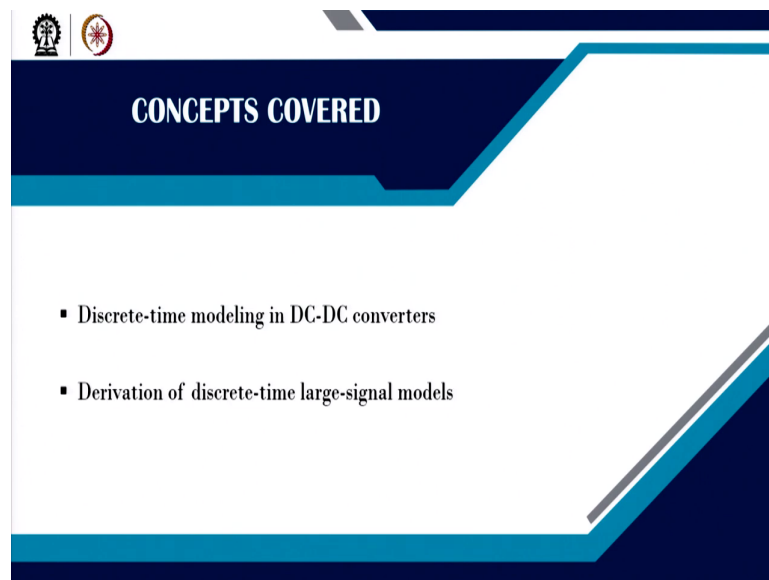


Digital Control in Switched Mode Power Converters and FPGA-based Prototyping
Prof. Santanu Kapat
Department of Electrical Engineering
Indian Institute of Technology, Kharagpur

Module - 04
Modeling Techniques and Mode Validation using MATLAB
Lecture - 34
Derivation of Discrete-Time Large-Signal Models

Welcome. In this lecture, we are going to derive the complete Discrete Time model Large Signal Model.

(Refer Slide Time: 00:31)



The slide features a dark blue header with two logos on the left and the title 'CONCEPTS COVERED' in white. Below the header, there is a white area containing two bullet points. The slide is decorated with blue and white geometric shapes on the right side.

- Discrete-time modeling in DC-DC converters
- Derivation of discrete-time large-signal models

So, we will discuss the first discrete-time modeling in the DC-DC converter that we started in the previous lecture. And then we want to derive the complete discrete time large signal model.

(Refer Slide Time: 00:40)

State-Space Matrices of a Synchronous Buck Converter

Synchronous buck converter

$$A_1 = A_2 = A = \begin{bmatrix} -\frac{(r_c + \alpha r_c)}{L} & -\frac{\alpha}{L} \\ \frac{\alpha}{C} & -\frac{\alpha}{RC} \end{bmatrix}$$

$$B_1 = \begin{bmatrix} \frac{1}{L} & \frac{\alpha r_c}{L} \\ 0 & -\frac{\alpha}{C} \end{bmatrix} \quad B_2 = \begin{bmatrix} 0 & \frac{\alpha r_c}{L} \\ 0 & -\frac{\alpha}{C} \end{bmatrix}$$

in absence of current sink

So, first, if we take a synchronous buck converter and this is the circuit diagram more or less practical synchronous buck converter, then we know how to get A 1 A 2 matrix and for r 1 is equal to r 2, then this A 1 A 2 matrix are same that we have discussed. Then we will get beyond the B 2 matrix and if we ignore the external current load if we ignore this part then you will get this matrix if it is ignored, ok.

(Refer Slide Time: 01:12)

Waveforms under Trailing-Edge Modulation with Interval-2 Sampling

Trailing-edge PWM

Two subsequent sampling points

Now, so this is the diagram of this complete interval 2 sampling that we have discussed; how does it work? So, we will take the output voltage sample right here. So, we will take the

