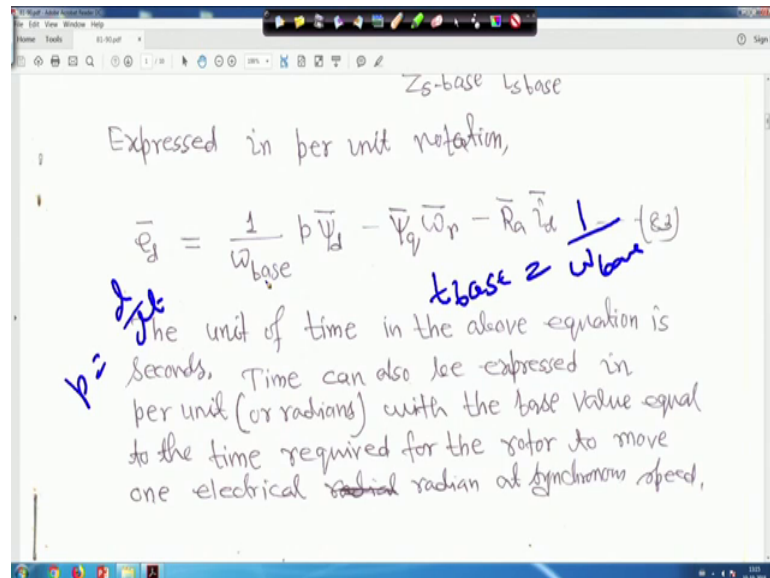


**Power System Dynamics, Control and Monitoring**  
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**Lecture – 08**  
**Power System Stability (Contd.)**

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We are back again; so this equation how you got p bar right. So, it is actually this is we have taken that t base is equal to 1 upon omega base right, that is your omega base. Now question is p actually is equal to your d by dt and 1 upon omega base is there; that means, let me clear it; that means, this equation I can write like this,.

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Z<sub>s</sub>-base I<sub>s</sub>base

Expressed in per unit notation,

$$\bar{E}_d = \frac{1}{\omega_{base}} p \bar{\psi}_d - \bar{V}_q \bar{\omega}_r - \bar{R}_a \bar{i}_d \quad \dots (83)$$

The unit of time in the above equation =  $\frac{dt}{\omega_{base}} = \frac{d}{\omega_{base}} = \frac{1}{p}$  seconds.

Time can also be expressed in per unit (or radians) with the base value equal to the time required for the rotor to move one electrical radian at synchronous speed,

This equation, I can write like this is equal to your t base instead of 1 upon omega base only this term later you will know everything is this is p, then psi d bar only this term I am writing right.

Now, p is equal to d dt therefore, this term can be written as your d by your it is d dt. So, it can be written by dt divided by t base right. So, that is this term right. So, if you write like this then this term will become d by dt bar right. Because dt upon t base. So, that can be written as actually p bar right.

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base       $\omega_{base}$        $I_s$  base

With time in per unit, Eqn.(83) may be written as:

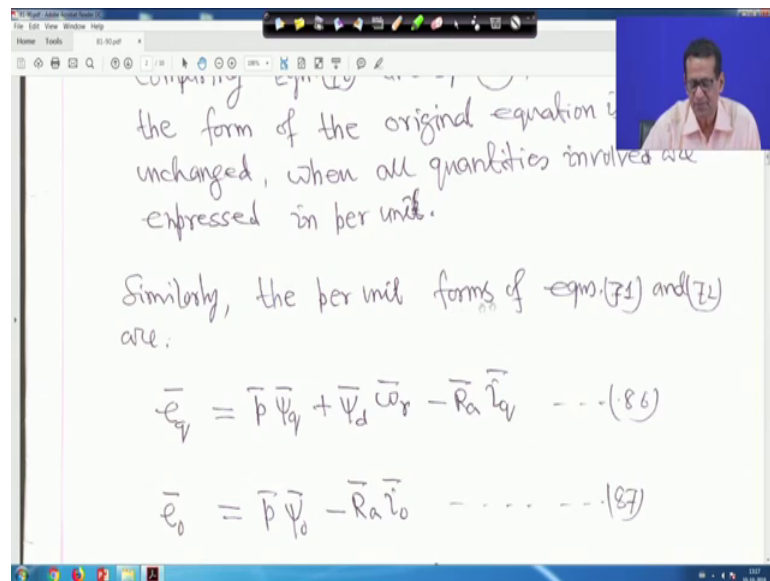
$$\bar{E}_d = p \bar{\psi}_d - \bar{V}_q \bar{\omega}_r - \bar{R}_a \bar{i}_d \quad \dots (85)$$

Comparing Eqn.(70) and Eqn.(85), we see that the form of the original equation is unchanged, when all quantities involved are expressed in per unit.

So, if you want to represent the time in per unit that is why this equation, this t base is written ed bar is equal to p bar psi d bar minus psi q bar omega r minus Ra bar i d bar these are all per unit values bar means per unit values. But throughout our analysis we will only study for your what you call to in a time in second right, but this is some representation in time in per unit So, equation 70 and an 85, compare equation 70 and equation 85 you will see that the form of the original equation is unchanged.

Only when all quantities involved expressing per unit so, this here equation 70 also they are also ed is equal to p psi d minus psi q omega r minus Ra id in per unit also it is like that right. So, ultimately equation is unchanged only that (Refer Time: 02:33) your 70 you have to consider all that here exact values and here they are dimensionless that is all otherwise expressions will remain same right.

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Similarly, per unit forms of equation 71 and 72 easily similar way you can do this similar way right. So, it will be e q bar will be p bar psi q bar plus psi d bar omega r bar minus Ra bar iq bar, this is equation 86. Similarly e 0 bar will be p bar psi 0 bar minus Ra bar i 0 bar. This is 87 bar means all are per unit values, but equation an unchanged only there in per unit values right.

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$$\bar{e}_q = \bar{p} \bar{\psi}_q + \bar{\psi}_d \omega_r - R_a \bar{i}_q \quad \dots (86)$$

$$\bar{e}_o = \bar{p} \bar{\psi}_o - R_a \bar{i}_o \quad \dots (87)$$

The per unit time derivative  $\bar{p}$  appearing in the above equations is given by

$$\bar{p} = \frac{d}{dt} = \frac{1}{\omega_{base}} \frac{d}{dt} = \frac{p}{\omega_{base}} \quad \dots (88)$$

So, whatever I told you the p bar it is d by dt. So, it is 1 upon omega base d by dt. So, p by omega base right. So, this is whatever the way I showed you that how it will be p bar.

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Per Unit Rotor Voltage Equations

From eqn(50), dividing throughout by  $e_{fd\text{base}}$

$$e_{fd\text{base}} = \omega_{base} \psi_{fd\text{base}} = z_{fd\text{base}} i_{fd\text{base}},$$

the per unit field voltage equation may be written as:

$$\bar{e}_{fd} = \bar{p} \bar{\psi}_{fd} + \bar{R}_{fd} \bar{i}_{fd} \quad \dots (89)$$

Next is per unit rotor voltage equations. Now from equation 50 you divide throughout by  $e_{fd\text{base}}$  it is easy  $e_{fd\text{base}}$  that is your field voltage field size right, is equal to omega base into psi fd base is equal to z fd base into i fd base same philosophy like stator here also it is rotor right So, the per unit field voltage equation may be written as same thing both side you divide by  $e_{fd\text{base}}$  left hand side then other terms you divide by omega

base psi f d base and z fd base your i fd base the way we have done it for the stator similar meaning right.

