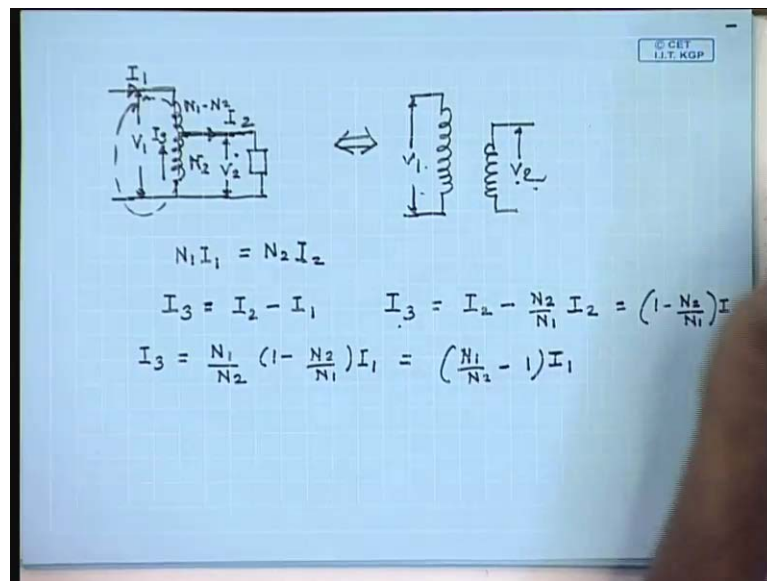


Electrical Machines- I
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Lecture - 17
Auto Transformers

You can recall that we introduced the concept of a 2 angle transformer through a inductive potential divider of this form.

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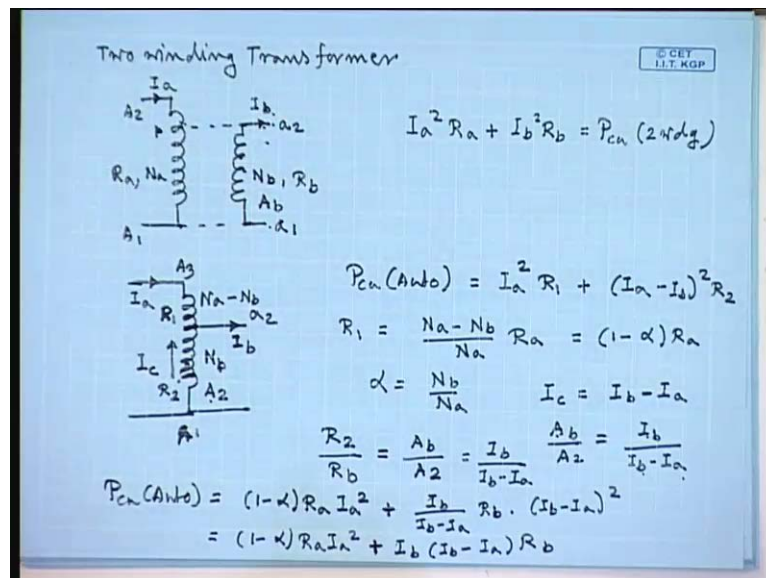
That is, if we give a input voltage of V 1 then we will get a output voltage of V 2, which is different from V 1 and from here we arrived at the concerto of 2 winding transformer showing that these 2 parts can be separated out unlike a resistive potential divider. The reason being the power transform for transfer from input to output, in this case occurs not only by the conductive path like this, but also by magnetic induction, by that we means when we apply a voltage here a flux is produced leaves both part of the coil, and when a load is connected here the current flowing through the load tries to change the flux as a result a reflection current is drawn from the primary side. A part of the power is transferred by the conductive path, but a part is transferred by the inductive part as well.

While therefore, if we say this current is I 1 this current is I 2 then and this current is I 3 then the phasor diagrams of I 1 I 2 I 3 can be drawn as follows, assuming negligible magnetization current, if we say this number of turns of this part is N 2 and this part is N

$1 - N_2$ then from balance of $N_m f$ we can say $N_1 I_1$ equal to $N_2 I_2$. So, that the net magnetization current is 0 in ideal transformer. Therefore, what is I_3 ? I_3 equal to I_2 minus I_1 . In other words I_3 equal to I_2 minus N_2 by N_1 into I_2 equal to 1 minus N_2 by N_1 into I_2 is same as or I_3 equal to N_1 by N_2 into $1 - N_2$ by N_1 I_1 equal to N_1 by N_2 minus 1 into I_1 . From this expression, we can see N_2 by N_1 is larger than 0 therefore, we can see that the current I_3 will be smaller than the current I_2 , that is because, the I_3 is the current due to induction, where as the rest of the current follows by conduction.