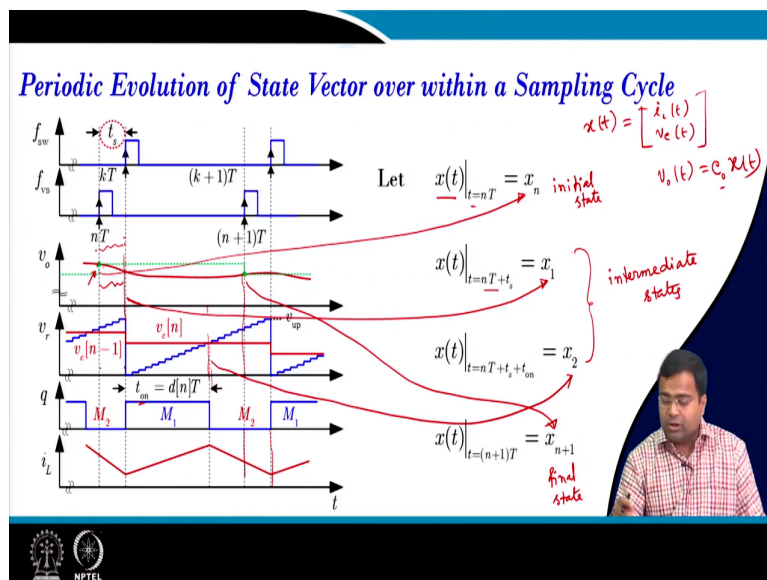
sample, somewhat earlier than the actual switch turns on because we are talking about the trailing edge modulation. So, this is under trailing edge modulation trailing edge PWM.

So, under this modulation we want to take the sample earlier than the switch is turned on and that is why, it is called interval 2 because as if we are taking the sample during the switch-off time, which is mode 2. What does it do? So, we take the sample here and we will use this sample in the subsequent cycle, but this sample is used and it is this time is provided for ADC conversion time and the computational time and then your control output; that means, the output of the controller is ready after this time.

So, then your actual DPWM start and here we are taking a step k approximation of the ramp signal. So, if we ignore the effect of quantization, then how do you derive the discrete-time model? So, you see we want to derive the discrete-time model between two subsequent sampling points, two subsequent sampling points. So, earlier we wanted to derive a point. So, earlier we want to derive between two switching points there was no delay, but if there is a delay in the sampling.

So, we will take the sampling clock as a reference clock to derive the discrete-time model. So, that is used for nT and n plus 1.

(Refer Slide Time: 03:04)



Now, how do we start? So, if you take this waveform, let x of t ; that means, any state variable. So, what are the state variables? We know the state variable here we have taken, the

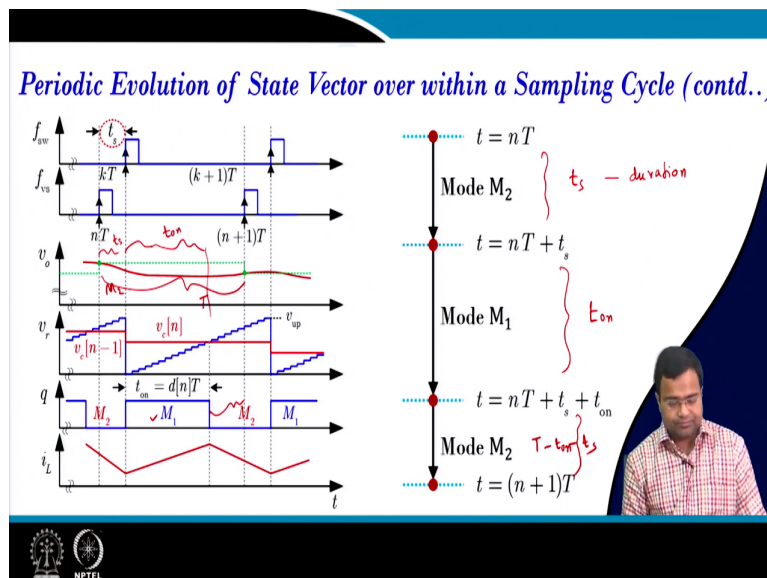
inductor current, and the output sorry capacitor voltage. And the output voltage will be C matrix time x of t right, that we know. So, C we want to make C 0 because C is the output capacitor just to separate that notation, we are using C 0.

Now, if you take the sample here you will see that first, it will undergo mode 2, and at this point, we are calling the state variable we are calling x_n . Then at this point what is the state variable? We will call here x_1 . So, this is my x_1 , then it will come to this point when the switch will change its state.

