

Electrical Machines - I
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Lecture - 38
Speed Control of DC Series Motors

In the last class, we have seen how to apply dynamic braking to a DC series motor. We have mentioned that although it is possible to apply dynamic braking in a DC series motor by reversing the field terminal and connecting a braking resistance at the terminal of the machine. The problem is as the machine speed goes down the braking torque also reduces. This problem can be overcome using a chopper and we will see through an example how it is done.

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220V, 70 A DC Series Motor
 $r_a + r_{sc} = 0.12 \Omega$
 O.C.C. at 600 RPM.

I_A	10	20	30	40	50	60	70	80
V	64	118	150	170	184	194	202	210

$0.1 \leq \delta \leq 0.9$
 $R_B = ??$ at $I_a = 70 \text{ A}$, $N = 800 \text{ RPM}$.

For that let us assume that a DC series motor the following rating 220 volt, 70 ampere motor, the combined resistance r_a plus r_{sc} equal to 0.12 ohm, and the O C C at 600 R P M is given by the following data . 10, 63, 20, 40 ampere, this is the O C C at 600 R P M . Now, you want to break this, this is series motor using dynamic braking and the chopper. The chopper duty ratio changes from. So, what should be the value of R B. So, that at I a equal to 70 ampere. The motor and the braking region the motor speed is maximum motor speed is 800 R P M.

For that what should be the braking resistance R B. From the magnetization data we find

that for N equal to for I a equal to 80 and speed equal to 60. The back unit is 210 therefore, at I a equal to same 70 ampere and back e m f and speed is equal to 800 R P M. We can find out the back e m f, N equal to 800 R P M, I a equal to 70 ampere.

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$$N = 800 \text{ RPM}, I_a = 70 \text{ A}, E = ??$$

$$N = 600 \text{ RPM}, I_a = 70 \text{ A}, E = 202 \text{ V}$$

$$E|_{800} = \frac{800}{600} \times 202 = 269.33 \text{ V}$$

$$E = (r_a + r_{se} + \delta R_B) I_a$$

$$\therefore r_a + r_{se} + \delta R_B = \frac{269.33}{70}$$

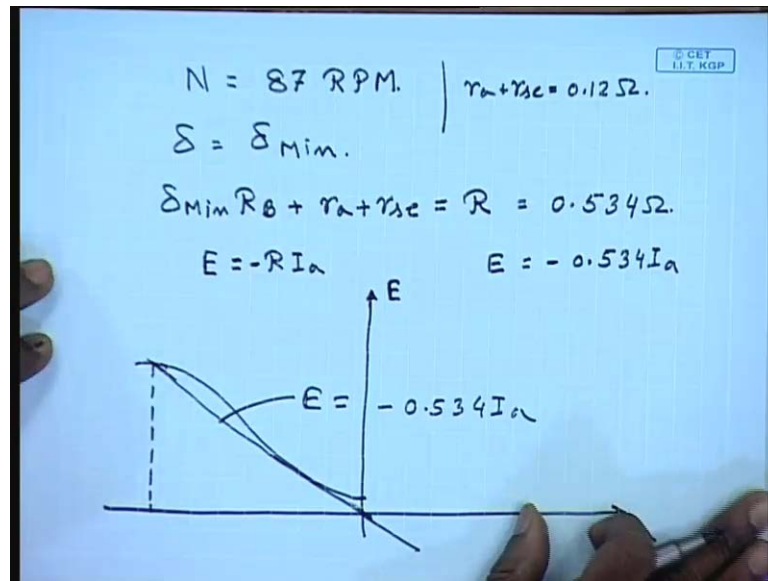
$$\delta R_B = 3.73 \Omega$$

$$\delta_{\text{max}} R_B = 3.73 \Omega, \delta_{\text{max}} = 0.9$$

$$R_B = 3.73 / 0.9 = 4.14 \Omega$$

First we have to find out, what is E. The given data is N equal to 600. I a equal to 70 ampere. E equal to 202 volts therefore, E at 800 will be equal to 800 by 600 into 202, 269.33 volts. So, in the regenerative braking we know that E equal to r a plus r s e plus delta R B. So, into I a term r a plus r s e plus delta R B comes to 269.33 divided by 70 or delta R B equal to 3.73 ohm. Now at maximum speed we will keep delta equal to at its maximum value. So, delta max R B equal to 3.73 ohm or delta max equal to 0.9 therefore, R B equal to 3.73 divided by 0.9 this gives me 4.14 ohm.