So, in a auto transformer power transfer takes place both by electrical conduction and magnetic induction, and hence certain advantages result. For example, if the turns ratio N_2 by N_1 is close to 1 then I_3 will be very small compared to I_2 and therefore, the current carrying capacity of this part of the winding will can be designed to be low and hence there is a possibility of considerable saving in the copper, which is a the advantage for this kind of a arrangement this is called a auto transformer. This advantage does not exceed exist in a 2 winding transformer, where the entire power transfer is by inductive method.

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Let us look at a few examples of the advantages of this auto transformer. For example, let us compare the losses in both cases for the 2 winding transformer, let us say this is the 2 winding transformer $A_2 A_1 a_2 a_1$. Let this current be I_a , this current be I_b , number

of turns here N_a , number of turns here N_b , resistance of this winding let us say is R_a , resistance of this winding is R_b therefore, the total copper loss in this 2 winding transformer will be $I_a^2 R_a + I_b^2 R_b$ equal to $P_{\text{copper loss in 2 winding}}$. Now, if we join this windings to form a auto transformer we can join this point to this and this point to this that this stepping being the point, where the voltage is same as the voltage between a_2 and a_1 then the operation of the transformer does not change. At the same operating condition, this is now call it $A_3 A_1$ and a_2 say the current is again I_b here now, this are there are N_b number of turns and these number of turns is $N_a - N_b$.

Let this current be I_a , in this case the power loss is $P_{\text{cu auto transformer}}$ is equal to $I_a^2 R_1 + I_c^2 R_2$, where R_1 is the resistance of this part of the winding and R_2 is the resistance of this part of the winding. Now, the current on the upper part of the auto transformer and that of the 2 winding transformer are same. Therefore, assuming same current density the conductor cross section in of the 2 winding transformer hv winding and upper part of the auto transformer are same. Hence, the resistances depend on the number of turns therefore, R_1 can be written as $(N_a - N_b) / N_a \times R_a$ let us call it that is $1 - \alpha$ R_a where α equal to N_b / N_a .

To calculate the resistance R_2 we note that the number of turns of the l_v winding of the 2 winding transformer and the number of turns of the lower part of the auto transformer are same; however, while the current in the l_v winding is I_b the current in the lower part of the auto transformer is I_c , where I_c equal to $I_b - I_a$. Now, again if we assume the current densities of this winding and in this part of the winding to be same, then the cross sectional area of the conductors on the l_v winding of the auto transformer and the l_v winding of the 2 winding transformer of the hv winding lower part of the auto transformer should be inversely proportional to the current carrying capacity. Hence, if we say that the conductor cross section here is A_b and the conductor cross section here is A_2 .

Then A_b / A_2 will be equal to the inversely proportional equal to $I_b / (I_b - I_a)$ that is $A_b / A_2 = I_b / (I_b - I_a)$, which is the current density of this winding should be equal to $I_b - I_a / A_2$, which is the current density in this part of the winding. Now, R_2 / R_b resistance is inversely proportional to the cross

sectional area R_2 by R_b equal to A_b by A_2 that is equal to I_b divided by I_b minus I_a . Hence, the total $I^2 R$ loss in the auto transformer will be P_{cu} auto equal to 1 minus $\alpha R_a I_a^2$ plus $R_b I_b^2$ is given by, I_b divided by I_b minus I_a into R_b into I_b minus I_a square equal to 1 minus $\alpha R_a I_a^2$ plus I_b into I_b minus $I_a R_b$ but, if we neglect the magnetization current.