So, this point we will call x_2 and if you see the duration, the first point will come to T equal to nT , the second point will come to $nT + t_s$ this is the duration t_s and the third point will come $nT + t_s + d n t_{on}$, that is the on-time t_{on} x_2 and the final point the point which will be here; that means, the sampling point; that means, this point we are taking this state here $x_1 t$.

So, your intermediate variables are the intermediate states, right? This is my initial state and this is my final state. We want to write the final state in terms of the initial state and we want to substitute the intermediate state. How to start with?

(Refer Slide Time: 05:10)

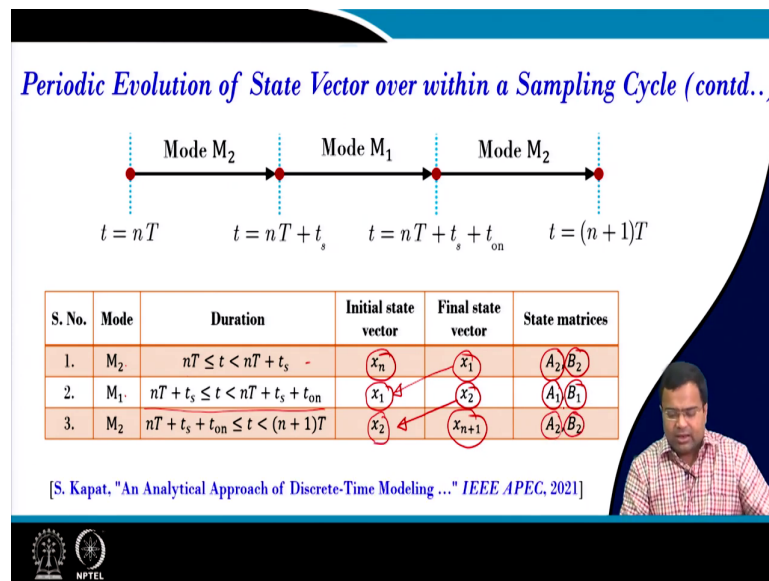


So, let us start t equal to nT , then it will undergo mode 2. So, this is my mode 2, then so the duration of mode 2 is t_s , that is the duration. Then mode 1, the duration is what? It will be t_{on} and this is under mode 1. So, you can see it is mode 1, then the rest duration which is this

one; what is the duration? This duration if you different then it will be total time; that means, t minus t on minus t s right if you just subtract this; that means, from this point to this point is our total time, this point to this point in my time is t .

So, this point is t s and this point is t on. So, naturally, the rest of the point will be t minus t on minus t s ok.

(Refer Slide Time: 06:14)



So; that means, this is the model diagram; that means, how the state propagates. So, the total duration; means, first serial M 2, then M 1 then M 2. So, it will be for the duration $n T$ to $n T$ plus t s, then it will be the duration between $n T$ plus t s to $n T$ plus t s plus t on and then $n T$ plus t s plus t on till the n plus $1 T$.

And for this mode x_n is the initial state x_1 is the final state and the matrix corresponds to off-state matrix A_2 and B_2 . Then this mode's initial state is x_1 , this state will become an initial state and the final state is x_2 in this mode 1, it will be A_1 and B_1 matrix will be considered. Again this will be the initial state for the next cycle, the next configuration.

So, x_2 is the initial state and the final state is x_{n+1} and in this mode again it is mode 2. So, A_2 and B_2 matrix. So, in that way we will get; so we will get detail about this, there are different books also you can refer to in this paper.

