

Circuit Theory

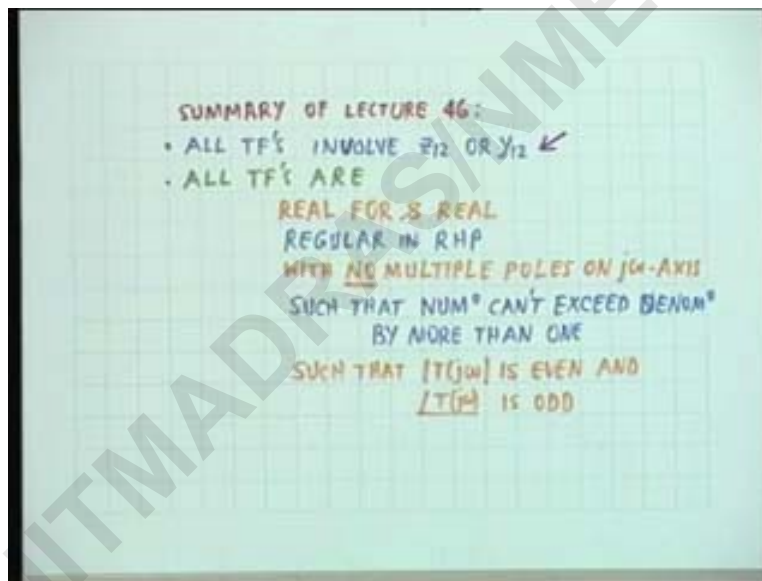
Prof. S.C. Dutta Roy

Department of Electrical EngineeringIIT DelhiLecture 47

Properties and Synthesis of Transfer Parameters

forty seventh lecture and we are going to discuss properties and synthesis of transfer parameters in the last lecture we had discussed some of the properties of transfer functions and a summary is as follows we showed that all transfer functions

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we take several examples of transfer function and we showed that all transfer functions involve besides the driving point parameters that is Z_{11} or Y_{11} or Z_{22} or Y_{22} the transfer parameters Z_{12} or Y_{12}

we have assumed the networks to be reciprocal therefore it is either Z_{12} or Z_{21} it doesn't matter they are equal they are identical we showed that all transfer functions are real for s real they are regular in right half plane does this mean something to you regular in right half plane means there are no poles in the right half plane

regularity means absence of poles no poles in the right half plane all transfer functions are with no multiple poles on the $j\omega$ axis because multiple poles give rise to multiple poles on the $j\omega$ axis give rise to instability and we are talking of passive table reciprocal networks in all transfer functions the degree of the numerator cannot exceed the degree of the denominator by more than one

whereas the reverse is not true that is the denominator may exceed the degree of the numerator by any number okay all transfer functions such that that the magnitude is an even function and the angle is an odd function this where we ended the last lecture alright

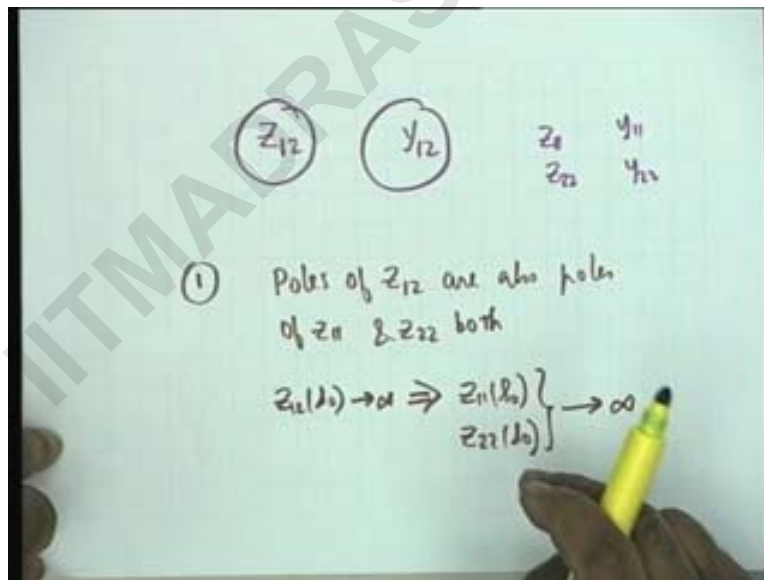
today yes

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it cannot have a multiple pole even at infinity no it cannot

it can have a simple pole at infinity [Noise] okay since all transfer functions

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involve Z_{12} or Y_{12} and in addition to the driving point parameters that is Z_{11} , Z_{22} or Y_{11} , Y_{22} the properties of which you all ready know because they are DPs it suffices to consider a properties of Z_{12} and Y_{12} and there are several properties which have of interest to us at the moment [Noise] we shall we shall discuss only those one of the properties is that poles of Z_{12}

poles of Z_{12} are also poles of Z_{11} and Z_{22} both okay Z_{11} and Z_{22} both but the reverse is not necessarily true what we mean is that any poles of Z_{12} if $Z_{12} \rightarrow \infty$ this implies that $Z_{11} \rightarrow \infty$ $Z_{22} \rightarrow \infty$ both of them will tend to infinity but the reverse is not necessarily true

that means if Z_{11} has a pole it is not necessarily shared by Z_{12} if Z_{22} has a pole it is not necessarily shared by Z_{12} the question at this point is if Z_{11} has a pole does it have to be shared by Z_{22} [Noise] no alright it suffices to make a counter example

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whatever (()) (00:04:16) if Z_{11} has a pole it does not necessarily have to be shared with Z_{12} that is the reverse is not necessarily true

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also Z_{22} Z_{11} and Z_{22} can have poles which are independent of each and independent of Z_{12} one example one counter example will suffice to prove this

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that is what i say that Z_{11} poles and Z_{22} poles can be independent of each other they can also be independent of Z_{12} but Z_{12} cannot have a pole which is not shared by both Z_{11} and Z_{22} agreed

what i said is to forward statement is correct the reverse statement is not necessarily true in other words it is possible for Z_{11} to have pole which is not shared by either Z_{12} or Z_{22}

similarly Z_{22} can have a pole which is not shared by Z_{11} or Z_{12} and a simple counter example