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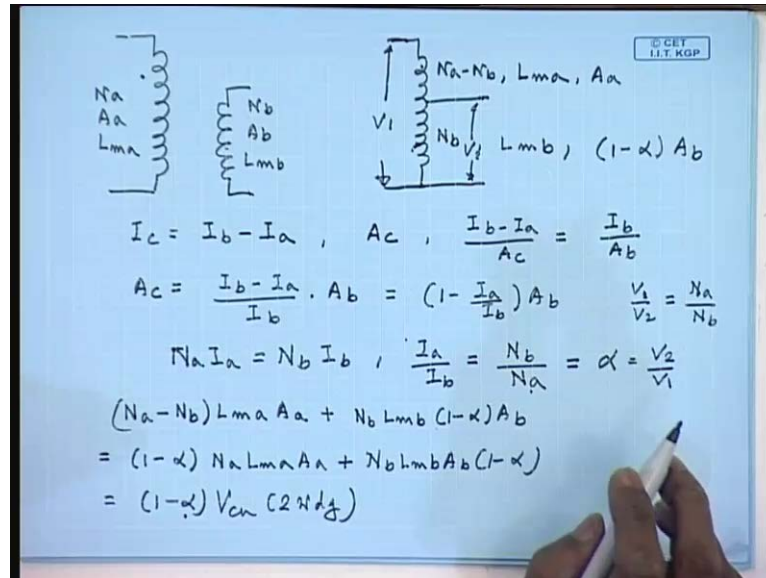
$N_a I_a = N_b I_b \quad \frac{I_a}{I_b} = \frac{N_b}{N_a} = \alpha$
 $\frac{I_b - I_a}{I_b} = 1 - \alpha \quad \text{or} \quad (I_b - I_a) = (1 - \alpha) I_b$
 $P_{cu}(Auto) = (1 - \alpha) R_a I_a^2 + (1 - \alpha) R_b I_b^2$
 $= (1 - \alpha) [R_a I_a^2 + R_b I_b^2] = (1 - \alpha) P_{cu}(2Wdg)$
 $A_a \rightarrow$ Cross section of H.V. Wdg of 2Wdg TxF
 $A_b \rightarrow$ " " " L.V. " " 2Wdg "
 $L_{m a} \rightarrow$ Mean length of Turn of H.V. winding
 $L_{m b} \rightarrow$ " " " " " L.V. winding
 $V_{cu}(2Wdg) = N_a L_{m a} A_a + N_b L_{m b} A_b$

Then $N_a I_a$ equal to $N_b I_b$ hence I_a by I_b equal to N_b by N_a equal to α therefore, I_b minus I_a by I_b equal to 1 minus α or I_b minus I_a equal to 1 minus α into I_b . Hence, the copper loss in the auto transformer should be equal to 1 minus α into $R_a I_a^2$ plus 1 minus $\alpha R_b I_b^2$ equal to 1 minus α into $R_a I_a^2$ plus $R_b I_b^2$, which is the power loss in the 2 winding transformer equal to 1 minus α into P_{cu} 2 winding. So, we see for the same rating, if the 2 winding transformer and the auto transformer are supplying the same load then the auto transformer will have lower loss not only that you'll find that the auto transformer will also use lower copper volume.

For that, let us define A_a to be the cross section of the of h v winding of the 2 winding transformer and A_b cross section of l v winding of the 2 winding transformer. Let $L_{m a}$ be the mean length of turn of H v winding and $L_{m b}$ mean length of turn of L v winding. When the total copper used in the 2 winding transformer V_{cu} 2 winding equal to copper used in the l v winding, which is N_a into $L_{m a}$ into A_a plus copper used in the l v

winding, which is $N_b L_m b A_b$. So, this is the volume of the copper used in the 2 winding transformer. Let us, now compute the volume of copper used in the auto transformer having the same k v a rating.

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For that, this is the 2 winding transformer, number of turns N_a , cross sectional area A_a , mean length at turn $L_m a$, number of turns N_b , cross sectional area A_b , mean length of turn $L_m b$ for the other transformer having the same k v a rating and the voltage rating. Number of turns here is N_b , number of turns here is N_a minus N_b , mean length of turn here let us say still $L_m a$ and here it is $L_m b$. Now, let us consider the cross sectional area this part of the auto transformer and the h v winding of the 2 winding transformer carrier the same current, if the 2 transformer have same k v a rating. Therefore, their cross sectional areas should also be same. So, this part as a cross sectional area of A_a ; however, the current carrying capacity of this part of the 2 winding of the auto transformer is I_c , which is I_b minus I_a whereas, for this it is I_b therefore, the current carrying capacity of the lower part of the auto transformer is I_c equal to I_b minus I_a .