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Now, suppose with this braking resistance let us try to find out what is the maximum torque we can get with this chopper when the speed goes down to N equal to 87 R P M. Now as the speed goes down we also reduce the effective resistance then at lower speed we will operate at δ equal to δ_{min} . So, the total $\delta_{\text{min}} R_B$ will be the effective resistance plus r_a plus r_{sc} will be the braking resistance R . This will come to 0.534 ohms as r_a plus r_{sc} is given as. Also E equal to $R I_a$. So, if we plot from the given data at 600 R P M we can plot the E versus I_a at 87 R P M, and then also plot E equal to this is has to be taken in the reverse direction because current has reversed minus $0.534 I_a$ and find out the intersection point turns out. At the intersection point I_a comes out to be approximately 50 ampere.

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$I_a = 50 \text{ A}$
At $I_a = 50 \text{ A}$,
$$K\phi = \frac{184}{\frac{2\pi \times 600}{60}} = 2.928$$

$$T = K\phi I_a = 2.928 \times 50$$

$$= 146.4 \text{ Nm.}$$

So, at 50 ampere from the given data, we have E equal to 184 volts at 600 R P M. So, K phi at I a equal to 50 ampere, K phi equal to 184 volts divided by 600 2 pi into 600 by 60 this comes to 2.928 therefore, T equal to K phi I a equal to is 146.4 newton meter . So, we can still generate so much torque at a reduced speed of just 87 R P M. So, we can also apply regenerative braking and let us see during regenerative braking what kind of torque we can expect.

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$V_t = 220 \text{ V}$, CHOPPER Driven.
 $N = ??$ when $\delta = 0.5$, $T_B = T_{\text{rated}}$.
at $T = T_{\text{rated}}$, $I_a = I_{a_{\text{rated}}} = 70 \text{ A}$
$$E = \delta V_t + I_a (r_a + r_{se})$$

$$= 0.5 \times 220 \text{ V} + 70 \times 0.12 = 118.4 \text{ V}$$

 $I_a = 70 \text{ A}$, $N = 600 \text{ RPM}$, $E = 202 \text{ V}$
$$N = \frac{118.4}{202} \times 600 = 351.7 \text{ RPM.}$$

So, let us say this same machine is supplied from a V t of 220 volts through a chopper

and chopper driven. So, what should be the motor speed when delta equal to 0.5 and braking torque equal to T_{rated} . Now at rated motor torque at $T = T_{rated}$ whether it is motoring operation or braking operation I_a will be equal to I_a rated. This is 70 ampere. So, what is E now it is braking operation. So, E equal to δV_t plus I_a into r_a plus r_s e that is equal to 0.5 into 220 volts plus 70 into 0.12 this comes to 118.4 volts.

From the magnetization characteristics we know that at I_a equal to 70 ampere and N equal to 600 R P M. E is equal to 202 volts. So, if E is to be 118.4 volts at the same armature current then the speed must be. So, even at this speed the regenerated braking torque equal to the maximum rated motor torque can be produced using a chopper.

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$$V_t = 220 \text{ V, CHOPPER Driven.}$$