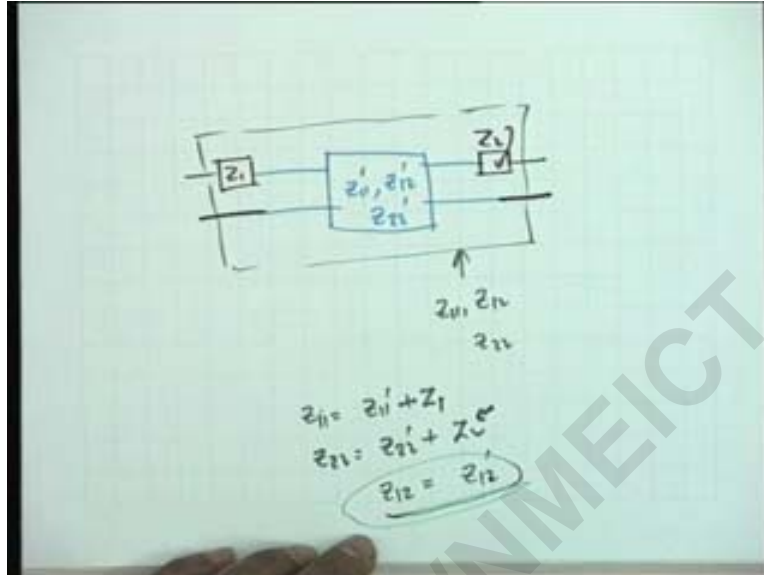
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it is not necessary to have this belong to Z_{12} also

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not necessary in addition Z_{11} and Z_{22} themselves can have independent poles they don't have to share a pole okay as a simple example would be this suppose

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suppose we have a two port network which has the parameters let's say Z'_{11} , Z'_{12} , Z'_{21} , and Z'_{22} okay suppose we have a network like this and then what we do is we supplement this with an impedance Z_2 here and an impedance Z_1 here okay

the supplement this with an impedance and call the total network call the network as the unprimed network that is we call this as Z_{11} , Z_{12} , and Z_{22} alright there is a network inside which is a prime network and then we supplement it with the help of two series impedances Z_1 and Z_2

now you notice that Z_{11} is simply equal to Z'_{11} plus Z_1 agreed similarly Z_{22} is Z'_{22} plus Z_2 and what about Z_{12}

<a_side> ((same)) (00:07:00) <a_side>

same Z'_{12} alright

therefore the poles of Z_{11} the poles of Z_{11} are poles of Z'_{11} not necessarily the poles of Z_1 do not affect Z_{12} is in that right the poles of Z_1 do not affect Z_{12} Z_{12} is the same as the previous Z'_{12}

similarly poles of Z_{22} affects only Z_{22} not Z_{11} or Z_{12} and the simple example shows that Z_{11} can have a pole which does not belong to either the other two parameters

Z_{22} can have a pole which does not belong to either Z_{11} or Z_{12} but any pole of Z_{12} must belong to Z_{11} as well as Z_{22}

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how did i prove that this pole also belongs to this okay good question [Noise]

<a_side> excuse me sir <a_side>

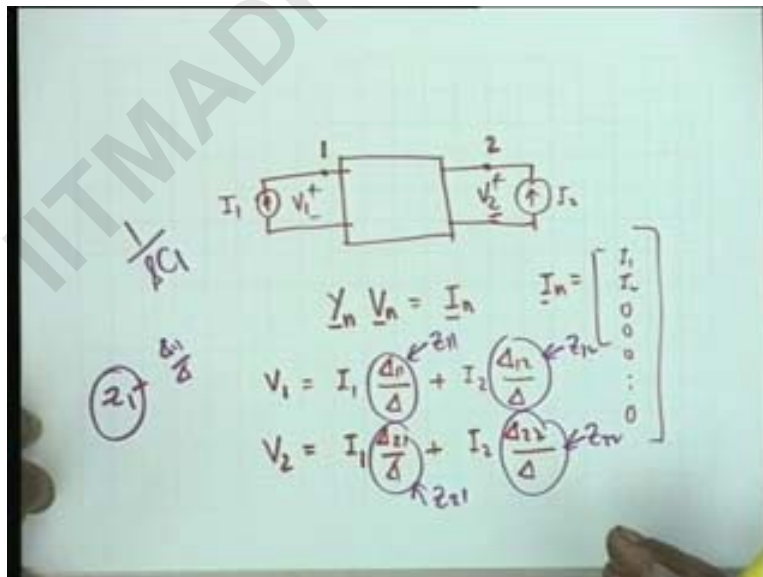
yeah

<a_side> could you please write clearly sir (()) (00:08:08) <a_side>

oh it's not clear the writing oh we will keep this up alright

how do i prove that any pole of Z_{12} also belongs to Z_{11} and Z_{22} alright let's recall

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our node analysis we have two current generators is this clear can you see this okay we have two current generators at the two poles we call this as node one this as node two there is some reference inside some reference and the voltages are the V_1 and V_2 okay

you recall that the node analysis gives you a nodal admittance matrix Y_n multiplied by the nodal voltage vector V_n this is equal to I_n alright

this is the node node matrix equation the nodal equation nodal analysis equation it can be put in this matrix for you have self admittances and mutual admittances and so on and so forth alright is this okay

where i have just two generators I_1 and I_2 so I_n for example is equal to I_1 I_2 then zero zero zero etcetera zero alright and what we wanted to find out is V_1 and V_2 that is this two voltages i want to express in terms I_1 and I_2 and you recall that this was $I_1 \Delta^{-1} + I_2 \Delta^{-1}$ where Δ is the determinate of this matrix

similarly i have done this earlier V_2 is $I_1 \Delta^{-1} + I_2 \Delta^{-1}$ agreed so you can now identify what are the Z_{11} Z_{12} this is obviously Z_{11} and this is Z_{12}

which is the same as Z_{21} because the network is a reciprocal Δ^{-1} is equal to Δ^{-1} and this is equal to Z_{22} and you see that poles poles of all the functions should normally be the same because a poles are created by putting Δ equal to zero any value of s that which Δ equal to zero is a pole a pole should be shared by all the four parameters any pole of Z_{12} must also belong to Z_{11} alright but the reverse is not necessarily true which we showed by this simple example that if there is an element in series at port one this affects only Z_{11} nothing else

<a_side> but sir for this case if we prove if Δ is zero (()) (00:11:24) <a_side>

yeah if Δ is zero

<a_side> for the pole of uh for the pole for Z_{11} Δ should be zero <a_side>

correct

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so what i do is i add an element another element Z_1 in series with this so all that it changes is that it becomes Z_1 plus

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del one one by del

so any pole of Z_{11} also is now a pole of the augmented network it does not affect Z_{22} or Z_{12} alright