(Refer Slide Time: 07:26)

Discrete-Time Large-Signal Model with Resistive Load


S. No.	Mode	Duration	Initial state vector	Final state vector	State matrices
1.	M ₂	$nT \leq t < nT + t_s$	x_n	x_1	$A_2 = A, B_2 = 0$
2.	M ₁	$nT + t_s \leq t < nT + t_s + t_{on}$	x_1	x_2	$A_1 = A, B_1$
3.	M ₂	$nT + t_s + t_{on} \leq t < (n+1)T$	x_2	x_{n+1}	$A_2 = A, B_2 = 0$

State-space solution

$$x(t) = e^{A(t-t_0)} x(t_0) + (e^{A(t-t_0)} - I) A^{-1} B u$$

$t_0 = nT \Rightarrow x(t_0) = x_n$
 $t = nT + t_s \Rightarrow x(t) = x_1$

Mode M₂ $\Rightarrow x_1 = e^{(A t_s)} x_n$



So, here we want to get the complete state. So, we know for each mode the state space solution. So, for this state, it starts with x_1 . So, you substitute here, what is the t_0 ? So, t_0 is nT right, that is the initial time for this state, and t is equal to x_n , which is starting value of x_n . Because if you take this mode the time starts t_0 from equal to nT its starting value is right. And what is the n value? n value of this state will be $nT + t_s$. So, x_1 is equal to x of t .

Then mode 2, is under mode 2. And what is the duration? If you take the difference it will be a t_s and during mode 2 of a buck converter, there is no output voltage disconnected. So, your solution is simply A into t_s because we know this solution. If you substitute total t , what is total t ? t equal to $nT + t_s$ and t_0 equal to nT . So, then the difference is t_s , this one will be x_n that we have defined and since B_2 is 0. So, it will simply be this solution.

(Refer Slide Time: 08:42)

Discrete-Time Large-Signal Model with Resistive Load (contd..)

S. No.	Mode	Duration	Initial state vector	Final state vector	State matrices
1.	M ₂	$nT \leq t < nT + t_s$	x_n	x_1	$A_2 = A, B_2 = 0$
2.	M ₁	$nT + t_s \leq t < nT + t_s + t_{on}$	x_1	x_2	$A_1 = A, B_1$
3.	M ₂	$nT + t_s + t_{on} \leq t < (n+1)T$	x_2	x_{n+1}	$A_2 = A, B_2 = 0$


State-space solution

$$x(t) = e^{A_q(t-t_o)} x(t_o) + (e^{A_q(t-t_o)} - I) A_q^{-1} B_q u$$

$A_1 = A_2 = A$

$t_o = nT + t_s \Rightarrow x(t_o) = x_1$
 $t = nT + t_s + t_{on} \Rightarrow x(t) = x_2$

Mode M₁ $\Rightarrow x_2 = e^{A t_{on}} x_1 + (e^{A t_{on}} - I) A^{-1} B_1 v_{in}$



Next for mode two, again you substitute. Here, what is the initial state is my $nT + t_s$. So, $nT + t_s$ and the state is x_1 and the final state $nT + t_s + t_{on}$ and the state is x_2 . So, what is this difference? This difference will be simply t_{on} . So, it will be t_{on} and the initial state here will be x_1 for this mode and the final state is x_2 and this state of a buck converter your now input voltage is connected, it is beyond the matrix.

So, you will write this and again the solution here this invertible A_q ; that means, A_1 is invertible and here for a buck we know that $A_1 = A_2 = A$ we have taken. So, here we will get the solution.

(Refer Slide Time: 09:32)

Discrete-Time Large-Signal Model with Resistive Load (contd..)

S. No.	Mode	Duration	Initial state vector	Final state vector	State matrices
1.	M ₂	$nT \leq t < nT + t_s$	x_n	x_1	$A_2 = A, B_2 = 0$
2.	M ₁	$nT + t_s \leq t < nT + t_s + t_{on}$	x_1	x_2	$A_1 = A, B_1$
3.	M ₂	$nT + t_s + t_{on} \leq t < (n+1)T$	x_2	x_{n+1}	$A_2 = A, B_2 = 0$

State-space solution


$$x(t) = e^{A(t-t_o)} x(t_o) + (e^{A(t-t_o)} - I) A^{-1} B u$$

$T - t_{on} - t_s$

$t_o = nT + t_s + t_{on} \Rightarrow x(t_o) = x_2$

$t = (n+1)T \Rightarrow x(t) = x_{n+1}$

Mode M₂ $\Rightarrow x_{n+1} = e^{A(T-t_{on}-t_s)} x_2 + (0)$



Next, for the third mode, we will substitute what is the initial value. It is x_2 . What is the initial time? $nT + t_s + t_{on}$. What is the final time? $(n+1)T$. So, what is the difference? It will be t ; that means if you subtract it will be you know $T - t_{on} - t_s$. And during this state x_2 is the initial state, x_{n+1} is the final state for this mode and again it is the off state of a buck converter where the input voltage is disconnected. So, there will be no solution here. So, it is 0, right?

