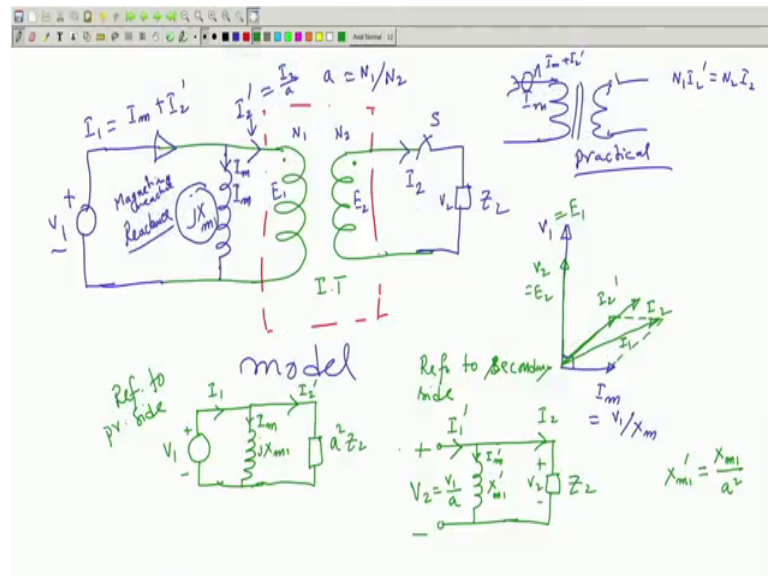


Electrical Machines - I
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Lecture - 09
Modelling of Practical Transformer - II

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Welcome to the 9th lecture and you recall we were gradually going towards a practical transformer. And in my last class, this was the slide, where this is a practical transformer. Here there is no X_m connected; you must understand that this is a practical transformer in the laboratory ok; two secondary, two primary, there was nothing like X_m connected there.

But it was our thought process, which lead us to believe that this whatever is happening to a practical transformer, what is happening with S opened, current turn from the supply is finite, magnetizing current I_m and when S closed, it must be I_m plus I_2' dashed, because net MMF in the circuit has to be $N_1 I_m$, why? Because flux in the core is decided by supply voltage and frequency, nobody has any say on that.

But if you are trying to disturb the secondary, I mean if you are trying to pass some current through the secondary, primary cannot be a mere specter at to this happening. It will react immediately by drawing an extra current I_2' dashed, and that I_2' dashed cannot be of any magnitude; it has to be I_2' by a , so that $N_1 I_2'$ dashed becomes equal to $N_1 I_m$

I_2 dashed becomes equal to $N_2 I_2$, so that net MMF once again is $N_1 I_m$ and this is what we have discussed last class.

So, this is a reactance, this is an ideal transformer and it correctly models it. So, V_1 , I_m I have drawn, then I am completing the phasor diagram once again. And suppose, this is V_1 to the ideal transformer applied voltage is V_1 , so this is E_1 , this is E_2 and this is V_2 ; V_2 , E_2 , etcetera, they are all same.

So, depending upon the turns ratios your, so this V_1 is nothing but E_1 , they still remains nothing in between, and your this will be your V_2 , which is same as E_2 . And this is suppose the load power factor decide what is the current here I_2 , then current drawn from the primary will be I_2 dashed, I_2 we have got, get I_2 dashed.

And then this I_2 dashed, plus this I_m if you add, you will get primary current I_1 , understood. This is how magnetizing current can be taken into account of a it is somewhat a practical transformer, still not a full practical transformer. I have neglected, so many other things till now, only magnetizing current, I have been incorporated and for that an external element $j X_m$ is to be selected.

If you like you put $j X_m$; side 1 ok, because we have seen parameter value changes from side this side to that side and so on. Therefore, what will be the equivalent circuit looking from the primary side, it will be V_1 , here is a reactance; no windings this one $j X_m$ and here will be the impedance a square z_2 , you know this will be the equivalent circuit refer to the primary side $j X_m$.