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del one one then the whole thing is not a pole or del one one can also have a pole at the same point

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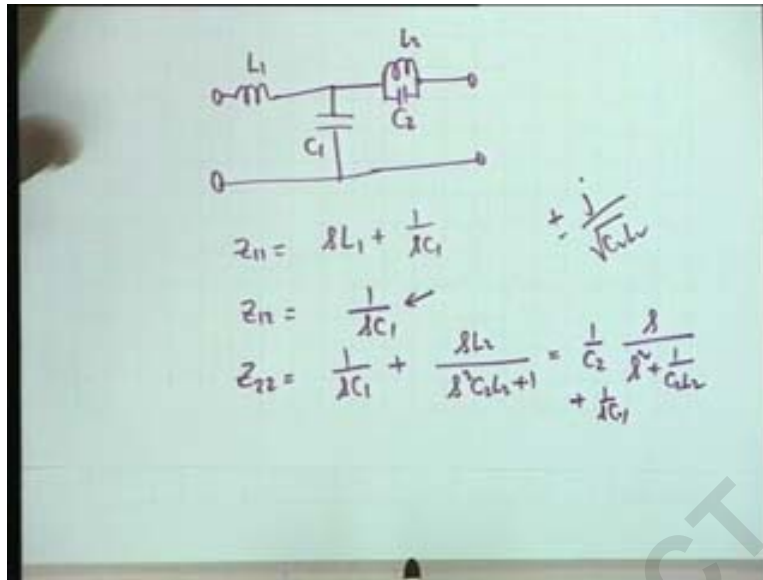
that will be an independent pole

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you see what i [Laughter] what your going to do ultimately ultimately is that del one one and del both in general will be rational functions and what you will do is you will break you make this into a polynomial divided by polynomial by clearing of inverse expressions like one by sC one and so on

so the denominators of all this rational function will be the same [Noise] correct and therefore the poles the zeros of the denominator shall occur at the same point poles must in general be shared on the other hand there are exceptions with regard to Z_{11} Z_{22} because we can add anything in series it does not affect Z_{11} alright let's take a simple example

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let's have an inductor L_1 a capacitor C_1 and let's say an L_2 and C_2 okay what are Z_{11} , Z_{12} , Z_{21} and Z_{22} of this structure $sL_1 + 1/sC_1$ what is it equal to

<a_side> $(\frac{1}{sC_1})$ (00:13:37) <a_side>

one over sC_1 and Z_{22} is one over sC_1 plus can someone tell me what this is

<a_side> $(\frac{sL_2}{s^2 C_2 L_2 + 1})$ (00:13:50) <a_side>

sL_2 divided by $s^2 C_2 L_2 + 1$ agreed which is equal to one over $C_2 s$ divided by $s^2 C_2 L_2 + 1$ i am sorry plus one over sC_1 this we must ignore we must not ignore

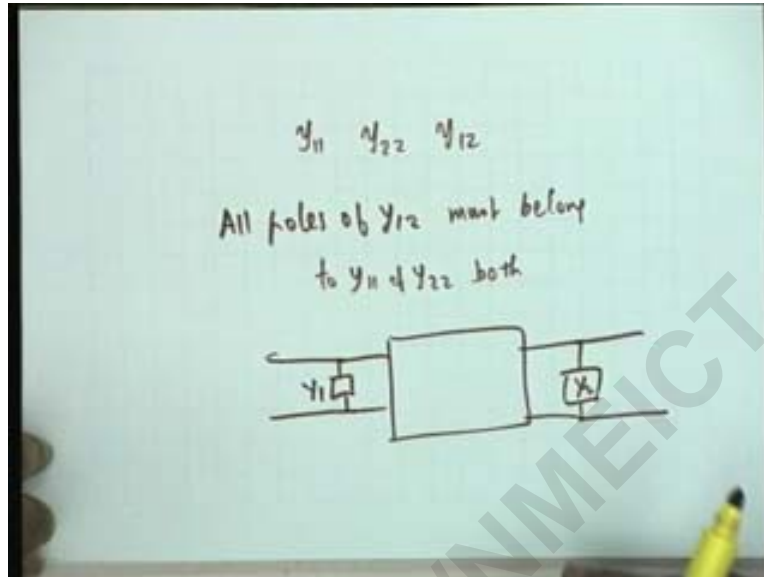
and if you notice that the pole at $s = 0$ which is the pole Z_{12} is also present in Z_{11} and Z_{22} that is this pole is shared by all the three parameters

on the other hand the pole at infinity of Z_{11} is not shared by either Z_{12} or Z_{22} there is no pole at infinity of either of them so this pole is as if a personal property of Z_{11} it is called the personal pole [Noise] you may call it a [Noise] personal pole

similarly the pair of poles at $\pm j \sqrt{C_2 L_2}$ belongs only to Z_{22} it doesn't belong to Z_{11} and Z_{12} alright so the property is that any pole of Z_{12} must also belong to Z_{22} and Z_{11} but Z_{11} and Z_{22} can have poles which are personal to themselves it doesn't have to be shared

Z_{12} is not in that privileged position its transfer parameter poles must be shared by the other two parameters also in a similar manner you can show

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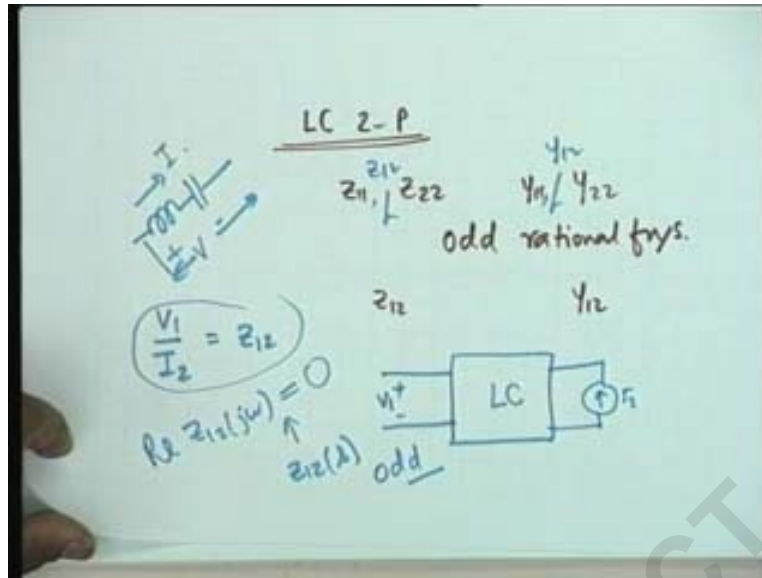
that if you take the Y_{11} , Y_{22} and Y_{12} parameters you can show that all poles of Y_{12} must also belong to Y_{11} and Y_{22} all poles of Y_{12} must belong to Y_{11} and Y_{22} both but the reverse statement is not necessarily true

that is Y_{11} can have a pole which is not shared with Y_{22} or Y_{12} Y_{22} can have a pole which is not necessarily shared by Y_{11} as well as Y_{12} and the counter example here is that if you add an admittance in parallel with port one if you add an admittance in parallel with port one Y_{11} and an admittance Y_{22} here

then Y_{11} affects small y_{11} only Y_{22} affects small y_{22} only it is exactly the dual of the previous case in the previous case we are used to impedance in series now there are two admittance in (parallel) (00:16:58)