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Similarly, the per unit form of eqn. (51)

$$0 = \bar{p} \bar{\Psi}_{kd} + \bar{R}_{kd} \bar{i}_{kd} \quad \dots (90)$$

$$0 = \bar{p} \bar{\Psi}_{kq} + \bar{R}_{kq} \bar{i}_{kq} \quad \dots (91)$$

The above equations show the form of the rotor circuit voltage equations. However, we have not yet developed a basis for the choice of the rotor base quantities.

Then you will get  $e_{fd}$  bar is equal to  $p$  bar psi  $f_d$  bar plus  $R_{fd}$  bar  $i_{fd}$  bar this is equation 89 similar way. Similarly the per unit form of equation 51 and 52 it will be  $0$  is equal to  $p$  bar psi  $k_d$  bar. Actually nothing is change just making bar to represent unit dividing those quantity and  $i_{kd}$  bar this is 90. And another one  $0$  is equal to  $p$  bar psi  $k_q$  bar plus  $R_{kq}$  bar  $i_{kq}$  bar this is equation 91 right.

Therefore the above this above equation shows the form of rotor circuit voltage equation. However, we have not yet developed a basis for the choice of the rotor base quantities right. Because we have to make things reciprocal, but earlier we have seen it is not reciprocal right.

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The above equations show the form of rotor circuit voltage equations. However, we have not yet developed a basis for the choice of the rotor base quantities.

Stator Flux Linkage Equations

Using the basic relationship  $\Psi_{sbase} = L_{sbase} i_{sbase}$ , the per unit forms of equations (64), (65) and (66) may be written as:

So, stator flux linkage equation using the basic relationship of  $\psi_{s \text{ base}}$  is equal to  $L_{s \text{ base}}$   $i_{s \text{ base}}$  right the per unit forms of equation 64, 65, and 66 may be written as. So, I mean using this relationship  $\psi_{s \text{ base}}$  actually in general we know  $\psi$  is equal to  $L$   $i$  right flux linkage is equal to inductance in current in general.

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$$\bar{\Psi}_d = -\bar{L}_d \bar{i}_d + \bar{L}_{afd} \bar{i}_{fd} + \bar{L}_{akd} \bar{i}_{kd}$$

$$\bar{\Psi}_q = -\bar{L}_q \bar{i}_q + \bar{L}_{aq} \bar{i}_{q'} \dots (93)$$

$$\bar{\Psi}_0 = -\bar{L}_0 \bar{i}_0 \dots (94)$$

where by definition,

$$\bar{L}_{afd} = \frac{L_{afd}}{L_{sbase}} \cdot \frac{i_{fdbase}}{i_{sbase}} \dots (95)$$

So,  $\psi_{s \text{ base}}$  is equal to  $L_{s \text{ base}}$   $\psi_{s \text{ base}}$  and it is  $\psi_d$  bar same way you could divide and simplify you will find it is minus  $L_d$  bar  $i_d$  bar plus  $L_{fd}$  bar  $i_{fd}$  bar plus  $L_{kd}$  bar  $i_{kd}$  bar this is equation 92. Similarly,  $\psi_q$  bar will be minus  $L_q$  bar,  $i_q$  bar plus  $L_{aq}$  bar

$L_{akq}$  bar  $i$   $q$  bar this is 93. And  $\psi_0$  bar will be minus  $L_{0}$  bar  $i$   $0$  bar this is equation 94 right.

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Where by definition,

$$\bar{L}_{afd} = \frac{L_{afd}}{L_{sbase}} \cdot \frac{i_{fdbase}}{i_{sbase}} \dots (95)$$

$$\bar{L}_{akd} = \frac{L_{akd}}{L_{sbase}} \cdot \frac{i_{kdbase}}{i_{sbase}} \dots (96)$$

$$\bar{L}_{akq} = \frac{L_{akq}}{L_{sbase}} \cdot \frac{i_{qbase}}{i_{sbase}} \dots (97)$$

Rotor Flux Linkage Equations

Now where by definition  $L_{fd}$  bar will be  $L_{fd}$  upon  $L_{sbase}$  into  $i_{fdbase}$  upon  $i_{sbase}$  these are very simple thing, but I suggest that little bit you derive right little bit you derive right. So,  $L_{fd}$  bar will be actually  $L_{afd}$  upon  $L_{sbase}$  into  $i_{fdbase}$  upon  $i_{sbase}$  right. Similarly  $L_{akd}$  bar will become  $L_{akd}$  upon  $L_{sbase}$  into  $i_{kdbase}$  upon  $i_{sbase}$  this is equation 96. Similarly  $L_{akq}$  bar will be  $L_{akq}$  upon  $L_{sbase}$  into  $i_{qbase}$  upon  $i_{sbase}$  right so this is equation 97.

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Rotor Flux Linkage Equations

Similarly, in per unit form equations (67), (68) and (69) become,

$$\bar{\Psi}_{fd} = \bar{L}_{ffd} \bar{i}_{fd} + \bar{L}_{fkd} \bar{i}_{kd} - \bar{L}_{fda} \bar{i}_d \quad \dots (98)$$

$$\bar{\Psi}_{kd} = \bar{L}_{kdf} \bar{i}_{fd} + \bar{L}_{kkd} \bar{i}_{kd} - \bar{L}_{kda} \bar{i}_d \quad \dots (99)$$

$$\bar{\Psi}_{kq} = \bar{L}_{kkq} \bar{i}_{kq} - \bar{L}_{kqa} \bar{i}_q \quad \dots (100)$$

Now, rotor flux linkage equation, similarly in per unit form of equation 67, 68, and 69 same way will transform equation remains same only everywhere bar is there; that means, they are per unit. Therefore,  $\bar{\Psi}_{fd}$  will be  $\bar{L}_{ffd} \bar{i}_{fd}$  plus  $\bar{L}_{fkd} \bar{i}_{kd}$  minus  $\bar{L}_{fda} \bar{i}_d$  this is equation 98.

Similarly,  $\bar{\Psi}_{kd}$  will be  $\bar{L}_{kdf} \bar{i}_{fd}$  plus  $\bar{L}_{kkd} \bar{i}_{kd}$  minus  $\bar{L}_{kda} \bar{i}_d$  this is equation 99. And similarly  $\bar{\Psi}_{kq}$  will be  $\bar{L}_{kkq} \bar{i}_{kq}$  minus  $\bar{L}_{kqa} \bar{i}_q$  this is equation 100. So, all these things all these things this per unit system later I will take your example also on per unit you will all calculations will be shown you will find the things are quite easy right.



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Where by definition,

$$\bar{L}_{fda} = \frac{3}{2} \frac{L_{afd}}{L_{fd\text{base}}} \cdot \frac{i_{s\text{base}}}{i_{fd\text{base}}} \quad \dots (101)$$

$$\bar{L}_{fkd} = \frac{L_{fkd}}{L_{fd\text{base}}} \cdot \frac{i_{kd\text{base}}}{i_{fd\text{base}}} \quad \dots (102)$$

$$\bar{L}_{kda} = \frac{3}{2} \frac{L_{akd}}{L_{kd\text{base}}} \cdot \frac{i_{s\text{base}}}{i_{kd\text{base}}} \quad \dots (103)$$

So, whereby definition again we know that  $\bar{L}_{fda}$  is equal to 3 by 2  $L_{afd}$  upon  $L_{fd\text{base}}$  into  $i_{s\text{base}}$  by  $i_{fd\text{base}}$  this is equation 101. Similarly,  $\bar{L}_{fkd}$  is equal to  $L_{fkd}$  upon  $L_{fd\text{base}}$  into  $i_{kd\text{base}}$  upon  $i_{fd\text{base}}$ , right. Similarly  $\bar{L}_{kda}$  is equal to 3 by 2  $L_{akd}$  upon  $L_{kd\text{base}}$  into  $i_{s\text{base}}$  upon  $i_{kd\text{base}}$  right.