So, if this part has a cross sectional area of A_c the current density is I_b minus I_a by A_c this should be same as the current density of the 1 v winding of the 2 winding transformers. So, this should be equal to I_b minus I_b by A_b . Therefore, A_c equal to I_b minus I_a by I_b into A_b 1 minus I_a by I_b into A_b , but we have seen for negligible magnetization current $N_a I_a$ equal to $N_b I_b$ hence I_a by I_b equal to N_b by N_a equal

to alpha. Therefore, the volume of the lower part of the auto transformer will be the cross sectional area of the lower part of the auto transformer will be $(1 - \alpha) A_b$. Hence, the volume of the copper in the auto transformer will be N_a minus N_b into L_m a A_a plus $N_b L_m$ b $(1 - \alpha) A_b$ equal to $(1 - \alpha) N_a L_m$ a A_a plus $N_b L_m$ b A_b into $(1 - \alpha)$ hence this is also equal to $(1 - \alpha)$ volume of copper in a 2 winding transformer.

Hence, see that for the same k v a rating the auto transformer will give lower losses as well as will use lower copper volume; however, as we have mentioned in the beginning it will not provide electrical isolation between the 2 sites therefore, where the electrical isolation is necessary we cannot use a auto transformer but; however, if the electrical isolation is not very important it is advantageous to use auto transformer particularly when the quantity alpha that is N_b by N_a which incidentally is also the voltage ratio if this voltage is V_1 and this voltage is V_2 then we know V_1 by V_2 equal to N_a by N_b . So, alpha equal to V_2 by V_1 , so if the quantity V_2 by V_1 that is the voltage combustion ratio is close to unity then this quantity $(1 - \alpha)$ is almost 0.

Hence, there will be a large saving in copper and also a large saving in losses. Hence, if the requirement of electrical isolation is not very important and the voltage combustion ratio is close to unity then it is advantageous to use a auto transformer rather than a 2 winding transformer. Generally auto transformers are suitable for a value of alpha between 1 to 0.5.

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$$\frac{E_{bc}}{E_{ab}} = \frac{N_b}{N_a - N_b}$$

$$E_{bc} = Z_{bc} I_c + V_L$$

$$V_L = I_b Z_L$$

$$V_a = I_a Z_{ab} + E_{ab} + V_L$$

$$V_a = I_a Z_{ab} + \left(\frac{N_a - N_b}{N_b}\right) E_{bc} + V_L$$

$$= I_a Z_{ab} + \frac{(N_a - N_b)}{N_b} [Z_{bc} I_c + Z_L I_b] + Z_L I_b$$

$$V_a = I_a Z_{ab} + \left(\frac{N_a}{N_b} - 1\right) [Z_{bc} (I_b - I_a) + Z_L I_b] + Z_L I_b$$

$$= I_a \left[Z_{ab} + \left(\frac{N_a}{N_b} - 1\right) \left(\frac{I_b}{I_a} - 1\right) Z_{bc} + \frac{N_a}{N_b} \cdot \frac{I_b}{I_a} Z_L \right]$$

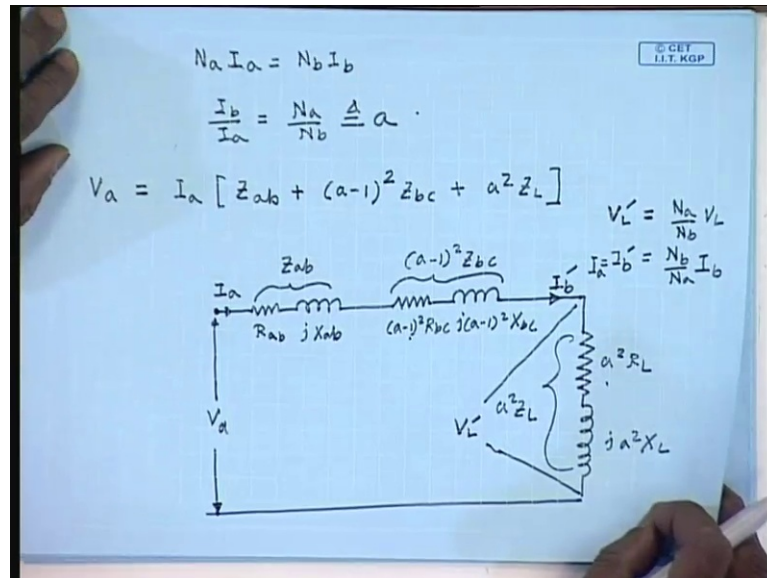
Now, that we know about the advantages of a auto transformer let us pay our attention to analyses of an auto transformer how do I analyse a auto transformer. For that, let us assume that this auto transformer is supplied with a voltage of V_a on the h v site draws a current of I_a here and the output is taken from here supplies to a load Z_L ((Refer Time: 27:27)) load for the time being we will assume with a current of I_b this point let us call it a this b this c.

