega_n t} [A_1 \sin \omega_d t + A_2 \cos \omega_d t] = e^{-\omega_n t} [A_1 \sin \omega_d t + A_2 \cos \omega_d t]$ ✓
where ω_n is undamped natural frequency and ω_d is damped natural frequency.
Also, $\omega_d = \omega_n \sqrt{1 - D^2}$ for $D < 1$

Handwritten notes on the right side of the slide:

- $D = \text{Damping ratio} = \frac{c}{c_c}$
- $\omega_n = \text{Natural frequency of the undamped system}$
- $\omega_d = \text{Natural frequency of damped system}$
- $= \omega_n \sqrt{1 - D^2}$

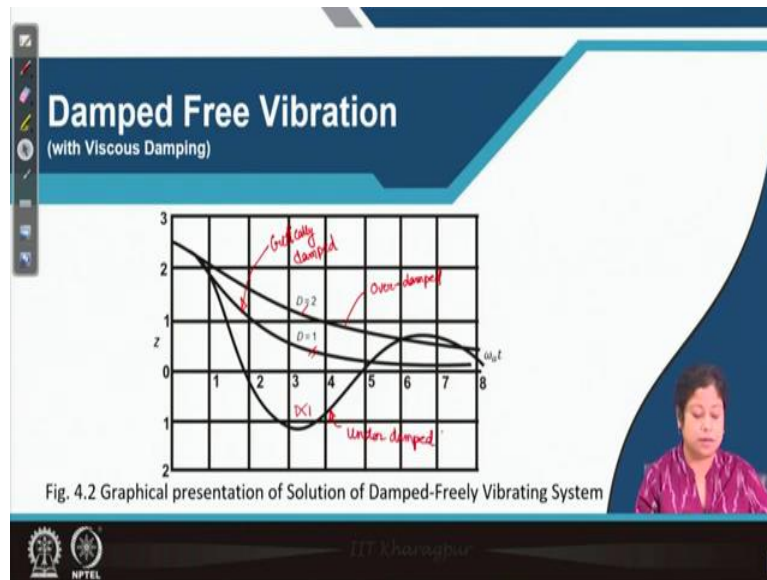
And I can show now what we have done here. So, the general solutions for the three cases which are discussed today can be summarized here, for the over damped system we get Z is equal to A_1 times e to the power $\beta_1 t$ plus A_2 times e to the power of $\beta_2 t$. We can write β_1 and β_2 in terms of D which is damping ratio and the natural frequency of the undamped system which is ω_n .

So, here D is damping ratio which is the ratio of the coefficient of damper to the critical damping and ω_n is the natural frequency of the undamped system. Now, for critically damped system the general solution can be written as $A_1 + A_2 t$ everything within bracket being multiplied by e to the power minus $\omega_n t$. In this case actually D is equal to 1 that is the reason when writing e to the power minus $\omega_n t$ D is not written.

Third case is under-damped system and the general solution for under-damped system is Z equals to e to the power $\omega_n t$, one D is missing here, so let me write it, so there will be a

D also, so I can write once again $e^{-\zeta \omega_n t} [A_1 \sin(\omega_D t) + A_2 \cos(\omega_D t)]$. Now, in this case ω_D is called the natural frequency of the damped system which is equal to $\omega_n \sqrt{1 - \zeta^2}$.

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You can see here the graphical presentation of the solution for damped freely vibrating system for three different cases, this one for D when D is equal to D is less than 1, this curve for D is equal to 1 and the third curve is for D equals to 2. That means this one for over damped, middle one is for critically damped and the third one is for under damped system.

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SUMMARY

In this lecture we discussed the followings:

- ✓ Different types of damping
- ✓ Equation of motion for a mass-spring-dashpot system under free vibration
- ✓ Solutions for Equation of motion for mass-spring system with viscous damping under free vibration
- ✓ Mathematical form of damped natural frequency (ω_d)

So, finally come to the summary. Today we have discussed different types of damping, say viscous damping, coulomb damping, material damping and non-viscous damping. Then we discussed different, then we discussed about the equation of motion how to form the equation of motion for a mass spring dashpot system under free vibration. And then we determine the solution of equation of motion. Finally we have seen what will, what is the mathematical form of damped natural frequency which is ωD . Thank you.