Y_{11} does not affect Y_{22} why not because in measuring Y_{22} you have to short this so Y_{11} goes out of the picture okay now [Noise] the third property that we shall be interested in is the special case of LC two pole

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if a two port is LC okay then you no that Z one one Z two two [Noise] and Y one one and Y two two they had a particular character can you pinpoint this character the kind what kind of rational function

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odd all of them are odd rational functions if the two port is LC then all of them are odd rational functions what can you say about Z one two and Y one two what can you say about Z one two and Y one two can they be even or can they be neither odd nor even

this requires a bit of investigation now i cannot give you ah [Noise] strict proof of this this is beyond the scope of the class but let me sight a very simple simple logic suppose we consider Z one two by definition what is Z one two Z one two is what is the definition V two

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by I one with

<a_side> (()) (00:18:45) <a_side>

V one by I two okay alright

i have a current generator I two here and V one this has to be kept open circuited and this elements are all LC alright

so under this condition if i measure V_1 by I_2 if i measure V_2 by I_1 this would be Z_{12} we are asking the question we are asking question what is the is there is there any special character that you can assign to Z_{12} is it purely even is it purely odd or is it neither purely even not purely odd okay this is the question that i am asking

the logic that i am extending is the following that if this is an LC network any voltage in the LC network and any current in the LC network any voltage and any current they have to be ninety degrees out of phase in the steady state isn't that [Noise] right

in other words in other words if i take $Z_{12}(j\omega)$ if i take $Z_{12}(j\omega)$ this has to be purely imaginary which means that real part of $Z_{12}(j\omega)$ must be equal to zero which means now that $Z_{12}(s)$ if it is purely imaginary for $s = j\omega$ obviously $Z_{12}(s)$ must be purely odd

so the property that we have come to the conclusion know is that for an LC two port all parameters all Z parameters and all Y parameters must be purely odd

so you add to this Z_{12} and add to this Y_{12} all of them must be odd rational functions
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could i explain it again [Laughter]

the argument that i gave was all voltages shall have to be ninety degree out of phase because at a particular frequency at a sinusoidal frequency in this steady state all voltages must be ninety degree out of phase with all currents respective of every measuring and therefore this ratio if i take the real part that must be zero for $s = j\omega$ it must be purely imaginary either plus j times a constant or minus j times a constant that is either plus ninety or minus ninety

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we cannot have a real part

<a_side> (()) (00:21:21) <a_side>

what is what is what is obvious

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it is not a driving point function if it is a driving point function it is obvious

it is a transfer parameter now which means that any point at any point you measure the voltage that any other point you measure the current

these two voltages and currents must be ninety degree out of phase it cannot be anything other word they cannot be in between because it is an LC network

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no not necessarily you can draw a phase of diagram with voltages and currents at different points no problem

<a_side> (()) (00:22:02) <a_side>

they cannot be in phase no voltage and current can be in phase in a in an LC network

<a_side> (()) (00:22:12) <a_side>

[Laughter] you construct your example you take you construct a counter example

<a_side> (()) (00:22:20) <a_side>

not example

<a_side> (()) (00:22:21) <a_side>

in the case of resonance well i was expecting this [Laughter] if you have [Noise] if you have a voltage and current this is a driving point function okay if this is V and this is I okay then the impedance is zero which means that the ratio of voltage to current is either zero or infinity

in other words at that point it has a pole we are not talking of a pole or a zero okay we are talking in general if the function has a pole well all LC parameters have to have poles on the $j\omega$ axis only oh is that obvious

that if the network is LC that's an interesting point let's pause for a moment if the network is LC then all poles have to be on the $j\omega$ axis poles of the all the parameters yes

<a_side> yes sir <a_side>

because Z_{12} cannot have a pole which is not shared by Z_{11} and Z_{22} also because Z_{12} poles must also be on the $j\omega$ axis okay

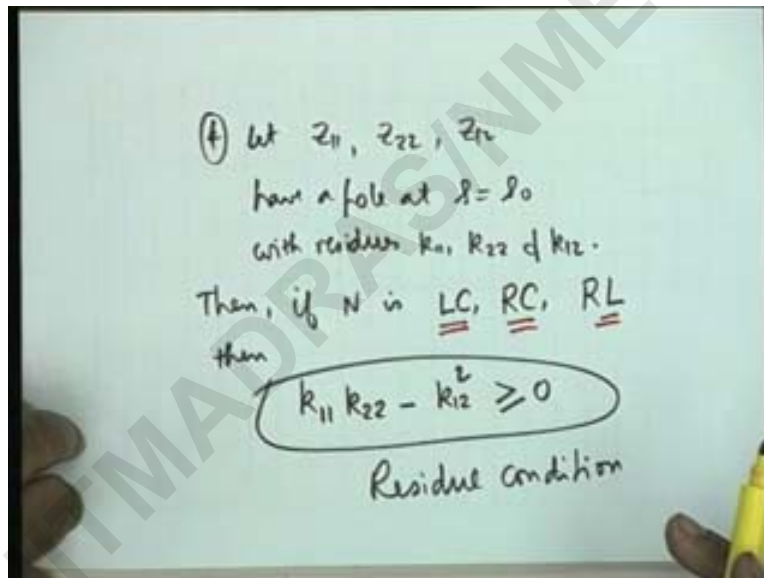
we are not talking of poles or zeros we are talking of of the {ratio} (00:23:42) of frequency at which the ratio is neither pole nor a zero at that point the voltage and current measured anywhere in the network shall be ninety degree out of phase and if you if you consider this ah a challenge construct a counter example alright that i leave to go

the third point [Noise] the third point that i ah third or fourth

<a_side> (()) (00:24:22) <a_side>

it shall be the fourth one okay the fourth point that i want to mention here is [Noise] the follows and this i have to state without proof because it proof is beyond this scope of this [Noise] of this class the fourth point is that