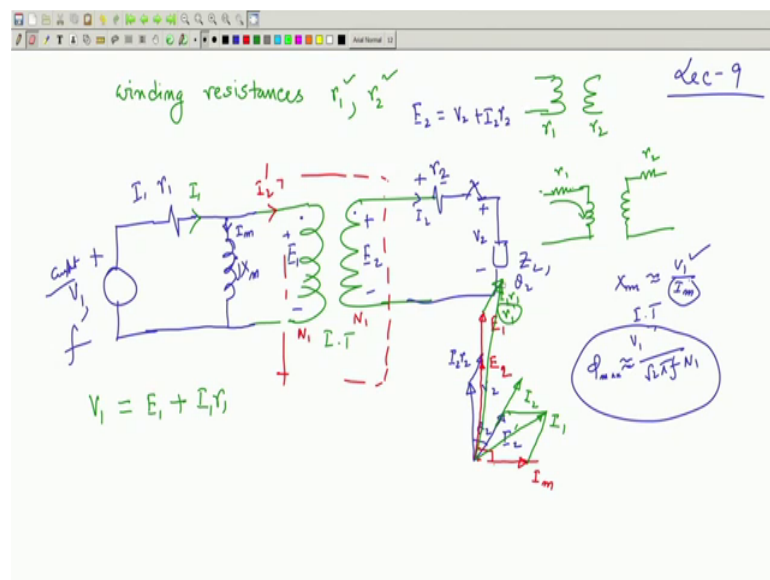
So, whatever impedance, voltage, this that are there and this current I will show as I_2 dashed reflected current and this current I will show as magnetizing current and this current is your I_1 . Mind you I am not drawing, but these are dots that is very important with respect to this. So, this is the equivalent circuit refer to the primary side.

What will be the equivalent circuit refer to the secondary side, refer to source side; refer to primary or source side, primary side. And refer to load side or secondary side, it will be secondary voltage remain secondary voltage; this will be z_2 , secondary things I should not disturbed, they are already there z_2 , this voltage is V_2 , this current is I_2 , I will show it.

And this follow the transfer of impedance from this to that side will be X_{m1} dashed, what is X_{m1} dashed; it will be X_{m1} by a square and what is this V_2 ? V_1 by a. So, this is the equivalent circuit refer to the secondary side. So, you solve this you write I_m dashed (Refer Time: 06:46) reflected current. And then you will what current you will get, I will get I_1 dashed.

So, you either solve this circuit get everything, because if this somewhat practical transformer, solve this circuit get I_2 dashed and then predict what will be I_2 . So, people always refer to work on a equivalent circuit instead of drawing some coupled coils, then individually calculated. We can do that, but this is a better way of doing things.

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After I have done this, our next reality which is present in a practical transformer is let us assume, I will assume winding resistance. Till now, I have neglected winding resistances r not 0, that is r_1 is present, r_2 is present that is the what is r_1 , this winding; one side, side 1 resistance and this winding as also got r_2 , because resistance is after all ρl by a .

So, there is some resistivity of this conducting material, some cross sectional area, so many turns are there, so many length. Of course, the resistance will be pretty small, it is made of very good material for example, copper. But none the less there will be some finite resistances of primary side and secondary side.

And it looks like, this is resistance which is of course, distributed can be considered to be lumped and I can show it like this. Similarly for this coil, this resistance, I will consider it to be lumped and represent it like this, this is how I can represent.

Now, the question is how this r_1 , r_2 should be shown in this transformer. In this transformer, there was finite magnetizing current; no resistance, no leakage flux, fine and this is I_m magnetizing current taking care of by $n X_m$.

So, now once again I will add some parameters to this circuit that is r_1 , r_2 in appropriate place that is very important, so that effect of r_1 and r_2 will be addressed by this model. Question is where should I put r_1 , should I put it here, should I put it there, where that is an interesting question.

This portion is ideal mind you therefore, if there is winding resistance, what it is going to do. There will be whenever this coil will carry current your practical transformer, there will be a voltage drop here in the resistance. Applied voltage minus this drop is going to create flux, not this full voltage is going to produce your magnetizing current, because a portion of the voltage will be dropped in r_1 , got the point.

Therefore, in this circuit I will spoil this circuit, do not mind; what I will do now if I add something here, our previous thing will also get disturbed. So, what I am telling is this what I will do now listen carefully, here I will draw the ideal transformer and I will put a dotted box around it in order to indicate that and then these are the terminals of the ideal transformer ok.

And then I am telling to this ideal transformer, this winding is not purely this thing. So, so you are there will be resistances in series, I will connect it here; which is small resistance none the less r_1 , it will come in series.

Now, the question is should I put that magnetizing current branch X_m , before this or after this, I must put it after this $j X_m$. Similarly here of course, there is no magnetizing branch, r_2 is simply comes here. I have shown only one way I am showing not like this resistance; because these resistances are small, it only indicates that a small resistance in series. Therefore, you know this is this thing and here is your supply voltage, frequency f .

So, whatever current it supplies which is decided by it may be the load connected here, ultimately some current is drawn and when that current flows through the winding, there will be a voltage drop r_1 ; and that voltage drop must be subtracted from your supply voltage and the remaining voltage is responsible for creating flux and giving you the transformer action, so that is why r_1 should not be shown here, it must be after this. Therefore, this is V_1 , this is ideal transformer, this is r_2 .