(Refer Slide Time: 10:13)

Discrete-Time Large-Signal Model with Resistive Load (contd..)

S. No.	Mode	Duration	Initial state vector	Final state vector	State matrices
1.	M ₂	$nT \leq t < nT + t_s$	x_n	x_1	$A_2 = A, B_2 = 0$
2.	M ₁	$nT + t_s \leq t < nT + t_s + t_{on}$	x_1	x_2	$A_1 = A, B_1$
3.	M ₂	$nT + t_s + t_{on} \leq t < (n+1)T$	x_2	x_{n+1}	$A_2 = A, B_2 = 0$


$x_n \rightarrow x_1 \rightarrow x_2 \rightarrow x_{n+1}$

Mode M₂: $x_1 = e^{At} x_n$

Mode M₁: $x_2 = e^{A t_{on}} x_1 + (e^{A t_{on}} - I) A^{-1} B_1 u_{in}$

Mode M₂: $x_{n+1} = e^{A(T-t_{on}-t_s)} x_2$

[S. Kapat, "An Analytical Approach of Discrete-Time Modeling ..." IEEE APEC, 2021]



So, now if you combine together mode 2; that means, how it is propagated? So, your propagation is x_n propagated to x_1 it is here, then mode 1, x_1 propagates to x_2 it is coming like this, then mode 2 x_2 propagates to x_{n+1} . So, we will get x_{n+1} with detail and you can get the detail process in this paper.

(Refer Slide Time: 10:40)

Discrete-Time Large-Signal Model with Resistive Load (contd..)

Eliminate x_1 and x_2 to obtain x_{n+1} in terms of x_n

Mode M₂: $x_1 = e^{At_s} x_n$


Mode M₁: $x_2 = e^{At_s} x_1 + (e^{At_{on}} - I)A^{-1}B_1 v_{in}$
in terms of x_n

Mode M₂: $x_{n+1} = e^{A(T-t_{on}-t_s)} x_2$

Large-Signal Discrete-Time Model

$$x_{n+1} = e^{AT} x_n + e^{A(T-t_{on}-t_s)} (e^{At_{on}} - I) A^{-1} B_1 v_{in}$$

Handwritten notes:
 $e^{At_s} \cdot e^{A(t_s+t_{on})} = e^{A(t_s+t_{on}+T-t_{on}-t_s)} = e^{AT}$
 if $A_1 A_2 \neq A_2 A_1$



So, the complete solution x_{n+1} , if you propagate; that means, you will backpropagate. So, first, you start with eliminate x_1 x_2 to obtain x_{n+1} in terms of x_n . So, in mode 2, we have know x_1 and x_2 also we know. Now, you substitute; that means, this x_1 you substitute here, and then it will be in terms of x_2 and the x_2 term, x_2 you substitute here sorry. So, in this case, it will be in terms of x_n and you substitute x_2 since x_1 is already replaced. So, the whole term will be in terms of x_n .

So, you will get the complete discrete time model like this and you see for all these three cases it will be product; that means, e to the power $A t_s$ into e to the power $A t_{on}$ into e to the power $A T$ minus t_{on} minus t_s . So, since all a matrix is identical. So, you can simply write e to the power; that means, e to the power t_s plus t_{on} plus T minus t_{on} minus t_s . So, it will be e to the power $A T$ that is it.

But, if the $A_1 A_2$ matrix is different; that means, can you always write e to the power $A_1 t_1$ into e to the power $A_2 t_2$ will not be equal to e to the power $A_1 t_1$ plus $A_2 t_2$ if $A_1 A_2$ is not equal to $A_2 A_1$. If we can show that means, commutative property if they are not equal then we cannot write.