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$$\bar{L}_{kda} = \frac{3}{2} \frac{L_{akd}}{L_{kd\text{base}}} \cdot \frac{i_{s\text{base}}}{i_{kd\text{base}}} \quad \dots (103)$$

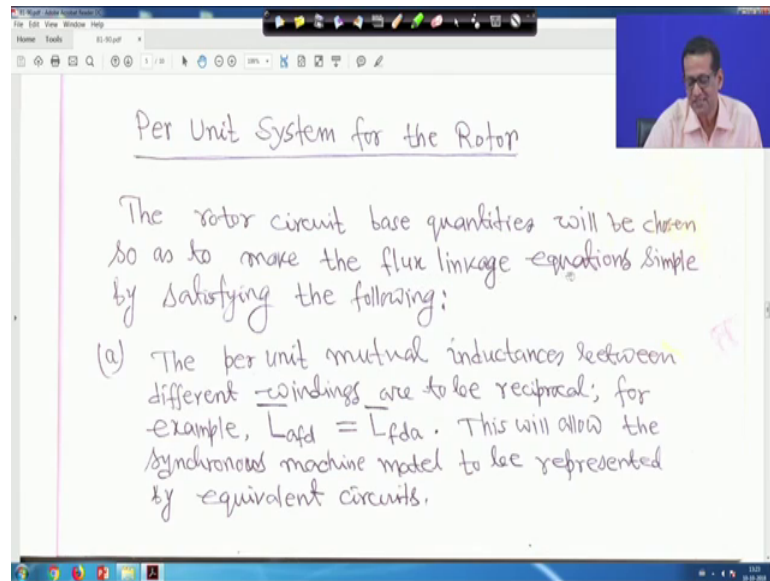
$$\bar{L}_{kdf} = \frac{L_{fkd}}{L_{kd\text{base}}} \cdot \frac{i_{fd\text{base}}}{i_{kd\text{base}}} \quad \dots (104)$$

$$\bar{L}_{kqa} = \frac{3}{2} \frac{L_{akq}}{L_{kq\text{base}}} \cdot \frac{i_{s\text{base}}}{i_{kq\text{base}}} \quad \dots (105)$$

Similarly,  $\bar{L}_{kdf}$  will be  $L_{fkd}$  upon  $L_{kd\text{base}}$  into  $i_{fd\text{base}}$  upon  $i_{kd\text{base}}$  this is equation 104 right. similarly  $\bar{L}_{kqa}$  is equal to 3 by 2  $L_{akq}$  upon  $L_{kq\text{base}}$  into  $i_{s\text{base}}$  upon  $i_{kq\text{base}}$ . Now, all these things what you call if we see that here  $\bar{L}_{fda}$  is

equal to  $3 \times 2 L_{fd}$  based upon the left side. And just hold on and if you see here here  $L_{fd}$  is equal to  $L_{afd}$  based upon the right side and here your  $L_{LLfd}$  is  $3 \times 2 L_{afd}$  here  $L_{fd}$  where multiplied by your  $3 \times 2 L_{fd}$  upon  $L_{fd}$  base is based upon the right side. So, similarly your  $L_{kqa}$  also multiplied by  $3 \times 2$ , but we have to actually what we have to do is.

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That we have to see that things are reciprocal; that means, per unit values either refer to stator or rotor side have to be same like transformer by refer to primary or secondary side. But one  $3 \times 2$  factor is there we have to eliminate that So, the rotor circuit base quantities will be chosen first to make the flux linkage equations simple by satisfying the following. The per unit mutual inductances between different winding are to be reciprocal that is for example,  $L_{afd}$  must be is equal to  $L_{fda}$  this should be equal right per unit refer to either side. This will allow the synchronous machine model to be represented by equivalent circuit right.

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(b) All per unit mutual inductances between stator and rotor circuits in each axis are to be equal; for example,  $\bar{L}_{afd} = \bar{L}_{akd}$

In order to have  $\bar{L}_{fkd} = \bar{L}_{kdf}$ , so that reciprocity is achieved, from eqn. (102) and (104), it is necessary to have,

$$\frac{L_{fkd}}{L_{fdbase}} \cdot \frac{i_{kdbase}}{i_{fdbase}} = \frac{L_{kdf}}{L_{kdbase}} \cdot \frac{i_{fdbase}}{i_{kdbase}}$$

So, for that second thing is that all per unit mutual inductances between stator and rotor circuit in each axis are to be equal for example,  $\bar{L}_{afd}$  is equal to  $\bar{L}_{akd}$  right. In order to have  $\bar{L}_{fkd}$  is equal to  $\bar{L}_{kdf}$ , because it is what you call this has to be made reciprocal. So, that reciprocity is achieved from equation 102 and 104 it is necessary to have this relationship.

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In order to have  $\bar{L}_{fkd} = \bar{L}_{kdf}$ , so that reciprocity is achieved, from eqn. (102) and (104), it is necessary to have,

$$\frac{L_{fkd}}{L_{fdbase}} \cdot \frac{i_{kdbase}}{i_{fdbase}} = \frac{L_{kdf}}{L_{kdbase}} \cdot \frac{i_{fdbase}}{i_{kdbase}}$$

$$\therefore L_{kdbase} \cdot i_{kdbase}^2 = L_{fdbase} \cdot i_{fdbase}^2 \quad \text{--- (106)}$$

That  $L_{fd}$  upon  $L_{kd}$  base into  $i_{kd}$  base upon  $i_{fd}$  base is equal to  $L_{kd}$  upon  $L_{fd}$  base into  $i_{fd}$  base upon  $i_{kd}$  base just equation 102 and equation 104 if you do so if you do so, because this condition has to be made otherwise it cannot be reciprocal right.

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$$\frac{L_{fd}}{L_{kd}} \cdot \frac{i_{kd}}{i_{fd}} = \frac{L_{kd}}{L_{fd}} \cdot \frac{i_{fd}}{i_{kd}}$$

$$\therefore L_{kd} \cdot i_{kd}^2 = L_{fd} \cdot i_{fd}^2 \quad \text{--- (106)}$$

Multiplying by  $\omega_{base}$  gives

$$\omega_{base} L_{kd} i_{kd}^2 = \omega_{base} L_{fd} i_{fd}^2$$

So, in that case what will happen this side is becoming  $L_{kd}$  base into  $i_{kd}$  base square is equal to  $L_{fd}$  base into  $i_{fd}$  base square right. So, just what you do see cross multiply cross multiplication right. So, in this case that means multiplying both sides by omega as if if you do omega base.

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$$\frac{L_{fd}}{L_{kd}} \cdot \frac{i_{kd}}{i_{fd}} = \frac{L_{kd}}{L_{fd}} \cdot \frac{i_{fd}}{i_{kd}}$$

$$\therefore L_{kd} \cdot i_{kd}^2 = L_{fd} \cdot i_{fd}^2 \quad \text{--- (106)}$$

Multiplying by  $\omega_{base}$  gives

$$\omega_{base} L_{kd} i_{kd}^2 = \omega_{base} L_{fd} i_{fd}^2$$

Since  $\omega_{base} L_{base} i_{base} = e_{base}$ ,

Then you will be  $\omega_{base} L_{kdbase} i_{kdbase}^2$  is equal to  $\omega_{base} L_{fdbase} i_{fdbase}^2$ .