$$N = ?? \text{ when } \delta = 0.5, T_B = T_{rated}.$$

$$\text{at } T = T_{rated}, I_a = I_{a \text{ rated}} = 70 \text{ A}$$

$$E = \delta V_t + I_a (r_a + r_{se})$$

$$= 0.5 \times 220 \text{ V} + 70 \times 0.12 = 118.4 \text{ V}$$

$$I_a = 70 \text{ A, } N = 600 \text{ RPM, } E = 202 \text{ V}$$

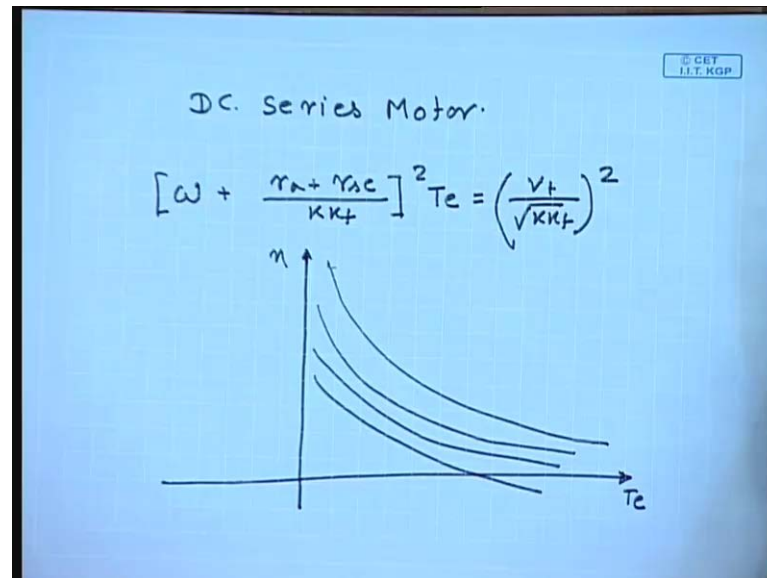
$$N = \frac{118.4}{202} \times 600 = 351.7 \text{ RPM.}$$

Now, also let us try to find out what is the maximum motor speed if I want that I_a to be same 70 ampere and if delta max is equal to 0.95 what is the maximum motor speed. At 70 ampere please note that it will still generate the rated braking torque because the current is rated. So, what is E , E equal to δ_{max} into V plus I_a into r_a plus r_s e 0.95 into 220 plus 70 into 0.12 this comes to 217.4 volts.

Now, for I_a equal to 70 ampere, N equal to 600 R P M, E equal to 202 volt. And I_a equal to 70 ampere and E equal to 217.4 volts, then N should be equal to 217.4 by 202 into 600 equal to 645.7 R P M. So, we see that 645.7 R P M we have a armature current of 70 ampere. The duty cycle of 0.95 the motor produces rated braking torque. also at 351 R P M we can reduce delta to 0.5 and still obtain rated regenerative braking torque.

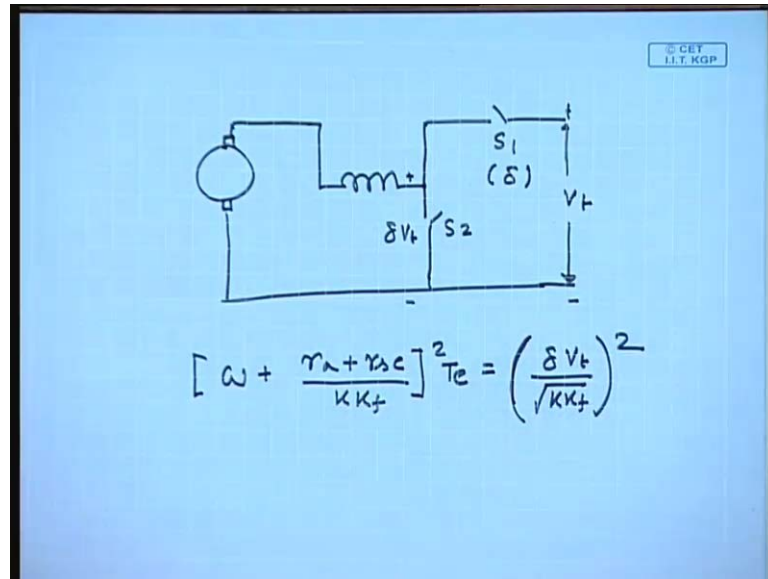
In fact, delta can be reduced further then even at a lower speed equal amount of regenerative braking torque can be obtained by using a chopper. In fact, choppers can be used for speed control of DC series motor.