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if you have a set of parameters let's say Z_{11}, Z_{22}, Z_{12} [Noise] and suppose all of them have a pole at all of them have a pole at let's say some point s equal to s_0 with residues if there is a pole there should be a residual okay with residuals K_{11}, K_{22} and K_{12} alright

then the statement of this propriety is that if the network is [Noise] two element kind that it is either LC or RC or RL

if the network is two element kind that it is either LC or RC or RL then the following property is true that is $K_{11} K_{22} - K_{12}^2$ [Noise] is greater then or equal to

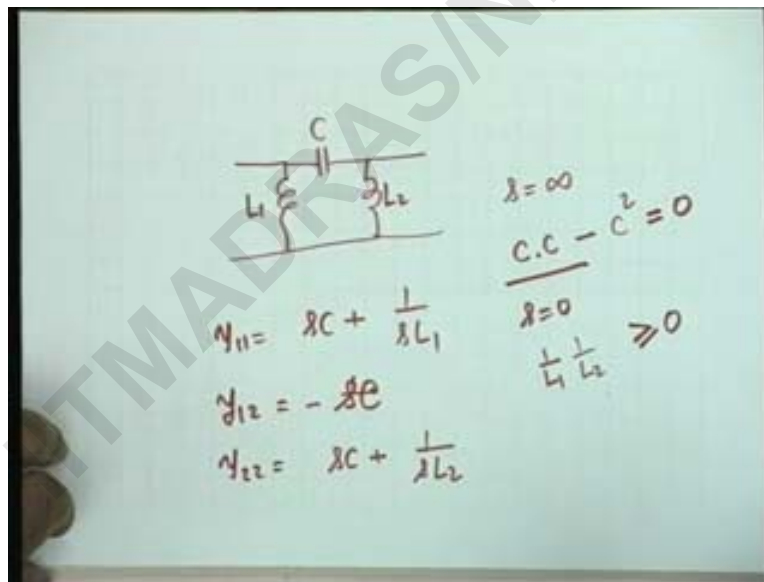
zero and this is called the residual condition as i said i cannot prove this in this class it is beyond the scope of this class but i can definitely illustrate by means of an example

[Noise] the restriction is that the network has to be two element kinds either LC or RC or RL okay then at all poles [Noise] okay as i said if Z_{12} has a pole it must be shared by Z_{22} and Z_{11} also but if Z_{11} has a pole it does not have to be shared by either Z_{22} or Z_{12} does that violate the residue condition

Z_{11} has a pole so K_{11} is non zero Z_{22} if it does not have a pole then K_{22} would be zero Z_{12} does not have a pole then K_{12} will be zero so it will be zero equal to zero it does not violate a residual condition

now let's take an example let's take the same example that we took no let's take a different example

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suppose we had we have L_{12} and C [Noise] which parameters tell me write down MY inspection

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Y parameters Y_{11} is equal to sC plus one over sL_1 is that okay is that okay

Y_{12} is equal to

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minus one over no minus sC minus sC don't forget the negative sign and Y two two is equal to sC plus one over sL two

now you notice that the residue a pole at s equal to infinity a pole that s equal to infinity is common to all the three parameters and at this pole the residues are K one one is C K two two is C and K one two is

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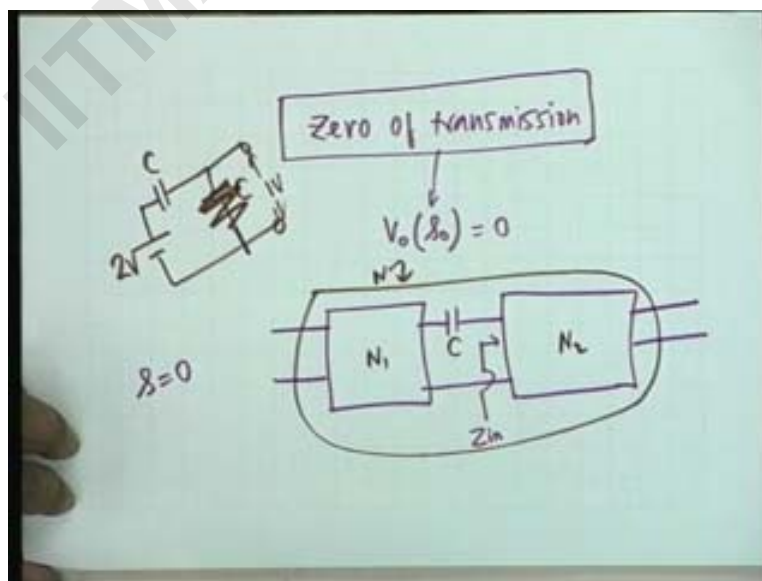
yes

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K one two is minus C and therefore minus C whole squared is C squared and K one one multiplied by K two two minus K one two squared is exactly equal to zero residue condition is satisfied

on the other hand for the pole at the origin pole at the origin what is K one one is one over L one K two two is one over L two and K one two is zero and therefore this is obviously greater than or equal to zero okay is a demonstration of the residue condition i could do this with ah with RC or RL networks also any question alright [Noise] next we introduce a term

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zero of transmission every obvious term nothing ah very special a zero of transmission of a two port network is the frequency at which there is no transmission as simple as that okay a zero of transmission is a frequency at which there is no transmission that is the output is equal to zero

if ah the output is a voltage let's say V zero then V zero at a zero of transmission s zero shall be equal to zero if the output is a current the current shall be zero okay

now [Noise] let's take some simple examples of zero of transmission simple examples on network to soak ah the idea of zero of transmission suppose we have a network which can be broken up into two sub networks connected by a capacitor

suppose this is my total network N which is broken up into two sub networks N one and N two and the capacitors C

obviously at DC at DC because of this capacitor there will be no transmission to N two so s equal to zero is a zero of transmission is that clear provided there is a hitch here provided if you measure this impedance Z in suppose Z in is that of a pure capacitor then what you have said is not true isn't it right no i have given this example earlier also yes