This current is I_a this current is I_b this current is I_c and the load voltage here is V_L , the number of turns in this section is N_b and in this section is N_a minus N_b . Therefore, we can write its just to be noted that the coil of a auto transformer is on a magnetic core on hence the both the parts of the winding brings the same magnetization flux therefore, we can write that E_{bc} that is the voltage induced in the part it turns N_b divided by E_{ab} is equal to N_b divided by N_a minus N_b and they will also be in phase from k b l we can write the induced voltage E_{bc} equal to the leakage impedance of this part $E_{bc} Z_{bc}$ into the current I_c plus load voltage V_L , where V_L equal to I_b into Z_L . Similarly, we can write the applied voltage V_a to be equal to the drop across the leakage impedance of the section $A b$ that is I_a into Z_{ab} plus the induced voltage in the section $A b$ that is E_{ab} plus the load voltage V_L .

Now, substituting from above equations we can write V_a equal to $I_a Z_{ab}$ plus N_a minus N_b by N_b into E_{bc} that is what E_{ab} is plus V_L on further substitution we get

equal to $I_a Z_{ab} + N_a - N_b \text{ by } N_b \text{ into } Z_{bc} I_c + Z_L I_b + Z_L I_b$ or V_a equal to $I_a Z_{ab} + N_a - N_b \text{ by } N_b - 1 \text{ into } Z_{bc} I_c$ equal to $I_b - I_a$ plus $Z_L I_b$ into $N_a - N_b \text{ by } N_b + 1$. This can be written as, I_a into Z_{ab} plus $N_a \text{ by } N_b - 1$ into I_b by $I_a - 1$ into Z_{bc} plus $N_a \text{ by } N_b$ into I_b by $I_a Z_L$.

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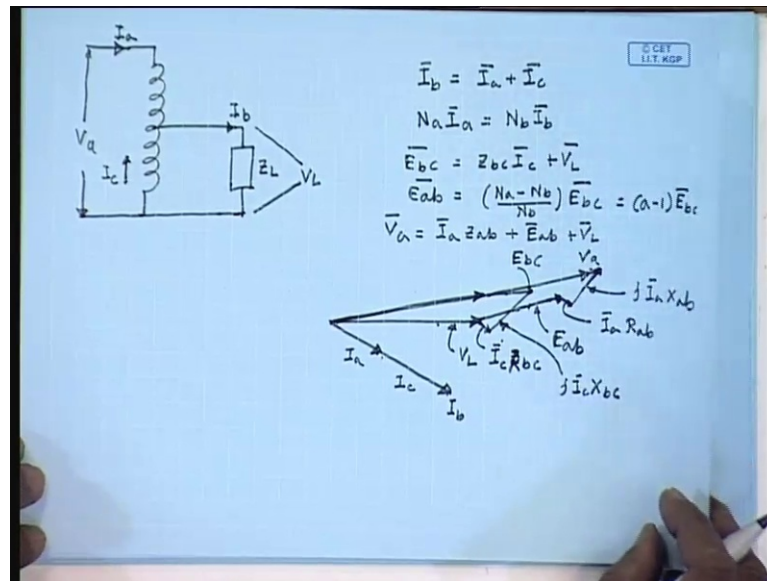


Again, if we neglect the magnetization current of the auto transformer we can write $N_a I_a$ equal to $N_b I_b$ or I_b by I_a equal to N_a by N_b let us define this quantity to be a , this is also same as the open circuit voltage of the auto transformer. Hence, we can write V_a to be equal to I_a into Z_{ab} plus $a - 1$ square into Z_{bc} plus a square into Z_L . Hence, the equivalent circuit of the auto transformer can be drawn as this is R_{ab} this is jX_{ab} , where this quantity is Z_{ab} this is $a - 1$ square R_{bc} this is $a - 1$ square jX_{bc} hence this part is $a - 1$ square Z_{bc} this is a square R_L this is j a square X_L . Hence this quantity is a square Z_L this is the referred load voltage V_L dash and this is the referred load current I_b dash. What is the relationship between V_L dash and I_b dash? V_L dash equal to multiplies by the turns ratio that is N_a by N_b into V_L and I_b dash equal to N_b by N_a into I_b .