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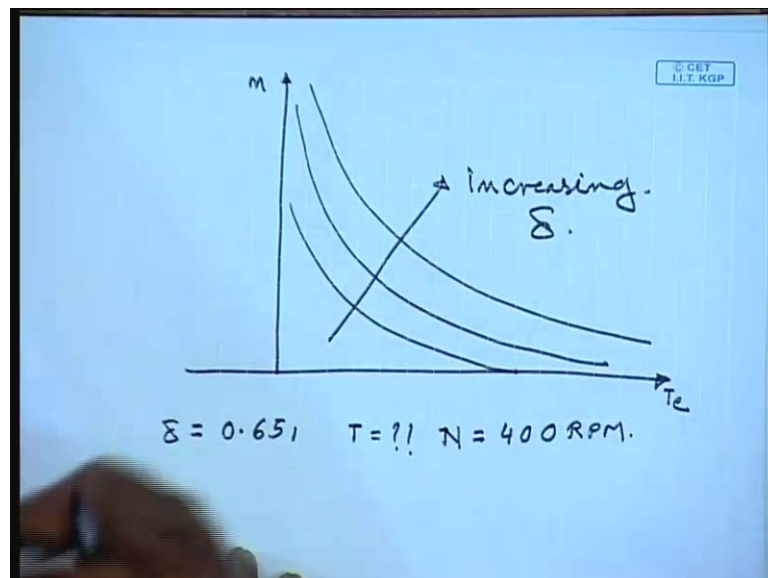
So, you know for DC series motor, the torque speed characteristics is given by. In order to this torque speed characteristics looks for constant r_a and V_t its looks like this. there are two ways to change this, one is to change the armature resistance with increasing armature resistance I can reduce the lower the torque speed characteristics; however, we as we know this is involves lot of loss in the additional armature resistance. Another more efficient method will be to control V_t and this V_t can be controlled by using a chopper.

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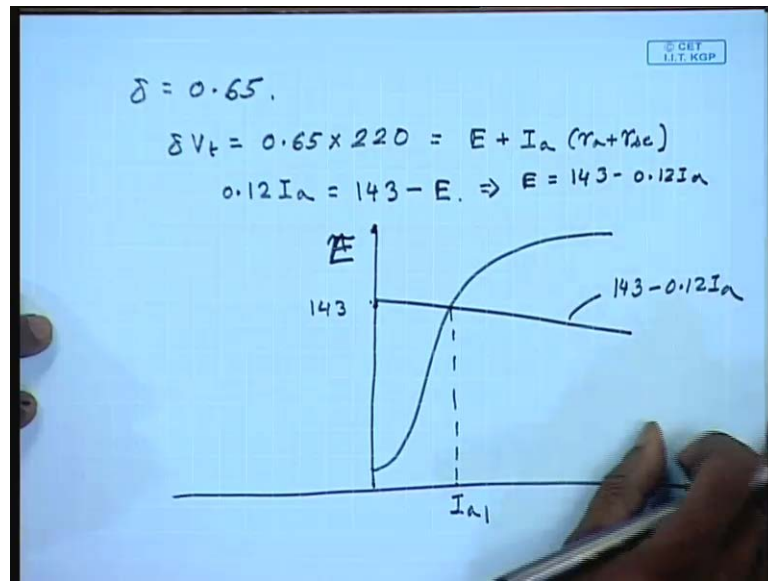
So, if we fit the DC series motor from a chopper, and this is one operates at the duty ratio of delta then the terminal voltage here will be delta V t and the torque speed characteristics will be given by... Hence by changing delta this is increasing delta.

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So, let us see through a problem the quantitative effect the same motor that we have been using now let us try to find out, if I set a delta equal to 0.65 then what should be the torque for N equal to 400 RPM.

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So, with delta equal to 0.65 delta V t equal to 0.65 into 220, and this should be equal to E plus I a, r a plus r s e or 0.12 I a equal to 143 minus E . So, we can find out where this intersection point will be, at N equal to 400 RPM. We are given the O C C at 600 RPM. These will we can scale to 400 RPM and on this we can plot. So this is 143 this will be intersection point I a 1. This I a 1 this is 143 minus 0.12 I a, this gives I a approximately equal to 70 amperes.