Now, the moment r_1 is present I must also distinguish between E_1 and V_1 , there will be a drop here in series. X_m what do you think; its value will be low or high, its value will be high you should not choose a magnetic material which requires very large magnetizing current. See X_m is what, X_m is approximately V_1 by I_m , I should not choose a magnetic material which requires very high value of magnetizing current, then X_m will be low. Better and better material I use, which is not certainly ideal its μ_r tending to infinity, may be μ_r is equal to 5000 quite a large number.

So, I_m will be small, V_1 is fixed, so X_m is general high that is why, I have written capital letter and we so many turns, just to indicate that ok, r_1 is small, small r_2 . Therefore, the magnetizing current which will be flowing here, I_m is not V_1 by X_m ; V_1 minus this drop divided by X_m .

And as you know, depending upon the degree of loading the magnitude of the current drawn from the supply will change. Therefore, drop in this resistance, V_1 minus this drop is the voltage what is coming here across the ideal transformer. Therefore, the magnitude of the voltage applied to this ideal transformer is will also we will not remain constant, as we were thinking in case of ideal transformer apply V_1 . I was telling the level of flux ϕ_{max} is equal to applied voltage in an ideal transformer is equal to $\frac{V_1}{2\pi f N_1}$ and if applied voltage and frequency is constant, ϕ_{max} gets decided.

But now I come to know ok, the applied voltage to this ideal transformer strictly speaking will not remain constant because of the presents of r_1 , this is constant mind you; V_1 is constant no doubt, but V_1 minus this drop is what is applied here, what is this drop, this drop depend on the magnitude of I_1 this your practical transformer is carrying and the magnitude of I_1 has I_2 dashed plus I_m , I_2 dashed depend on I_2 and depend on Z_2 .

So, by as you change z_2 , I_2 is going to change, I_2 dashed is going to change therefore, I_1 is also going to change, therefore drop in r_1 is not constant as you change loading. Therefore applied voltage to this ideal primary winding of this ideal transformer; strictly speaking is not constant, only consolation is this r_1 is quite small.

Therefore, what people say is this ok, ϕ_{max} will be approximately constant, because you have not certainly designed a transformer with high value of r_1 and r_2 , then no one is going to buy your transformer I mean why, there will be unnecessary power loss in the windings. Therefore, you must see that very good material is used for example, copper whose resistivity is very low. So, ρ by a the winding resistances are small, so that that way this assumption that ϕ_{max} practically remain same from no load to full load is good enough.

Anyway none the less, let us see try to draw the phasor diagram of ah this one and try to understand the implication of this. Now, what I will be doing here listen carefully; here I will start with E_1 and E_2 ok, this voltage and this voltage. Mind you, here is now that V_2 and E_2 will not be same is not, similarly V_1 and E_1 will not be same, because in between this two sources some $I_1 r_1$ drop here, some $I_2 r_2$ drop here will come, they cannot be same.

But none the less, we can do this things. Suppose how to start the phasor diagram drawing, I will do it like this. Suppose, I draw it will be slightly clumsy, but let it be, but follow my argument ok; you will draw V_2 first whatever it will be; I draw V_2 arbitrarily, vertically. If I know V_2 , then I can fix up where the I_2 will be is not, because load power factor angle is known. Suppose, power factor angle of the load is θ_2 , V_2 I_2 , I have drawn with S closed.

Then I will say, look here your E_2 is equal to V_2 plus $I_2 r_2$ follow the logic, the diagrams may be a bit clumsy, but this is what is going to happen. Suppose, V_2 is known, V_2 I_2 you draw; then I have to add to V_2 , this $I_2 r_2$ drop. Then I will add it what is there and $I_2 r_2$ drop will be very small, because r_2 is small, $I_2 r_2$ follow the logic that is all.

If you do that, then what I am telling you will get your E_2 . The induced voltage in this ideal transformer, which I will draw by a red line here, this will be your E_1 ; E_2 sorry. It is an ideal transformer, this is E_2 , then you can confidently draw your E_1 . If number of

turns of this side is higher, then its length of E_1 will be higher than E_2 , E_1 is drawn. So, this will be your E_1 .

And if this is E_1 , this is E_2 , your magnetizing current will be perpendicular to E_1 , 90 degree lagging. Here is your finite magnetizing current, I_m is not? I have got E_1 , so E_1 by $j X_m I_m$, I get; so, this is the magnetizing current. And it is an ideal transformer with S opened, I_2 was 0 this current was 0 with S closed, I_2 dashed will appear here, nowhere else it is an ideal transformer this portion.