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$$\therefore L_{kdbase} i_{kdbase}^2 = L_{fdbase} i_{fdbase}^2$$

Multiplying by  $\omega_{base}$  gives

$$\omega_{base} L_{kdbase} i_{kdbase}^2 = \omega_{base} L_{fdbase} i_{fdbase}^2$$

Since  $\omega_{base} L_{base} i_{base} = e_{base}$ ,

$$e_{kdbase} i_{kdbase}^2 = e_{fdbase} i_{fdbase}^2 \quad \dots (107)$$

But we know that  $\omega_{base} L_{base} i_{base}$  is equal to nothing, but the  $e_{base}$  right this we know. Therefore, this side we can write left hand side it will be  $e_{kdbase} i_{kdbase}^2$  from the dimension analyse of the per unit and this dimension your what you call that earlier we have seen this right from its dimension only right.

So, it basically it will be  $e_{kdbase} i_{kdbase}^2$  because it is  $i_{kdbase}^2$  is there. So, naturally it will be  $e_{kdbase} i_{kdbase}^2$  is equal to your this thing this base rate this  $e_{base}$  that is your this is the general formula for the dimension thing as far as per unit thing. So, instead of that we can write is  $e_{kdbase} i_{kdbase}^2$  and these are right hand side will be  $e_{fdbase} i_{fdbase}^2$  this condition has to be satisfied for the reciprocal thing right.

So, only thing is that apparently it looks little difficult, but it is not difficult. If you face any question if you face any problem you when you will go through these you put the question in the forum, we will answer all the questions right. And while at that time if you want you fail to derive one or two thing you will try to provide you what you call the derivation. But I did not bring it here it will kill lot of time right, but you have to keep this mind only keep it in your memory only right.

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$\omega_{base} L_{base} I_{base} = E_{base}$

$E_{kd_{base}} I_{kd_{base}} = E_{fd_{base}} I_{fd_{base}} \quad \dots (107)$

Therefore, in order for the rotor circuit mutual inductances to be equal, their ~~voltage~~ Volt-Ampere bases must be equal.

(87)

Therefore in order to for the rotor circuit mutual inductances to be equal their volt ampere base must be equal. Because this side is volt ampere b into i basically e into i this side also e into i. So, volt ampere base must be equal right.

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For mutual inductances  $\bar{L}_{afd}$  and  $\bar{L}_{fda}$  to be equal, from eqns. (95) and (101),

$$\frac{L_{afd}}{L_{s_{base}}} \cdot \frac{I_{fd_{base}}}{I_{s_{base}}} = \frac{3}{2} \cdot \frac{L_{afd}}{L_{fd_{base}}} \cdot \frac{I_{s_{base}}}{I_{fd_{base}}}$$

or

$$L_{fd_{base}} I_{fd_{base}}^2 = \frac{3}{2} L_{s_{base}} I_{s_{base}}^2$$

Similarly for mutual inductances that is  $\bar{L}_{afd}$  and  $\bar{L}_{fda}$  to be equal from equation 95 and 101 they have to be equal. Otherwise you cannot make per unit or refer to either side is equal you have to make this condition right.

So, if you do so then we are making  $L_{fd}$  upon  $L_{fd}$  upon  $i_s$  base into  $i_{fd}$  base upon  $i_s$  base is equal to  $3$  by  $2$   $L_{afd}$  upon  $L_{fd}$  base into  $i_s$  base upon  $i_{fd}$  base. And you cross multiply and simplify it will be  $L_{fd}$  base into  $i_{fd}$  base square is equal to  $3$  by  $2$   $L_s$  base into  $i_s$  base square right. So, both side you multiply by  $\omega$  base.

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op

$$L_{fdbase} i_{fdbase}^2 = \frac{3}{2} L_{sbase} i_{sbase}^2$$

Multiplying by  $\omega_{base}$  and noting that  $\omega L = Z$ , get,

$$(\omega_{base} L_{fdbase} i_{fdbase}) \times i_{fdbase} = \frac{3}{2} \omega_{base} L_{sbase} i_{sbase}^2$$

$$e_{fdbase} i_{fdbase} = \frac{3}{2} e_{sbase} i_{sbase}$$

$$= 3 \left( \frac{e_{sbase}}{\sqrt{2}} \right) \left( \frac{i_{sbase}}{\sqrt{2}} \right) \quad \text{--- (108)}$$

$$= 3\text{-phase VA base for stator.}$$

If you multiply both side by  $\omega$  base and same as before same as before you will find that this side you multiply both side by  $\omega$  base then  $\omega$  base  $L_{fd}$  base and it is  $i_{fd}$  square so, into  $i_{fd}$  base into  $i_{fd}$  base. So, first three terms will give you actually  $e_{fd}$  base. So, it will be  $e_{fd}$  base into  $i_{fd}$  base. Similarly the right hand side it will be  $3$  by  $2$   $e_{sbase}$  into  $i_{sbase}$  I mean it is something like this. I mean both side you multiply by  $\omega$  base then left hand side only I am writing right hand side similarly you can get it. It is  $\omega$  base then  $L_{fd}$  base then  $i_{fd}$  base right it is  $i_{fd}$  base square. So, into your  $i_{fd}$  base. So, this term is nothing, but  $e_{fd}$  base into  $i_{fd}$  base similarly the right hand side same meaning right

So, then we right hand side also you can write that your  $3$  by  $2$  then  $e_{sbase}$  into  $i_{sbase}$ . Now this  $1$  you can write  $3$  and  $2$  these two is there you can write  $e_{sbase}$  upon  $\sqrt{2}$  into  $i_{sbase}$  upon  $\sqrt{2}$  this is equation 108 or I mean or you can write it is basically  $3$  into it is  $3$  phase volt ampere base for the stator this is basically rms and this is basically rms we have taken earlier we have taken earlier.

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$$e_{fbase} i_{fbase} = \frac{3}{2} e_{sbase} i_{sbase}$$

$$E_{rms} = \frac{e_s}{\sqrt{2}} \quad I_{rms} = \frac{i_{sbase}}{\sqrt{2}}$$

$$E_{rms} I_{rms} = 3 \left( \frac{e_{sbase}}{\sqrt{2}} \right) \left( \frac{i_{sbase}}{\sqrt{2}} \right) \quad \text{--- (108)}$$

$$= 3 \frac{e_{sbase} i_{sbase}}{2}$$

3-phase VA base for stator.

Similarly in order for  $\bar{L}_{akd} = \bar{L}_{kda}$  and  $\bar{L}_{akq} = \bar{L}_{kqa}$ .

$$e_{kdbase} i_{kdbase} = \frac{3}{2} e_{sbase} i_{sbase} \quad \text{--- (108)}$$

That your  $e_{rms}$  is equal to  $e_s$  upon root 2 similarly  $i_{rms}$  is equal to  $i_{sbase}$  by root 2 right that is actually nothing, but 3 into  $e_{rms}$  into  $I_{rms}$  that is nothing, but 3 phase volt ampere base further stator right.