So, that V_L dashed I_b dashed equal to $V_L I_b$. This is also same as I_a since we have neglected the magnetization current. So, this equivalent circuit is similar to that of a approximate equivalent circuit of a 2 winding transformer except that for the lower part of the auto transformer we will have to use the turns ratio as $a - 1$ rather than a . For

a 2 winding transformer with the same number of turns it would have been a square into the leakage impedance of this part. Now, that tells that not only a auto transformer we will have lower loss and lower copper volume it will also have much lower leakage inductance or leakage reactance hence the voltage regulation of a auto transformer will also be better compared to a 2 winding transformer. How do you draw a phasor diagram for this auto transformer for that, let us draw the auto transformer again.

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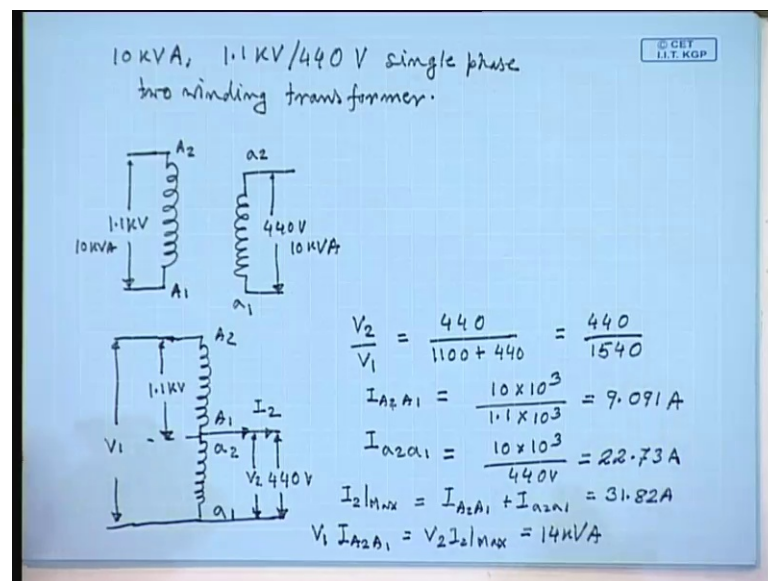


This is the voltage V_a current I_a and let us say we are drawing load current I_b to a load impedance Z_L , which we will assume to be inductive and this is the voltage V_L . So, let this be the phasor of the load voltage V_L and since this is lagging impedance this is an inductive load the current I_b will be lagging V_L by the power factor angle. So, this is the current I_2 or I_b the current I_a and I_c are in phase with I_b ; however. So, this is the current I_b the current I_a is a fraction of I_b because for the current relations we are I_b equal to I_a plus I_c and also $N_a I_a$ equal to $N_b I_b$, if you neglect the magnetization current. So, this is the current I_a and the rest is the current I_c .

Now, from the first equation that is E_{bc} equal to $Z_{bc} I_c$ plus V_L we can get the phasor E_{bc} , which will be this is the phasor E_{bc} , but we know E_{ab} equal to N_a minus N_b by N_b into E_{bc} equal to $\alpha - 1$ to E_{bc} . Since auto transformers are normally used with α less than 2 E_{ab} will be in phase with E_{bc} , but of smaller magnitude. Now, let us use the other equation that is V_a equal to $I_a Z_{ab}$ plus E_{ab}

plus V_L this is E_{bc} , a will be in phase with E_b , but of smaller magnitude. So, let us assume this is E_{ab} this is V_L plus E_{ab} plus I_a is in phase with I_b $I_a R_a$ plus $j I_a X_a$. Hence, this will be the phasor V_a , this is the phasor E_{bc} this is the phasor E_{ab} this is the phasor V_L this phasor is $I_c Z_{bc}$ R_{bc} this phasor is $j I_c X_{bc}$. Similarly, this phasor is $I_a R_a$ and this phasor is $j I_a X_a$. So, this will be the phasor diagram of the auto transformer. Now, let us solve the problem concerning the auto transformer to understand whatever has been taught so far.