So, I_2 is known and I_2 dashed will be in same phase with that so I will get I_2 dashed; whether its length will be higher than I_2 or not that depends upon the ratios. So, this will be your . .

Student: (Refer Time: 23:33).

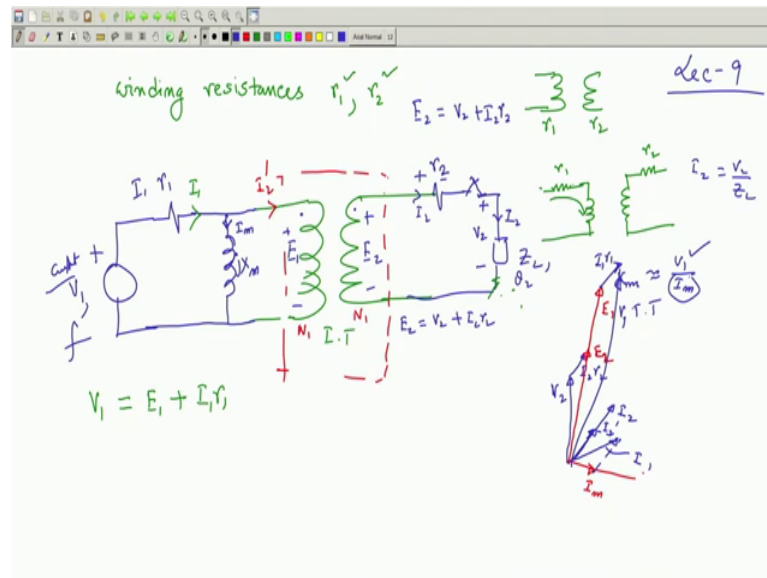
It will be less. So, what I will do is I will make these as I_2 , so that; so this is I_2 and suppose, please note this changes and this is I_2 dashed, because I have shown E_1 is higher. So, reflected current must be lower I_2 dashed, so this is your I_2 dashed.

Then I will say that this current I_1 will be I_2 dashed plus I_m . So, I_m is known, I_2 dashed is known; so I will add this two, mind you I have shown I_m slightly higher length it is not so, I_m is small, anyway whatever I have drawn. So, this will be your I_1 and if this is I_1 , then I will say your V_1 must be equal to E_1 plus $I_1 r_1$. So, E_1 is known to this add $I_1 r_1$ parallel to this and from this to this, then wherever you will end up that will be your V_1 .

I think you have got the idea, see life will be will not be so much complicated as we proceed, but what I am telling this is exactly what, how to draw phasor diagram. Start with I could start with V_1 , but it is better you, because the primary current drawn decided by load, it is much more easier. So, I will quickly go through this step, so that you can understand.

Suppose, switch is closed ok, I will clean this and once again redraw. So, I will just I will (Refer Time: 26:00), but the idea is very important you must keep this in mind. So, I am redrawing once again very quickly, what I am telling ok, you have close the switch the circuit is operating, choose V_2 , you start with V_2 ok.

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Voltage applied across the load is V_2 , then no one can contest me, then the current is I_2 is V_2 by Z_2 and I_2 suppose lagging power factor load, I_2 will lag here, I_2 will be higher low voltage side; I assumed I mean, while drawing ok, so I_2 . The moment you know I_2 you can find out E_2 , because E_2 is V_2 this drop is this plus minus, so V_2 plus $I_2 r_2$. So, V_2 plus $I_2 r_2$ you draw, this lengths are small.

And then you get this length to be E_1 , I am simply repeating, because for the first time you are doing this you get E_1 , E_2 sorry. If you get E_2 , this ratio of voltage is N_1 by N_2 absolutely no doubt; mind you this V_1 by V_2 may not be N_1 by N_2 strictly speaking, but this induced voltages are N_1 . So, E_2 is this, then I know E_2 and E_1 are in phase, so I can get E_1 assuming N_1 is greater than N_2 , it will be this.

Then once I know I_1 , I know the magnetizing current which will be 90 degree lagging. And this current is small, let me draw it now correctly I_m small current; I_m and once I know I_m and I_2 is known. So, I_2 dashed will be this one here will be your I_2 dashed. So, current drawn from the source will be this plus this, this is your I_1 ; and if this is I_1 , use this one E_1 plus $I_1 r_1$, whatever it is, parallel to this $I_1 r_1$ and you get your V_1 .

Anyway I am stopping now, but try to understand. So, this will now truly represent, it is somewhat practical circuit with the finite magnetizing current and winding resistance. In the next class, we will bring other realities into an ideal transformer to get a somewhat better picture of the model.

Thank you.