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Similarly in order for  $\bar{L}_{akd} = \bar{L}_{kda}$   
 $\bar{L}_{akq} = \bar{L}_{kqa}$ ,

$$e_{kdbase} i_{kdbase} = \frac{3}{2} e_{sbase} i_{sbase} \quad \text{--- (109)}$$

and

$$e_{kqbase} i_{kqbase} = \frac{3}{2} e_{sbase} i_{sbase} \quad \text{--- (110)}$$

These equations imply that in order to satisfy requirement (a) above, the VA base in all rotor circuits must be the same and equal to the stator three-phase VA base.

Similarly, we have to make this thing  $\bar{L}_{akd}$  is equal to  $\bar{L}_{kda}$  and  $\bar{L}_{akq}$  is equal to  $\bar{L}_{kqa}$  because you want everything should be in reciprocal right. So, the similar way you can make it  $e_{kdbase}$  if you equate if you equate this 1 and this 1 you will get  $e_{kdbase}$   $i_{kdbase}$  go back to those referred equation and just equate it just



equate it I did not write it here if you do it it will be e kd base i kd base is equal to 3 by 2 es base into i s base.

Similarly, ek ek q base you you are you have to call into i kq base is equal to 3 by 2 e s base i s base this is equation 110 right. So, these equations imply that in order to satisfy requirement a above the volt ampere base in all rotor circuits must be the same and equal to the stator three phase volt ampere base right. This we have to might be a quantities right I mean this side is the right hand side is the stator base quantities and left hand side is the rotor side right that have to be made equal.

(Refer Slide Time: 15:51)

The stator leakage inductances in the two axes are nearly equal. Denoting the leakage inductance  $\bar{L}_l$  and the mutual inductances by  $\bar{L}_{ad}$  and  $\bar{L}_{aq}$ :

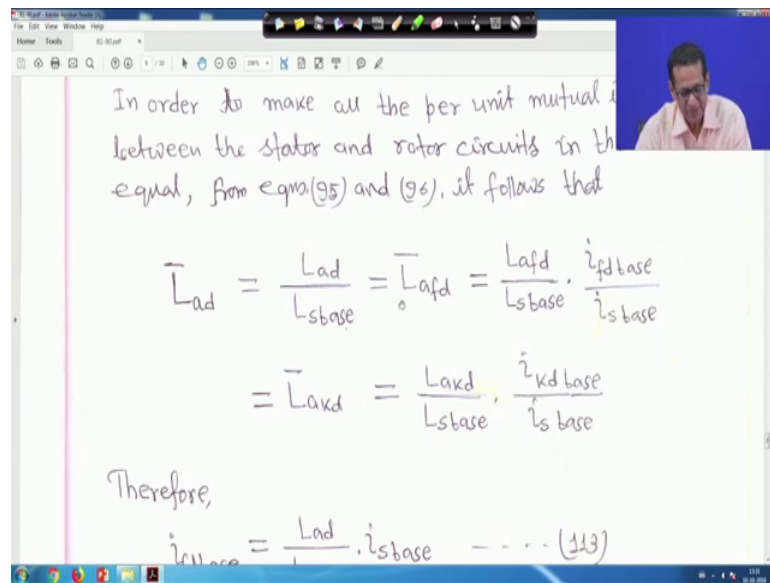
$$\bar{L}_d = \bar{L}_l + \bar{L}_{ad} \quad \dots (111)$$

and

$$\bar{L}_q = \bar{L}_l + \bar{L}_{aq} \quad \dots (112)$$

So, stator leakage inductances in the two axes are nearly equal right denoting the leakage inductance  $\bar{L}_l$  and the mutual inductances by  $\bar{L}_{ad}$  and  $\bar{L}_{aq}$  right. Therefore,  $\bar{L}_d$  is equal to  $\bar{L}_l$  plus  $\bar{L}_{ad}$  directly you can write and  $\bar{L}_q$  is equal to  $\bar{L}_l$  plus  $\bar{L}_{aq}$  directly you can write this 111, this is 112 right.

(Refer Slide Time: 16:15)



In order to make all the per unit mutual inductances between the stator and rotor circuits in the dx is your dx is equal from equation 95 and your 96. It follows that you have to make everything is equal because you have to make a primary thing either rotor side or stator side they should be equal. Therefore,  $L_{ad}$  bar you can write  $L_{ad}$  upon  $i_s$  base is equal to you have to equate it that  $L_{fd}$  bar that is also we have seen  $L_{fd}$  upon  $i_s$  base into  $i_{fd}$  base upon  $i_s$  base or this can be is equal to  $L_{kd}$  bar is equal to  $L_{kd}$  upon  $i_s$  base into  $i_{kd}$  base upon  $i_s$  base right.

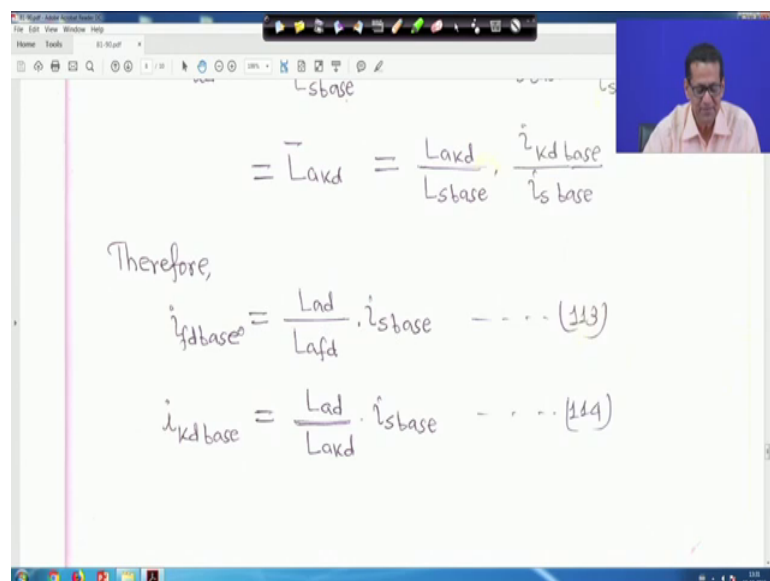
$$\bar{L}_{ad} = \frac{L_{ad}}{L_{sbase}} = \bar{L}_{afd} = \frac{L_{afd}}{L_{sbase}} \cdot \frac{i_{fdbase}}{i_{sbase}}$$

$$= \bar{L}_{akd} = \frac{L_{akd}}{L_{sbase}} \cdot \frac{i_{kdbase}}{i_{sbase}}$$

Therefore,

$$i_{fdbase} = \frac{L_{ad}}{L_{afd}} \cdot i_{sbase} \quad \dots (113)$$

(Refer Slide Time: 16:53)



$$= \bar{L}_{akd} = \frac{L_{akd}}{L_{sbase}} \cdot \frac{i_{kdbase}}{i_{sbase}}$$

Therefore,

$$i_{fdbase} = \frac{L_{ad}}{L_{afd}} \cdot i_{sbase} \quad \dots (113)$$

$$i_{kdbase} = \frac{L_{ad}}{L_{akd}} \cdot i_{sbase} \quad \dots (114)$$

Similarly, your i<sub>fd</sub> base will be L<sub>ad</sub> upon L<sub>fd</sub> into i<sub>s</sub> base and similarly your i<sub>kd</sub> base from that L<sub>kd</sub> base will be L<sub>ad</sub> upon L<sub>kd</sub> into i<sub>s</sub> base this is equation 114. Just my solutions to all of you when we will go through this course know all every week notes everything will be uploaded. But you please do it little bit of your own if you stuck somewhere you put the question in the forum immediately we will solve your problem right.