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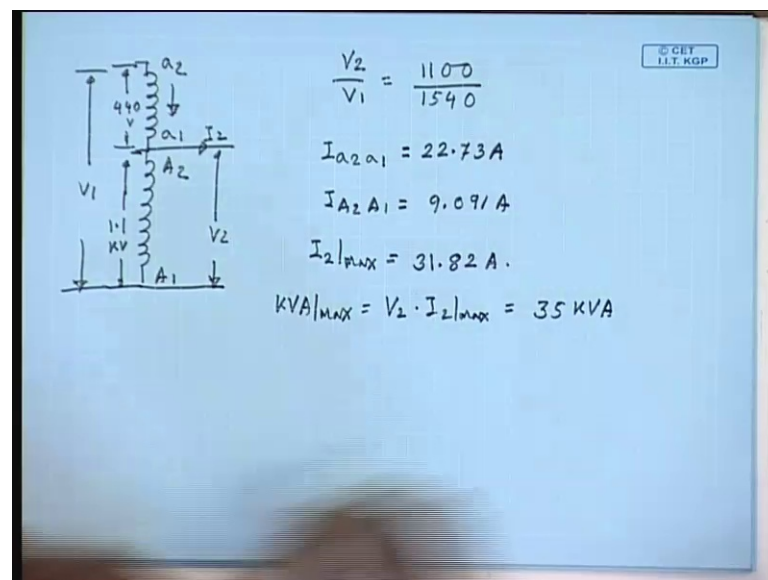


For that, let us take this example you have a 10 k v a 1.1 k v by 440 volt single phase 2 winding transformer. So, this is the 2 winding transformer, this is $A_2 A_1$ this is $a_2 a_1$ this rated voltage is 1.1 k v, 10 k v a relative voltage here is 440 volt again the k v rating is 10 k v a, if you wish to connect it in terms of an auto transformer what are the different possible connection. Obviously, there are 2 possibilities 1 is this is the part $A_2 A_1$ connected in series with the smaller part $a_2 a_1$ and we take the output from here. So, what will be the voltage ratio here the maximum voltage that can appear and this site is 440 volt. The maximum voltage that can appear here is 1.1 k v hence, the voltage ratio V_1 by V_2 or V_2 by V_1 here can be 440 divided by 1100 plus 440 equal to 440 divided by 1540 this is the voltage conversion ratio. What will be the current carrying capacity? The current carrying capacity of the section $A_2 A_1$ is $I_{A_2 A_1}$ equal to 10 k v a 10 into 10 to the power 3 divided by 1.1 k v this comes to 9.091 amperes. The current carrying

capacity of the section a2 a1 will be $I_{a2 a1}$ that part it is again 10 k v a because we have joined these 2 in series.

So, their current carrying capacity do not change divided by 440 volt this comes to 22.73 amperes. Therefore, the maximum value of the current output current I_2 I_2 max will be the sum of these 2 this should be equal to 31.82 amperes. Hence, the k v a rating will be $V_1 I_{A2 A1}$ equal to $V_2 I_2$ max this comes to about 14 k v a hence when I connect a 2 winding transformer the 2 as an series I get a auto transformer whose k v a rating increases to 14 k v a there's another connection possible, where the section a2 a1 is connected on the top.

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And the section capital a2 a1 is connected on the bottom in this that is here a2 a1 and here A2 A1 this part has a, and the output is taking across the high voltage winding. So, this part has a rated voltage of 1.1 k v and this part has a rated voltage of 440 volts. Hence, here the voltage conversion ratio will be here the V_2 by V_1 equal to 1100 divided by 1540 going by the same logic. Similarly, if the current carrying capacity here $I_{a2 a1}$ is equal to 22.73 amperes whereas, the current carrying capacity $I_{A2 A1}$ is 9.091 amperes means I_2 max in this case also equal to 31.82 amperes now the k v maximum k v a that is V_2 into I_2 max comes to about 35 k v a.

So, a 10 k v a 2 winding transformer can supply 35 k v a when connected as the auto transformer it is easy to see here the value of alpha was much lower than 1 hence the

increase in the k v was not all that great here the value of alphas is equals to 1 hence we get almost 3.5 times increase in the k v a rating of the auto transformer.

Thank you.