<a_side> ((sir if it was pure inductor)) (00:31:23) <a_side>

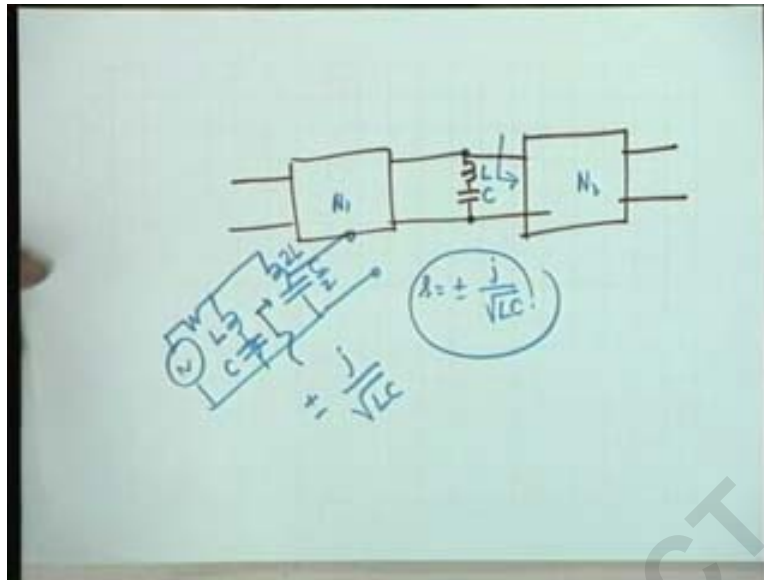
if it was pure inductor then also (()) (00:31:29) zero of transmission that will be now two zeros at s equal to zero if the input impedance is that of an inductor then obviously at s equal to zero inductor axis is short so the output voltage would be zero agreed

now the point that i was mentioning is if Z in is that of a capacitor

<a_side> (()) (00:31:52) <a_side>

if the input impedance is a capacitor then obviously s equal to zero is not a zero of transmission this you can very easily see i have given this example earlier also that if you have two capacitors in series and the voltage let's say two volt let the capacitors be identical then you will get a one volt here [Noise] it is not a zero of transmission but on the other hand if it is anything but a capacitor if anything but (()) (00:32:21) let's say resistance then obviously s equal to zero is a zero of transmission is that point clear okay similarly if we can break a network like this let's say ah [Noise]

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suppose a network N can be broken up into two sub networks N_1 and N_2 and connected by a shunt series resonant network then obviously $s = \pm \sqrt{j/LC}$ at this frequency at this two frequencies this axis a short circuit if it is a short circuit then obviously nothing will be transmitted to any two unless this exception must be remember unless the input impedance here is also a short circuit at this two frequencies

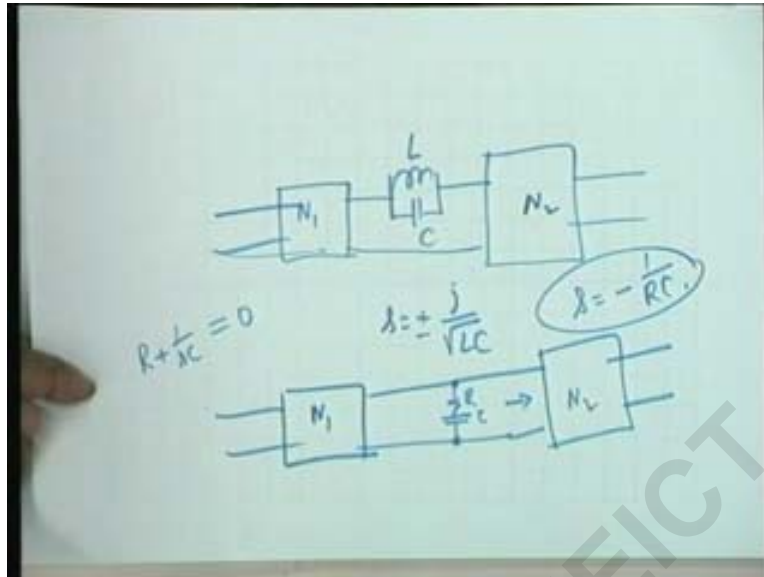
that is unless the network looking to the right has an input impedance which is also zero at this frequency if it is zero then there will occur current division between two short circuits okay current division between two so the zero of transmission shall not exist

<a_side> sir can you please explain <a_side>

can i please explain okay suppose i have a network like this suppose this is L and C this is two L and C by two okay now obviously at the frequency $s = \pm \sqrt{j/LC}$ this x is short and normally nothing should have been transmitted to the rest of the network but if by looking into the right by looking to the right if you have the pair of zeros is at the same frequency then obviously this is not a zero of transmission

that if if you measure the voltage across C by two example you will get a voltage why because there occurs a division of current between two short circuits at the frequency $s = \pm \sqrt{j/LC}$ is it point clear okay there can be many other examples of zero of transmission

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for example if we had a [Noise] a network like this L and C then at the frequency s equal to plus minus j by square root LC this parallel resonance circuit becomes infinite impedance and therefore it blocks transmission to N_2

so you had a zero we have a pair of zeros of transmission at plus minus j by square root LC alright similarly i can take examples of let's say RC let's if there is a network N_1 which has an RC series network in parallel then there is a network N_2 then the overall network has how many zeros of transmission due to RNC in along that two

if it is LC then plus minus j by square root LC here one at s equal to minus one over

<a_side> ((RC)) (00:36:11) <a_side>

RC correct [Noise] at this frequency this is a short and therefore that is a zero of transmission once again that qualification should be there that the impedance looking to the right of this should not also had a zero at the same frequency

if it does then of course that is not correct

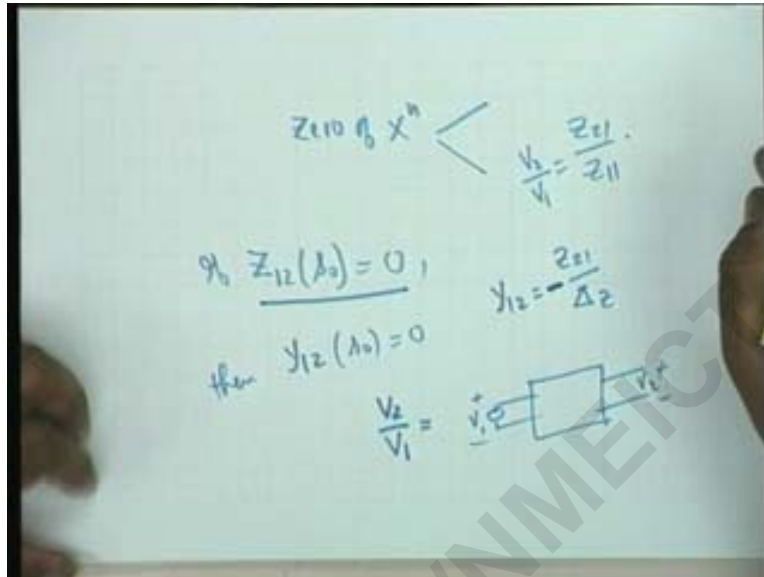
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pardon me