But nothing is there actually initially perhaps you may think that what things are, but just practice one or twice we will find actually everything is easy it is per unit system only per power system analysis course in your undergraduate course you have studied per unit. But in that synchronous machine case for dynamic stability studies this per unit representation is slightly different right, all the meaning is same.

(Refer Slide Time: 17:49)

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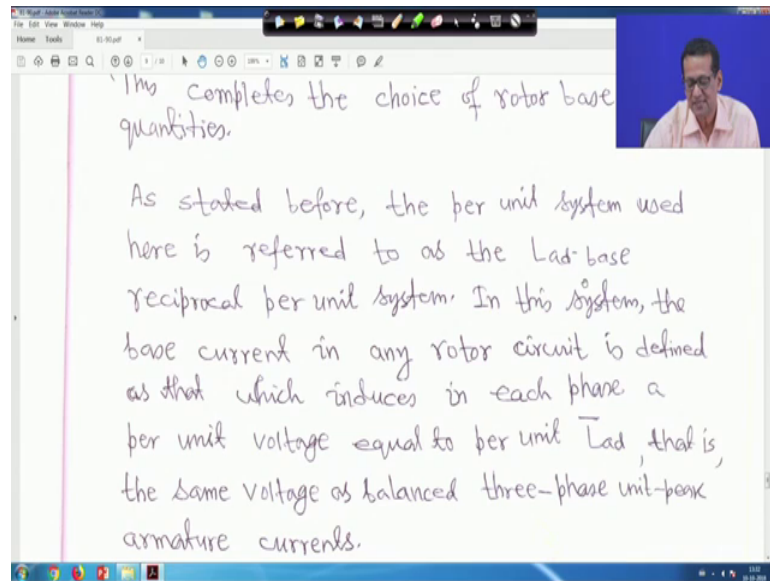
Similarly, for the q-axis mutual inductances  $\bar{L}_{aq}$  and  $\bar{L}_{kq}$  to be equal,

$$i_{kq/base} = \frac{L_{aq}}{L_{kq}} \cdot i_{s/base} \quad \dots (115)$$

This completes the choice of rotor base quantities.

Similarly, for the q axis mutual inductances  $\bar{L}_{aq}$  and  $\bar{L}_{kq}$  to be equal.

(Refer Slide Time: 17:57)



So, in that case we can write same as before  $i_{kq}$  base is equal to  $L_{akq}$  by a sorry  $L_{aq}$  by  $L_{akq}$  into  $i_s$  base this is equation 115 right. This completes that choice of the rotor base quantities right. So, as stated before the per unit system used here is referred to as the  $L_{ad}$  base reciprocal per unit system in this system the base current in any rotor circuit is defined as that which induces in each phase a per unit voltage equal to per unit  $L_{ad}$  that is the same voltage as balanced three phase unit your three phase unit peak armature currents right. So, this is what you call that is per unit system.

So, things are actually my experience show over the year; this per unit system initially student they have I will take I will take example also. Student may feel initially that things are difficult, but it is not at all difficult just to derive one or twice you will find actually the way you have done per unit analysis for power system courses in undergraduate studies it is the same thing, only the representation is slightly different right. Because of your Dq transformation right so you should practice. And if you have any problem then use this thing. I have over this over the years I have experienced on this initially is maybe little bit of problem, but after that when you will go through it will find things are quite easy right.

(Refer Slide Time: 19:27)

From eqn(73), the instantaneous power at machine terminal is

$$P_t = \frac{3}{2} (e_d i_d + e_q i_q + 2e_0 i_0)$$

Dividing by the base three-phase VA

$$\bar{P}_t = \left( \frac{3}{2} \right) \frac{e_{sbase} i_{sbase}}{e_s i_s} = \frac{e_d}{e_s} \frac{i_d}{i_s} + \frac{e_q}{e_s} \frac{i_q}{i_s} + 2 \frac{e_0}{e_s} \frac{i_0}{i_s}$$

Now, per unit power and torque; here also that we have derived this equation from equation 73 that  $P_t$  is equal to  $\frac{3}{2} e_d i_d$  plus  $e_q i_q$  plus  $2 e_0 i_0$ . So, divide the dividing by the base three phase volt ampere both side. That is  $\frac{3}{2} e_{sbase} i_{sbase}$  if you do. So, it will be it both side you divide by  $\frac{3}{2} e_{sbase}$ . So, this side it will be per unit left hand side  $\frac{3}{2}$ ,  $\frac{3}{2}$  will be cancel right hand side then it will become  $e_d$  upon  $e_{sbase}$  into  $i_d$  upon  $i_{sbase}$   $e_q$  upon  $e_{sbase}$  into  $i_q$  upon  $i_{sbase}$  it will be  $2$  into  $e_0$  upon  $e_{sbase}$  into your  $i_0$  upon  $i_{sbase}$ .

So, this is actually writing  $\bar{P}_t$  is equal to  $\frac{e_d}{e_s} \frac{i_d}{i_s}$  plus  $\frac{e_q}{e_s} \frac{i_q}{i_s}$  plus two  $\frac{e_0}{e_s} \frac{i_0}{i_s}$  there in per unit I mean it is like this because we know this dividing by your because it is power. So, three phase volt ampere of both side if you divide this 1 left hand side right it will be your  $\bar{P}_t$  part  $\bar{P}_t$  it will become actually  $\bar{P}_t$  that is  $\bar{P}_t$  upon  $\frac{3}{2} e_{sbase} i_{sbase}$ .

Now, right hand side if you do. So,  $\frac{3}{2}$ ,  $\frac{3}{2}$  will be cancel  $e_{sbase} i_{sbase}$  the first term will be your  $\frac{e_d}{e_s} \frac{i_d}{i_s}$  upon  $i_{sbase}$  right. So, this term actually nothing, but your  $\frac{e_d}{e_s}$  and this term is nothing, but your  $i_d$  bar

Similarly, this term also  $\frac{e_q}{e_s} \frac{i_q}{i_s}$  upon  $i_{sbase}$  will be  $\frac{e_q}{e_s}$  bar and  $i_q$  upon  $i_{sbase}$  will be  $i_q$  bar similarly  $2$  into  $e_0$  upon  $e_{sbase}$  will become  $\frac{e_0}{e_s}$  bar and  $i_0$  upon  $i_{sbase}$  will become  $i_0$  bar we because we are representing things are in per unit.

(Refer Slide Time: 21:11)

the expression for per unit may be written as

$$\bar{P}_t = \bar{e}_d \bar{i}_d + \bar{e}_q \bar{i}_q + 2\bar{e}_0 \bar{i}_0 \quad \dots (116)$$

Similarly, with base torque  $= \frac{3}{2} \left( \frac{p_f}{2} \right) \psi_{sbase} i_{sbase}$ , the per unit form of eqn.(75) is

$$\bar{T}_e = \bar{\psi}_d \bar{i}_q - \bar{\psi}_q \bar{i}_d \quad \dots (117)$$

So, that is why this equation is written as your  $P_t$  bar is equal to only expression even same only things are per unit values right. And all numerical rather things from real value to per unit of transformation we will see and all numerical will do in per unit value right. So,  $P_t$  bar is equal to  $e_d$  bar  $i_d$  bar plus  $e_q$  bar  $i_q$  bar plus  $2 e_0$   $i_0$  this is 116.