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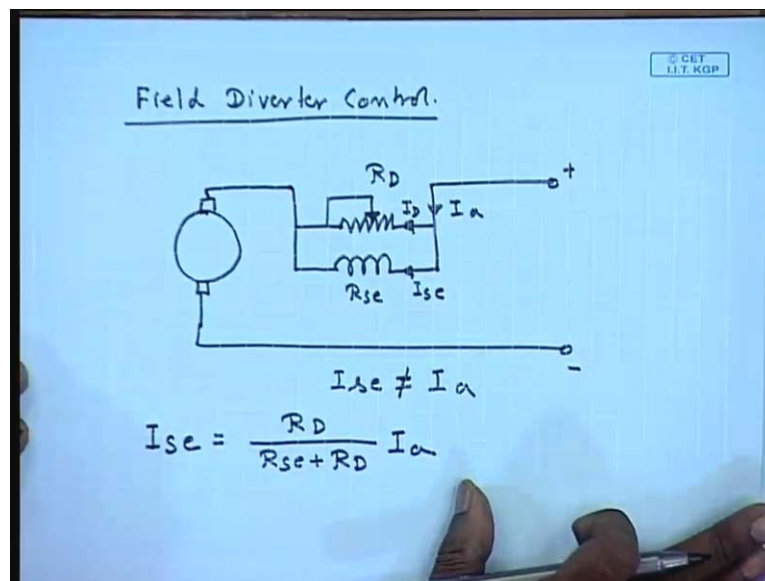
$I_a = 70 \text{ A}, E = 134.667 \text{ V}$
 $T = \frac{E I_a}{\omega} = \frac{134.667 \times 70}{\frac{2\pi \times 400}{60}}$
 $= 225 \text{ N-m.}$

And also gives a E of 134.667 volts. Torque will be equal to E I a by omega that is one

134.667 into 70 RPM. Please remember this should be O C C at 400 RPM not 600 RPM. 2π into 400 by 60 this comes to 225 Newton meter. So, given the delta and speed we can find out the torque or if we given the delta or current we can find out the speed. So, chopper control is an effective method of controlling the speed of a DC series motor efficiently.

However if we do not this has to be remembered that this chopper which is connected to the machine terminal has to carry the whole machine current. So, the switches that are used in this chopper should be designed to withstand the full current of the machine this makes the system of speed controls somewhat expensive there are other simpler method of controlling the speed of DC series motor in which case we can see that we can also control the value of $k k f$ in the equation of torque speed characteristics in order to control the speed of a DC series motor. There are several methods for doing this one is called the field diverter control.

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In this what we do is that, the field is shunted by a variable diverter resistance R_d . If this is R_{se} and the total current is I_a then there in there is current I_d and I_{se} . So, once you place a diverter by adjusting the value of R_d we can adjust the value of I_{se} , and I_{se} in this case will not be is not equal to I_a . We can also find out what will be the value of I_{se} . I_{se} equal to R_d divided by R_{se} plus R_d into I_a . For in which case the torque speed characteristics will also change because E equal to $K \phi I_a$ equal to $K k f, I_{se}, I_a$.

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$$E = k \phi_f I_a \omega$$
$$= k k_f I_{se} I_a \omega$$
$$I_{se} = \frac{R_D}{R_{se} + R_D} I_a = \alpha_d I_a$$
$$E = k k_f \alpha_d \omega I_a$$
$$V_t = E + (r_a + R_{D||R_{se}}) I_a$$
$$V_t = [k k_f \omega \alpha_d + (r_a + R_{D||R_{se}})] I_a$$
$$R_{D||R_{se}} = \frac{R_D R_{se}}{R_D + R_{se}} = \alpha_d R_{se}$$

Now, we have I_{se} equal to R_d divided by R_{se} plus R_d into I_a . Let us call it $\alpha_d I_a$ therefore, E equal to $k k_f \alpha_d$, this is ω . ωI_a V_t equal to E plus now r_a plus R_d parallel R_{se} into I_a . So, V_t equal to... Now R_d parallel R_{se} is equal to $R_d R_{se}$ divided by R_d plus R_{se} this is equal to $\alpha_d R_d$ or rather $\alpha_d R_{se}$.