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no j here because this impedance this impedances is R plus one over sC and this will be zero when s equal to minus one by s no j alright okay now [Noise] Z of transmission

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depending on zero of transmission two kinds of networks

<a_side> (() (00:37:06) <a_side>

may ore may not be will come to this point a little later

zero of transmission for voltage and current may be different yes may be different but in general let let's since you raise the question let's answer this question in general if Z one two has a zero if Z one two has a zero then Y one two also has a zero at the same frequency can you prove this

if this is true then Y one two s zero is also equal to zero it {is} (00:37:50) it follows very simple because Y one two is equal to what is the relationship

<a_side> (() (00:37:57) <a_side>

Z two one by del Z is there negative sign

<a_side> (() (00:38:02) <a_side>

don't forget the negative sign so if Z two one is zero obviously Y one two is also zero in fact in fact if Z one two has a zero all transfer functions in general have a zero for example for example

suppose i want the open circuit voltage transfer function of a network of a two port open circuit voltage transfer function it can be expressed in terms of Z_{12} and what

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i have a network i connect a voltage here V_1 and i measure the voltage here V_2 what is the relations between V_2 and V_1

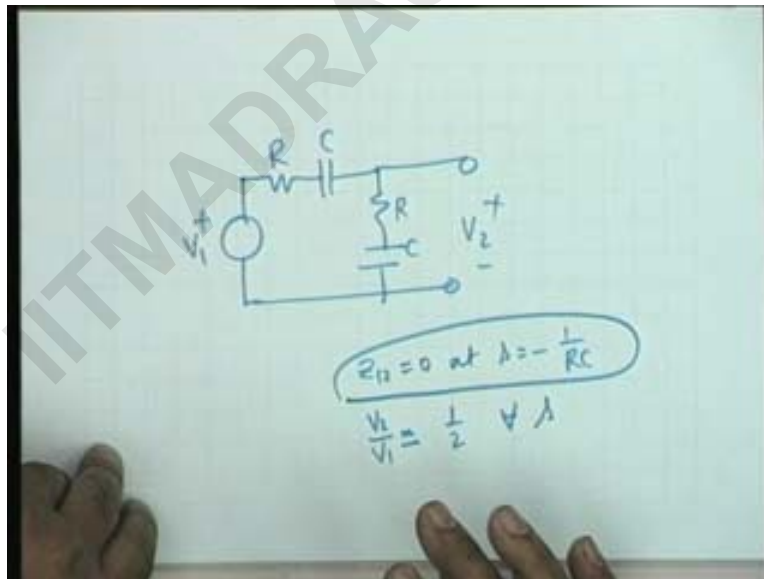
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Z_{21} by Z_{11} that is if you write the voltage equations and put I_2 equal to zero so you get V_1 equal to $I_1 Z_{11}$ and V_2 equal to $I_1 Z_{21}$ $I_1 Z_{21}$ the ratio is simply Z_{21} by Z_{11} therefore if Z_{12} has a zero obviously voltage transfer function can also have a zero not always there is a qualification required it should be obvious

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that's right Z_{11} should not have a zero then okay for example let's take a simple example

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let's say [Noise] an RNC in series and an RLC in shunt this is my V_1 and this is my V_2 obviously Z_{12} has a zero at s equal to

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minus one over RC but the transfer function V_2 by V_1 does not have a zero there

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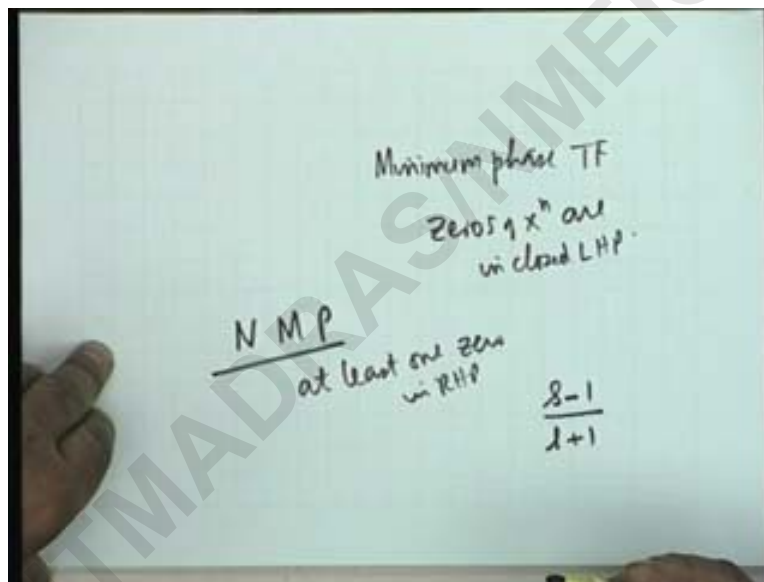
it is equal to one or

<a_side> ((half half)) (00:40:08) <a_side>

half at all s therefore a zero of Z one two is not necessarily shared by all other transfer functions but generally it is so unless there is cancellation generally it is so

so it suffices to consider in ordinary cases just Z one two or just Y one two alright is it point clear okay the other ah two terms that we have all ready introduced we would like recall at this point

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do you recall what is a minimum phase transfer function

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poles of any transfer function have to be in left half plane have to be they cannot be in the right half plane so it is the zeros minimum phase transfer function is one in which the zeros all transfer functions zeros are zeros of transmission isn't that right

so minimum phase transfer function is one in which the zeros of transmission are in the open or closed left half plane open or closed

<a_side> closed <a_side>

closed are in closed left half plane if the function has to be non minimum phase there must be at least one zero in the right half plane at least one zero at least one it can have more one zero in right half plane can you give me an example of a non minimum phase transfer function and all pass function first order all pass is of this form $s - 1$ divided by $s + 1$ the zero is in the right half plane the pole has to be in the left half planes

in addition if you recall all pass functions at the ((elegant)) (00:42:14) property that