(Refer Slide Time: 21:31)

$\bar{P}_t = \bar{e}_d \bar{i}_d + \bar{e}_q \bar{i}_q + 2\bar{e}_0 \bar{i}_0 \quad \dots (116)$

Similarly, with base torque  $= \frac{3}{2} \left( \frac{p_f}{2} \right) \psi_{sbase} i_{sbase}$ , the per unit form of eqn.(75) is

$$\bar{T}_e = \bar{\psi}_d \bar{i}_q - \bar{\psi}_q \bar{i}_d \quad \dots (117)$$

Per Unit Reactances

If the frequency of the stator quantities is

Similarly, with the base quantities with similarly with sorry base torque that is  $\frac{3}{2} p_f$  by  $2 \psi_{sbase} i_{sbase}$  this also you have seen; so per unit form of equation 75. Now you divide that your equation 75 by this 1 you will simply get  $T_e$  bar will be  $\psi_d$  bar  $i_q$  bar

minus  $i_q$  bar  $i_d$  bar same as before it will come  $\psi_d$  upon  $\psi_s$  base and it will become your  $i_q$  upon  $i_s$  base. So, all will bar similarly for  $\psi_q$  upon  $\psi_s$  base and this term will become  $i_d$  upon  $i_s$  base. So, all are bar bars per unit everything remains same all are per unit right and this is equation 117.

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Per Unit Reactances

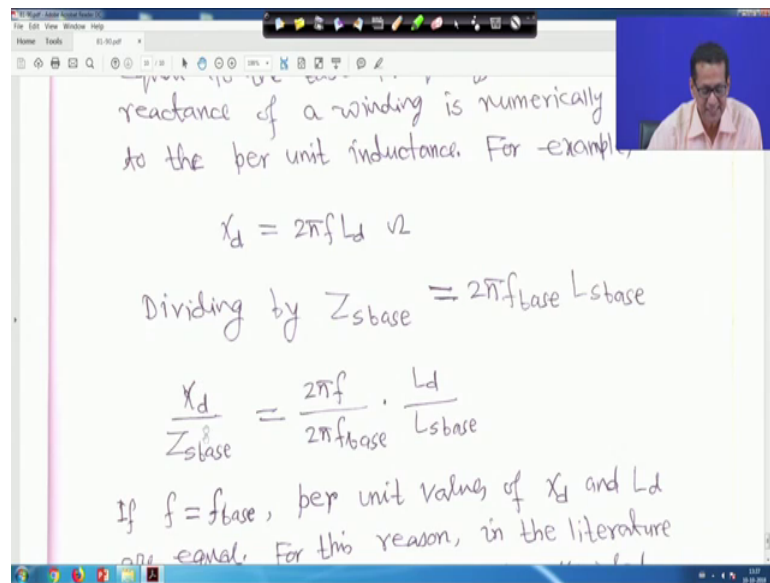
If the frequency of the stator quantities is equal to the base frequency, the per unit reactance of a winding is numerically equal to the per unit inductance. For example,

$$X_d = 2\pi f L_d \Omega$$

Dividing by  $Z_{s\text{base}} = 2\pi f_{\text{base}} L_{s\text{base}}$

Now, per unit reactance if the frequency of the stator quantities is equal to the base frequency per unit reactance of winding is numerically equal to the per unit inductance right sometimes in the numerical. So, it will per unit reactance it can be taken as per unit inductance also for example,  $X_d$  is equal to say  $2\pi f L_d \Omega$  right  $d$  by because dividing  $Z_s$  base because  $Z_s$  base is my impedance base and that is nothing but  $2\pi f$  base into  $L_s$  base right is  $\omega$  is equal to your that is  $Z_s$  base  $Z_s$  base is nothing  $Z$  is equal to  $L \omega$ . So,  $\omega$  base will be  $2\pi f$  base into  $L_s$  base

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reactance of a winding is numerically equal to the per unit inductance. For example,

$$X_d = 2\pi f L_d \quad \text{V}$$

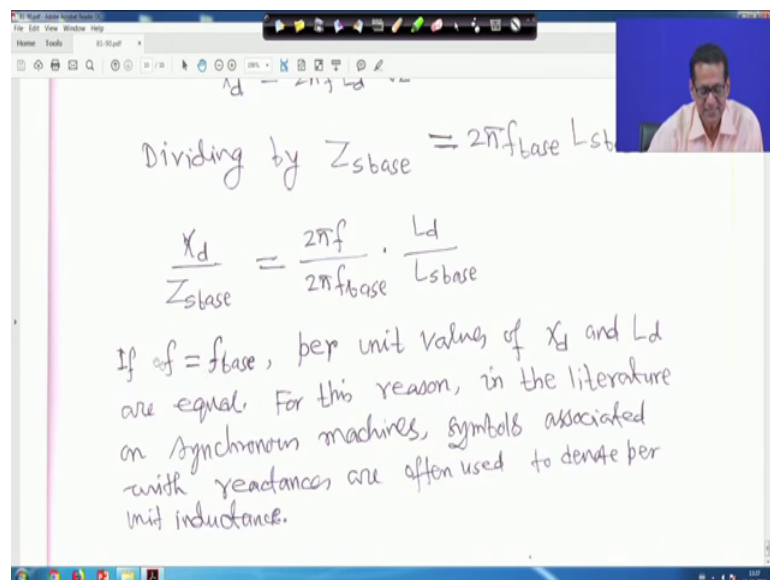
Dividing by  $Z_{sbase} = 2\pi f_{base} L_{sbase}$

$$\frac{X_d}{Z_{sbase}} = \frac{2\pi f}{2\pi f_{base}} \cdot \frac{L_d}{L_{sbase}}$$

If  $f = f_{base}$ , per unit values of  $X_d$  and  $L_d$  are equal. For this reason, in the literature

Now, if you divide both side  $X_d$  upon  $Z_s$  base. So, it is  $2\pi f$  upon  $2\pi f$  base into  $L_d$  upon  $L_s$  base right.

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Dividing by  $Z_{sbase} = 2\pi f_{base} L_{sbase}$

$$\frac{X_d}{Z_{sbase}} = \frac{2\pi f}{2\pi f_{base}} \cdot \frac{L_d}{L_{sbase}}$$

If  $f = f_{base}$ , per unit values of  $X_d$  and  $L_d$  are equal. For this reason, in the literature on synchronous machines, symbols associated with reactances are often used to denote per unit inductance.

But  $f$  is equal to  $f$  base right per unit values of  $X_d$  and  $L_d$  actually are equal because  $f$  is equal to  $f$  base because  $f$  base here may synchronous machine rotating at a say your synchronous speed and  $f$  base is nothing. But if it is 60 Hz it will be 60 Hz if it is 50 Hz it will be 50 Hz. So,  $f$  is equal to  $f$  base. So, this term will be cancel two  $\pi f$  is equal to  $f$  base and this is  $2\pi f$  base. So, ultimate it will become  $X_d$  per unit is equal to



Ld per unit. So, in per unit whenever say per unit reactance means it is per unit your inductance also right.

So, so for this reason in the literature as your, and since what you call on synchronous machine symbols associated reactances are often used to denote per unit inductance right So, numerically if it is given per unit reactance when it is per unit inductance also if it is given per unit inductance means it is per unit reactance also right so right

(Refer Slide Time: 23:59)

The image shows a screenshot of a presentation slide titled "Summary of Per Unit Equations". The slide content is as follows:

Summary of Per Unit Equations.