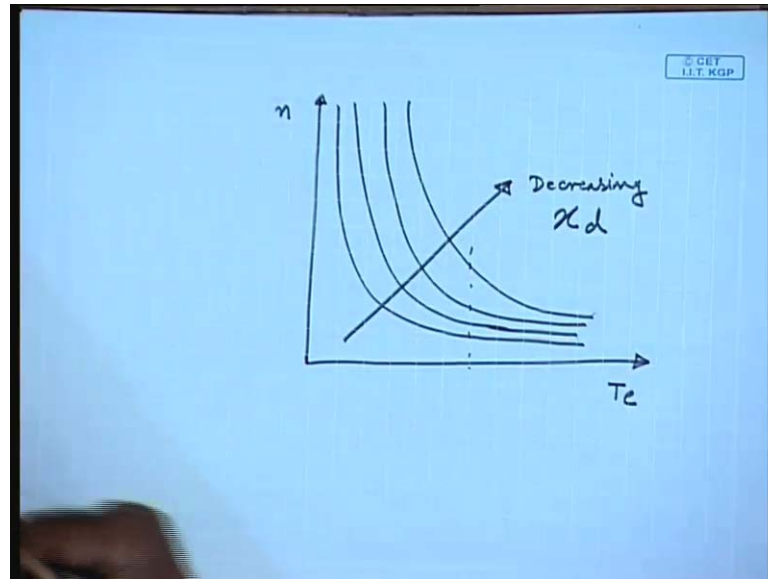
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$$V_t = [k k_f \alpha_d \omega + (r_a + \alpha_d R_{se})] I_a$$
$$[\alpha_d \omega + \frac{r_a + \alpha_d R_{se}}{k k_f}] I_a = \frac{V_t}{k k_f}$$
$$T_e = k \phi_f I_a$$
$$= k k_f \alpha_d I_a^2$$
$$T_e = \frac{k k_f \alpha_d V_t^2}{[k k_f \alpha_d \omega + (r_a + \alpha_d R_{se})]^2}$$

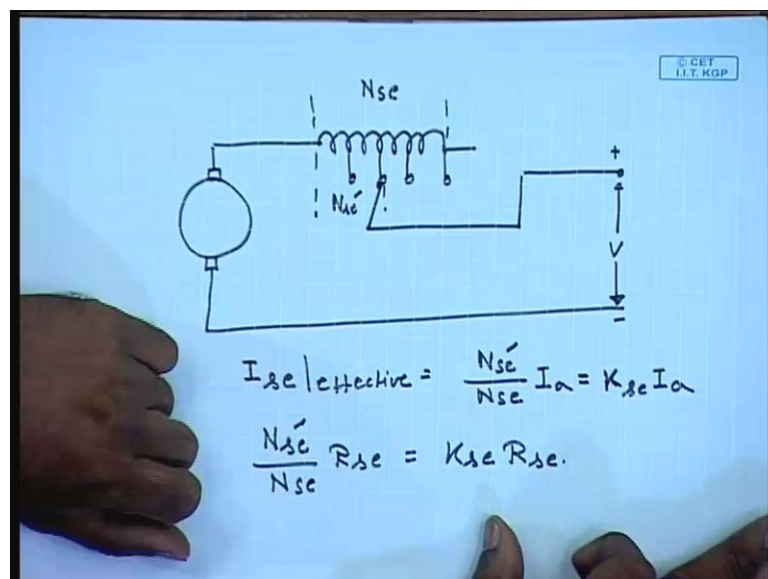
Therefore V_t equal to, so current speed characteristics now will be ... And the torque speed characteristics will be T_e equal to $k \phi_f I_a$ equal to $k k_f \alpha_d I_a^2$ T_e equal to ...

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We draw these torque speed characteristics it will look somewhat like, this is decreasing $x d$ that is this amounts to weakening the series field. So, we know that for the same torque if the field is weakened the speed increases. There are another method on somewhat the same line is called the tapered field control, in which tapped field control, in which there are several taps.