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no

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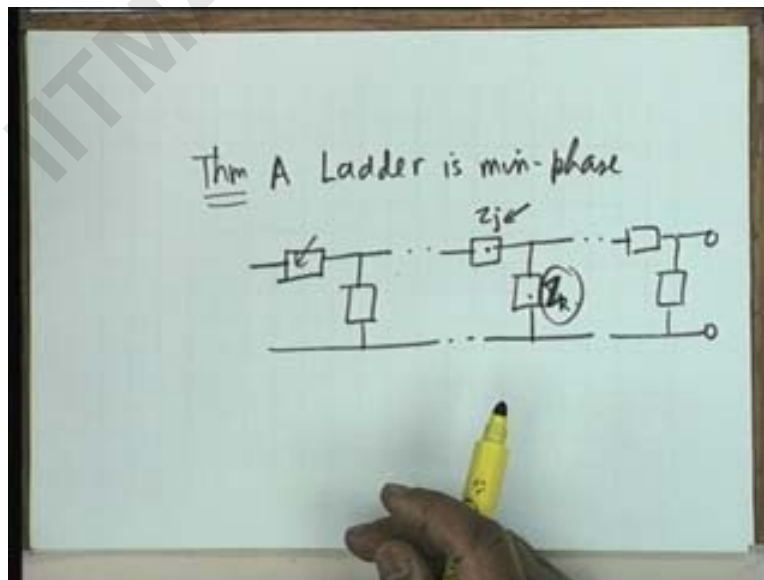
yes (()) (00:42:19) of course but the property in term of poles and zeros they are

<a_side> (()) (00:42:23) <a_side>

not symmetrical that's not the (()) (00:42:27) mirror image mirror image symmetry [Laughter] the symmetry is that of mirror image considering the $j\omega$ axis as a plane mirror right $j\omega$ axis is a mirror it has a mirror image symmetry

so minimum phase and non minimum phase and now we are going to state a theorem

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and the theorem is that if the network is a ladder if the network is a ladder alright you recall what is a ladder okay if the network is a ladder then it has necessarily to be minimum phase a ladder is minimum phase this is the theorem and the theorem can be proved very simply by common sense take a ladder take a ladder a ladder is like this [Noise] okay this is a typical ladder

a ladder is minimum phase all that you have to required to prove is that the zero of transmission of ladder is always in the left half plane poles no question poles have to be in the left half plane okay it's only the zero of transmission

now how can a ladder block transmission how can a ladder block transmission which is either two things can happen either a shunt element can be short circuit

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or a series a element can be an closed in circuit now a series element open circuit means what

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suppose an element Z_j is an open circuit which means that it has pole at that frequency right how can it be an open circuit at that point that frequency must be a pole of this impedance

similarly if you have a let's say Y_k [Noise] an admittance here let's put it a Z_k an impedance Z_k then

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zero can be created by zero of Z_k right and a ladder has to be made up of only impedances right and if these impedances have passive and reciprocal and therefore the poles and zeros of these impedances are in the left half plane agreed

which means that the transmission zeros of a ladder must all be in the left half plane there is no other way that is zero of transmission can be created in a ladder right it is either a series impedance pole now we state it in the formal language

a ladder the transmission zeros of a ladder are constituted by two kinds two kinds of frequencies frequencies at which the series impedances have a pole or shunt impedance have a zero and since any driving point impedance any driving point impedance has poles and zeros [Noise] at the left half plane

the transmission zeros of a ladder must be in the left half plane in other words a ladder must be a minimum phase are you convinced

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[Laughter] what what i saying is if it is to be minimum phase then it's zeros must be in a left half plane how can this zero be created either an impedance will be open series impedance where can it be open at it's poles and it's poles must be in the left half plane or a shunt impedance can be a short circuit

where can be it a short circuit at a zero where can it have zero in the left half plane and therefore all transmission zeros of a ladder must be in the left half plane

a question can a ladder have multiple transmission zeros

<a_side> ((yes sir)) (00:46:43) <a_side>

[Laughter] i am not finish the question anywhere anywhere in the in this plane can it have a multiple

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pardon me

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why not

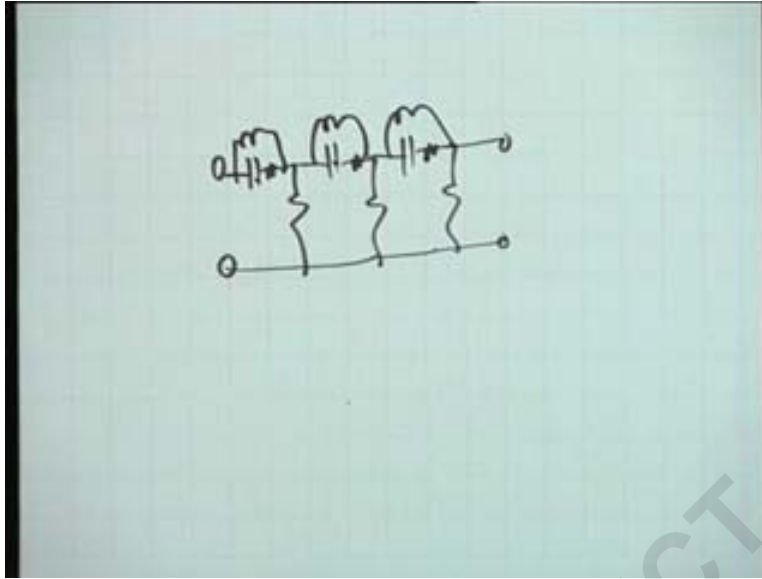
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anywhere because the zero of Z_j any impedance can be anywhere in the left half plane suppose this zero is this a pole is shared by another series impedance then there will be two zeros of transmission at the same frequency

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no they are they are quite separate from each other let me let me take an example

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you know this phase shifting network where are the zeros of transmission obviously at s equal to zero at DC if you have a voltage source here nothing will appear here

how many zeros of transmissions

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obviously three one due to this one due to this one due to this say it can have multiple zeros of transmission at any point to this s planes suppose we had a resistance here then obviously this zeros would have shifted to be negative real axis

suppose we had an L here then identical [Noise] then this zeros of transmission would have been complex alright therefore it is possible for a ladder to have multiple zeros of transmission anywhere in the s plane no not anywhere in the s plane

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in the left half in the closed left half plane okay can it have multiple poles transfer function can it have multiple poles

<a_side> ((no sir)) (00:48:35) <a_side>

not on the $j\omega$ axis it may [Laughter] have elsewhere on the $j\omega$ axis no no transfer functions can have multiple poles on the $j\omega$ axis okay will start from here tomorrow [Noise]