Base quantities

Stator base quantities

3-phase  $VA_{base}$  = Volt-Ampere rating of machine, VA.

$e_{base}$  = peak phase-to-neutral rated voltage, V.

$f_{base}$  = rated frequency, Hz.

$I_{base}$  = peak line current, Amp.

The slide is displayed in a software window with a toolbar at the top and a sidebar on the right containing options like Comment, Combine Files, Organize Pages, Redact, Protect, Optimize PDF, Fill & Sign, Send for Signature, Send & Track, and More Tools. A small video inset in the top right corner shows a man speaking.

So with this, what you call this per unit this is now summary of this per units equation right. So, base quantities now stator base quantities three phase volt ampere base is equal to volt ampere rating of machine volt ampere base is equal to peak phase to neutral, what you call p phase your sorry peak phase to neutral rated voltage in volt.

(Refer Slide Time: 24:37)

The screenshot shows a presentation slide with handwritten equations for base quantities. The equations are:

$$I_{sbase} = \frac{3\text{-phase } VA_{base}}{(3/2) E_{sbase}}$$
$$Z_{sbase} = \frac{E_{sbase}}{I_{sbase}}, \Omega$$
$$\omega_{base} = 2\pi f_{base}, \text{ elect. rad/sec.}$$
$$\omega_{mbase} = \omega_{base} \frac{2}{p_p}, \text{ mech. rad/sec}$$
$$L_{sbase} = \frac{Z_{sbase}}{\omega_{base}}, \text{ Henry}$$

The slide also features a video feed of a presenter in the top right corner and a sidebar with navigation and tool options.

So, whatever we have studied the summary I have made a summary for you  $f_{base}$  is equal to rated frequency in hertz  $i_{sbase}$  is equal to peak line current ampere that is 3 phase volt ampere base divided by 3 by 2  $s_{base}$  right. Similarly  $Z_{sbase}$  is equal to  $s_{base}$  upon  $i_{sbase}$  ohm right.  $\omega_{base}$  is equal to  $2\pi f_{base}$  that is electrical radian per second right.

(Refer Slide Time: 24:55)

The screenshot shows a presentation slide with handwritten equations for base quantities. The equations are:

$$\omega_{base} = 2\pi f_{base}, \text{ elect. rad/sec.}$$
$$\omega_{mbase} = \omega_{base} \frac{2}{p_p}, \text{ mech. rad/sec}$$
$$L_{sbase} = \frac{Z_{sbase}}{\omega_{base}}, \text{ Henry}$$
$$\psi_{sbase} = L_{sbase} i_{sbase}, \text{ Wb-turns}$$

The slide also features a video feed of a presenter in the top right corner and a sidebar with navigation and tool options. A circled number '92' is visible in the bottom right corner of the slide.

And omega m base is equal to omega base into 2 by pf that is mechanical radian per second. Then L s base will be Zs base upon omega base this is in Henry. And psi s base will be L s base into i s base that is turn that is y bar turns right.

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Rotor base quantities:

$$i_{fd\text{base}} = \frac{L_{ad}}{L_{fd}} i_{s\text{base}}, \text{ Amp.}$$

$$i_{kd\text{base}} = \frac{L_{ad}}{L_{kd}} i_{s\text{base}}, \text{ Amp.}$$

$$i_{kq\text{base}} = \frac{L_{aq}}{L_{kq}} i_{s\text{base}}, \text{ Amp.}$$

3-phase VA base

So, next rotor is base quantities this is a summary. So, ifd base will be L ad upon L fd into i s base ampere this will help you to solve numericals right. i kd base will be L ad upon L kd L kd is base ampere. ikq base will be L aq upon L kw L akw i s base ampere. Ef d base will be three phase volt ampere.

(Refer Slide Time: 25:39)

$$i_{kq\text{base}} = \frac{L_{aq}}{L_{kq}} i_{s\text{base}}, \text{ Amp.}$$

$$e_{fd\text{base}} = \frac{3\text{-phase VA}_{\text{base}}}{i_{fd\text{base}}}, \text{ Volt.}$$

$$Z_{fd\text{base}} = \frac{e_{fd\text{base}}}{i_{fd\text{base}}}, \Omega$$

$$= \frac{3\text{-phase VA}_{\text{base}}}{i_{fd\text{base}}^2}, \Omega$$

$$Z_{fd} = \frac{3\text{-phase VA}_{\text{base}}}{i_{fd\text{base}}^2}, \Omega$$

Based upon ifd base this is in volt right. z fd base is equal to ef d base upon ifd base this is ohm right. Is equal to three phase volt ampere divided by i fd square base right so, this is the summary.

(Refer Slide Time: 25:55)

The screenshot shows a presentation slide with handwritten equations for base impedances. The equations are:

$$Z_{fdbase} = \frac{V_{base}}{I_{fdbase}^2}, \Omega$$

$$= \frac{3\text{-phase } VA_{base}}{I_{fdbase}^2}, \Omega$$

$$Z_{kdbase} = \frac{3\text{-phase } VA_{base}}{I_{kdbase}^2}, \Omega$$

$$Z_{kqbase} = \frac{3\text{-phase } VA_{base}}{I_{kqbase}^2}, \Omega$$

And zkd base is equal to three phase volt ampere base upon i kd square base this is ohm right. Z k q base is equal to three phase volt ampere base upon i kq square base. So, this is your ohm right.

(Refer Slide Time: 26:13)

The screenshot shows a presentation slide with handwritten equations for base inductance and time constants. The equations are:

$$L_{fdbase} = \frac{Z_{fdbase}}{\omega_{base}}, \text{ Henry}$$

$$L_{kdbase} = \frac{Z_{kdbase}}{\omega_{base}}, \text{ Henry}$$

$$L_{kqbase} = \frac{Z_{kqbase}}{\omega_{base}}, \text{ Henry.}$$

$$t_{base} = \frac{1}{\omega_{base}}, \text{ sec}$$

If d base is equal to Z fd base upon omega base this is Henry. Then L kd base is equal to Z kd base upon omega base, this is also Henry. L k q base is equal to z k q base upon omega base this is also Henry.

(Refer Slide Time: 26:25)

The screenshot shows a presentation slide with the following handwritten equations:

$$L_{kdbase} = \frac{Z_{kdbase}}{\omega_{base}}, \text{ Henry}$$

$$L_{kqbase} = \frac{Z_{kqbase}}{\omega_{base}}, \text{ Henry.}$$

$$t_{base} = \frac{1}{\omega_{base}}, \text{ sec.}$$

$$T_{base} = \frac{3\text{-phase } VA_{base}}{\omega_{mbase}}, \text{ N-m.}$$

T base 1 upon omega base this is second right. And therefore, t base is equal to nothing three phase volt ampere at torque this is multi time this is torque base.

(Refer Slide Time: 26:43)

The screenshot shows a presentation slide with the following handwritten equations and text:

$$L_{kdbase} = \frac{Z_{kdbase}}{\omega_{base}}, \text{ Henry}$$

$$L_{kqbase} = \frac{Z_{kqbase}}{\omega_{base}}, \text{ Henry.}$$

$$t_{base} = \frac{1}{\omega_{base}}, \text{ sec.}$$

$$T_{base} = \frac{3\text{-phase } VA_{base}}{\omega_{mbase}}, \text{ N-m.}$$

Complete set of Electrical Equations in

Is equal to three phase volt ampere base upon omega mechanical base, this is Newton meter right. Complete set of electrical equations will be seen the next lecture.

Thank you very much. We will be back again.