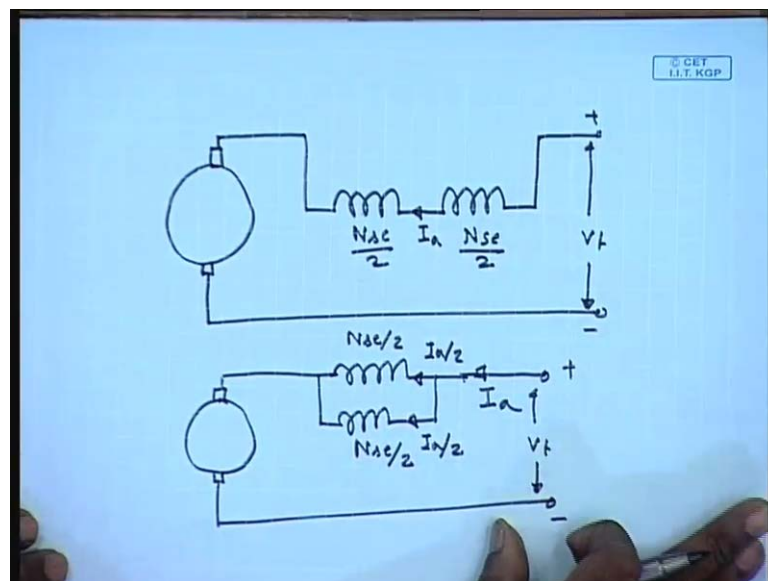
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There are several taps that are taken from the series field, and actually at any given moment the field can be connected to any one of those taps. Here also if we are basically

changing the field ampere turns and hence the field flux. Let us say the total number of series field turns is N_{se} and between the present tap it is N_{se}' . So, effective series current I_{se} equal to N_{se}' divided by N_{se} into I_a which is some $k_{se} I_a$. So, the resistance also next will be somewhat assuming them to be proportional to N_{se}' by N_{se} into R_{se} to $k_{se} R_{se}$. As in this case also we will get similar torque speed characteristics as in the case of field diverter where x_d will now be replaced by R_{se} . A special case of this type of field control is called where the field winding is arranged in several sections and series parallel combination of these sections are used.

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For example let us say that we have a DC series machine whose field winding has two sections of equal number of turns, each $N_{se}/2$. Now these two series these two field winding can also be connected in parallel like this, whereas in this case the total current flowing to each of them is I_a . Here it is $I_a/2$ and this is $I_a/2$ total current being same I_a .

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$$AT|_{\text{parallel}} = 2 \left(\frac{N_{sc}}{2} \times \frac{I_a}{2} \right)$$

$$= \frac{1}{2} N_{sc} I_a = \frac{1}{2} AT_{\text{series}}$$

$$R'_{sc} = \left(\frac{R_{sc}}{2} \parallel \frac{R_{sc}}{2} \right) = \frac{1}{4} R_{sc}$$

$$\phi|_{\text{series}} = K_f I_a$$

$$\phi|_{\text{parallel}} = \frac{1}{2} K_f I_a$$

Then A T ampere turns of the series field winding with parallel connection is A T with parallel connection will be equal to two times the A T of individual winding, which is N_{sc} by 2 into I_a by 2 this is equal to half $N_{sc} I_a$, which is half of A T with series connection. Also R'_{sc} will be R_{sc} by two parallel R_{sc} by two is equal to one fourth of R_{sc} . So, K_{sc} in this case, we assume linear field then ϕ in series will be equal to will be $K_f I_a$ whereas, ϕ with parallel connection will be equal to half $K_f I_a$. Hence only two speeds are possible, here only two speeds are possible. So, let us try to solve the how a few problems when how a speed control can be achieved.

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DC Series Motor.

O.C.C , 900 RPM					
I_a	0	50	100	150	200
E.	0	78	150	192	220

$r_a = 0.035\Omega$, $r_{sc} = 0.015\Omega$.

$V_t = 220V$, $N=?$ & $T_e=?$, at $I_a = 200A$, with full field.

Let us take a DC series motor, the O C C is given by $I_a = 0, 50$ ampere, $70, 800$ ampere. This is at 900 RPM, 150 volts, 150 ampere, 192 volts and 200 ampere, 220 volts. The r_a equal to 0.035 ohm and $R_s e$ equal to 0.015 ohm the supply voltage v_t equal to 220 volts. What should be the speed and torque of the motor if at I_a equal to 200 ampere with full field.