But if the matrix is identical then there is no problem. So, x a square. So, here since this case is very straightforward for buck converter you can very easily get it, but you will get a different scenario for a boost converter when the A 1 A 2 matrix is different. Then this property cannot be satisfied. So, you cannot write like this. So, then you have to write in the product.

(Refer Slide Time: 13:05)

Complete Discrete-Time Large-Signal Model with Resistive Load

Large-Signal Discrete-Time Model

$$x_{n+1} = e^{AT} x_n + e^{A(T-t_{on}-t)} (e^{At_{on}} - I) A^{-1} B_1 v_{in}$$

Handwritten annotations on the slide:

- $x_{n+1} = \begin{bmatrix} i_L(n+1) \\ v_C(n+1) \end{bmatrix}$
- $x_n = \begin{bmatrix} i_L(n) \\ v_C(n) \end{bmatrix}$
- $f(x_n, t_{on}) = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix}$
- Dimensions: 2×1 for x_{n+1} , 2×2 for e^{AT} , 2×2 for $e^{A(T-t_{on}-t)}$, 2×2 for $(e^{At_{on}} - I)$, 2×1 for B_1 , 1×1 for v_{in} .

[S. Kapat, "An Analytical Approach of Discrete-Time Modeling ..." IEEE APEC, 2021]

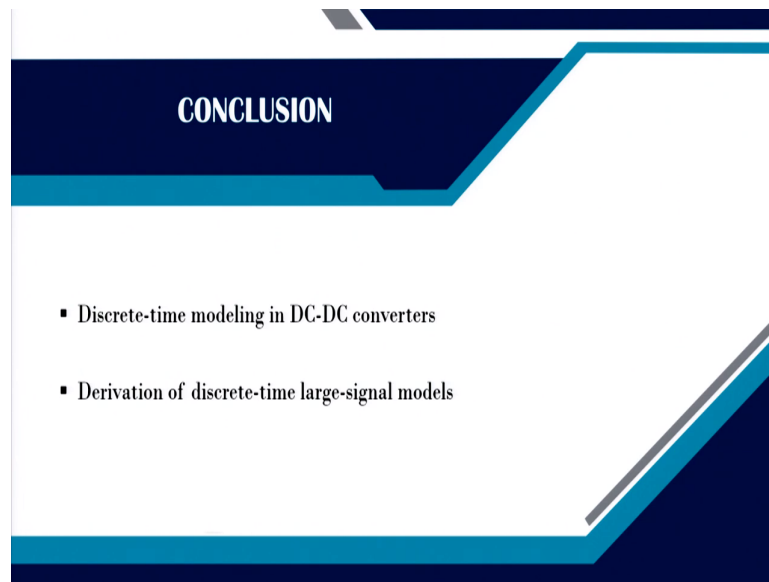
So, the complete discrete-time model for a buck converter can be derived by this method. As a complete discrete-time model and we will take this complete discrete time model as a vector function, because this x_{n+1} , is consisting of $i_L(n+1)$ and $v_C(n+1)$. So, naturally, this one will be a vector consisting of f_1 and f_2 . Why we are writing? Because we want to show this the large signal model can be used to derive the discrete-time small signal model using the Jacobian approach ok.

So, right now I am just representing this in the complete vector form. So, this will be a 2 cross 1 matrix, because there are only two states and you will find this matrix will be 2 cross 2, again this will be a 2 cross 2 matrix and B matrix is 2 cross 1, input is 1 cross 1 and this whole term again 2 cross 2, this will be also 2 cross 2. So, we will use this vector function to derive a discrete-time small signal model in the subsequent lecture.

So, we will get detail about this how this vector function can be used for deriving discretized small signal models, straight away mathematically. And that can be used for you know for buck-boost as well as it can be used for you know constant on-time modulation, constant

off-time modulation, then trailing edge modulation, leading-edge modulation, and all the derivations of small signal models are summarized in this paper. So, for detail, you can refer to this paper.

(Refer Slide Time: 14:47)



So, in summary, we have discussed discrete-time modeling in DC-DC converters, then we have discussed the derivation of discrete-time large-signal models. So, here we have shown only a buck converter, but as we move forward for stability analysis we can also do the for a boost converter because we already know the method. So, I think this is enough for today, we want to stop it here.

Thank you very much.