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$$r_a + r_{sc} = 0.035 + 0.015 = 0.05 \Omega$$

$$E_a = 220 - 200 \times 0.05 = 210 \text{ V}$$

$$I_a = 200 \text{ A}, N = 900 \text{ RPM}, E = 220 \text{ V}$$

$$I_a = 200 \text{ A}, E = 210 \text{ V}$$

$$N = 900 \times \frac{210}{220} = 859.1 \text{ RPM}$$

$$T = \frac{E I_a}{\omega} = \frac{210 \times 200}{\frac{2\pi \times 859.1}{60}} = 466.85 \text{ Nm}$$

(a) Full field, $I_a = 200 \text{ A}, N = 859.1 \text{ RPM}$
 $T_e = 466.85 \text{ Nm}$

Let us first find this out with field total r_a plus $R_s e$ equal to 0.035 plus 0.015 equal to 0.05 ohm. E_a equal to 22 minus 200 into 0.05 equal to 210 volts. So, with with I_a equal to 200 ampere. N equal to 900 RPM we know e equal to 220 volts. Now, here are same I_a equal to 200 ampere, we have got an E of 210 volts. So, N equal to 900 into 210 divided by 220 this comes to 859.1 RPM. So, what is $T_e I_a$ by ω . So, 210 into 200 divided by 2π into 859.1 by 60 . This comes to 46.85 Newton meter . So, with full field at I_a equal to 200 amperes we got N equal to 859.1 RPM and T_e equal to 466.85 Newton meter.

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$$N_{se}' = N_{se}/2.$$
$$R_{se}' = \frac{R_{se}}{2} = \frac{0.015}{2} = 0.0075 \Omega$$
$$R = r_a + R_{se}' = 0.035 + 0.0075 = 0.0425 \Omega.$$
$$I_a = 200 \text{ A}, \quad E_a = 220 - 200 \times 0.0425$$
$$= 211.5 \text{ V}.$$
$$N_{se}' = N_{ac}/2$$
$$I_{se} = \frac{200}{2} = 100 \text{ A}.$$

Now, let us see how these values will change when the field is field turns are reduced to half. Then the resistance R_{se}' will be equal to R_{se} by 2, that will be 0.01 by 2, 0.0075 ohm. So, total resistance R equal to r_a plus R_{se}' will be 0.035 plus 0.0075. This will be equal to 0.0425 ohm. So, the when I_a equal to 200 ampere then E_a will be 220 minus 200 into 0.425 equal to 211.5 volts. Now, N_{se}' equal to N_{se} by 2. So, effective field current effective full field current equal to I_{se} equal to 200 by two equal to 100 amperes.

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$$I_a = 100 \text{ A}, \quad N = 900 \text{ RPM}, \quad E = 150 \text{ V}.$$
$$I_a = 100 \text{ A}, \quad E = 211.5 \text{ V}$$
$$N = 900 \times \frac{211.5}{150} = 1269 \text{ RPM}.$$
$$T_e = \frac{E I_a}{\omega} = \frac{211.5 \times 200}{2\pi \times \frac{1269}{60}}$$
$$= 318.5 \text{ Nm}$$
$$N = 1269 \text{ RPM}$$
$$T_e = 318.5 \text{ Nm}$$

So, for 100 amperes, we have the given data we have seen that at I_a equal to 100 amperes, and N equal to 900 RPM. We have got E equal to 150 volts therefore, now if our we have same I_a equal to 100 amperes, and E equal to 211.5volts therefore, N will be 900 into 211.5 divided by 150 equal to 1269 RPM. And torque will be $E I_a$ by ω that is 211.5, but armature current is 200 ampere divided by 2π into 1269 by 60.

This will come to 318.5 Newton meter. So, with half the series field winding now we have N equal to 1269 RPM, and T_e equal to 318.5 Newton meter. comparing with the previous result we find that as the series field turn reduces the speed increases from 859 to 1269, and the torque decreases from 466 to 318. This is the field weakening mode of operation of DC series motor.

Thank you.