

**Analog Integrated Circuits**  
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**Lecture – 28**  
**Telescopic OpAmp – 4**

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Telescopic Opamp-4

1) Input & Output CM range  
 2) Slew rate

Input CM =  $V_{CM,in}$   
 as  $V_{CM,in}$  reduces  
 $\rightarrow I_{D1}$  &  $I_{D2}$  remain @  $I_D$   
 as long as  $M_0$  is in sat.  
 $\rightarrow V_{GS1}$  &  $V_{GS2}$  remain constant  
 $\rightarrow V_{XY}$  follows change in  $V_{CM,in}$

We are now going to look at the input and output common mode ranges of the telescopic op amp as well as its slew rate. So, let us look at the input common mode range. So, let us assume that the input common mode is equal to the  $V_{CM,in}$  and we want to find out the minimum and maximum values of  $V_{CM,in}$ . So, of course, to when you apply an input common mode, you connect the 2 inputs together and apply  $V_{CM,in}$ .

Now, suppose you started reducing  $V_{CM,in}$ . So, because the total current in  $M$  naught remains 2,  $i$  naught till  $M$  naught goes into triode the 2 transistors  $M_1$  and  $M_2$  will continue to have a current  $i$  naught each and therefore,  $V_{GS1}$  and  $V_{GS2}$  will remain constant. So, therefore, the voltage that at  $xy$  reduces. So, as  $V_{CM,in}$  reduces. So, the points we will make  $i_{D1}$  and  $i_{D2}$  remain at  $i$  naught as long as  $M$  naught is in saturation this means that  $V_{GS1}$  and  $V_{GS2}$  remain constant.

Finally this means that  $v_{xy}$  follows the change in  $V_{CM,in}$ . So, as  $V_{CM,in}$  is reduced  $v_{xy}$  also reduces till  $M_0$  goes to the edge of triode region.

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$$\min V_{CM,in} = V_{xy,min} + V_{as1} = V_{Dsat0} + V_{as1}$$

As  $V_{CM,in}$  is increased:

$\rightarrow V_{xy}$  follows  $V_{CM,in}$ ,  $V_{as1}$  &  $V_{as2}$  stay constant

$V_{D1} = V_{B3} - V_{as3}$

$M_1$  enters triode when  $V_{CM,in} = V_{D1} + V_{T1}$

$\leftarrow V_{D1} = V_{B3} - V_{as3}$

$\max V_{CM,in} = V_{B3} - V_{as3} + V_{T1}$

$ICMR = \{ V_{Dsat0} + V_{as1}, V_{B3} - V_{as3} + V_{T1} \}$

Therefore minimum VCM is reached when the transistor M1 is just at the edge of the triode region at that point the voltage of that at x y is  $V_{Dsat0}$  and. So, this is nothing, but  $V_{Dsat0}$  plus  $V_{GS1}$  one just remember  $V_{Dsat0}$  is calculated at a current  $I_{D1}$   $V_{GS1}$  is calculated at a current of  $I_{D1}$ .

Now, next we will see what happens as you start increasing the value of value of VCM in. So, now, suppose we start increasing the value of VCM in as you can see you can follow the same set of arguments. So, as VCM in is increased you can say that  $v_{xy}$  follows VCM in and therefore,  $M_1$  is actually moving further away from triode there is no problem and  $V_{GS1}$  and  $V_{GS2}$  stay constant and both of them carry a current now as please note that the voltage at the drain of  $M_1$  which we shall call  $V_{D1}$  is biased  $V_{D1}$  is actually at a voltage equal to  $V_{B3}$  minus  $V_{GS3}$ .

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1) Input & Output CM range  
2) Slew rate

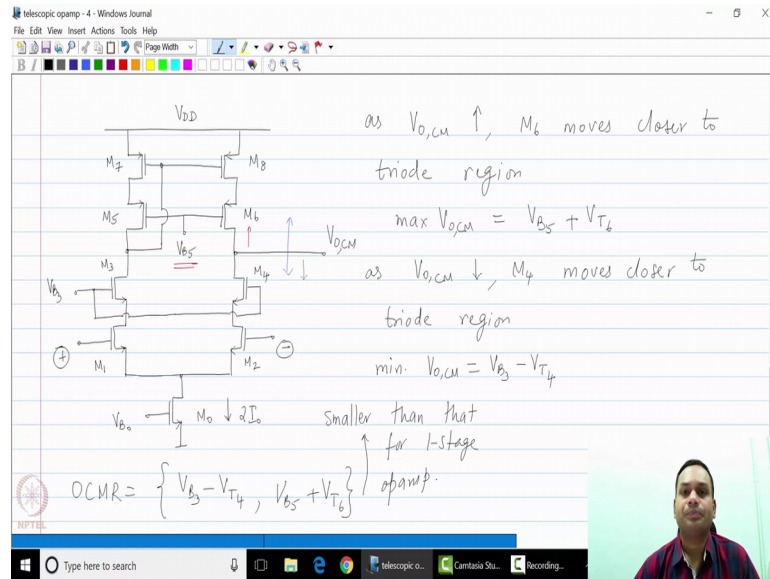
Input CM =  $V_{CM,in}$

as  $V_{CM,in}$  reduces  
 $\rightarrow I_{D1}$  &  $I_{D2}$  remain @  $I_0$   
 as long as  $M_0$  is in sat.  
 $\rightarrow V_{GS1}$  &  $V_{GS2}$  remain constant  
 $\rightarrow V_{XY}$  follows change in  $V_{CM,in}$

Therefore one equals  $V_{B3} - V_{GS3}$  where  $V_{GS3}$  is calculated at a current  $i$  naught please note that because the current stays constant  $V_{GS3}$  also stays constant now please note that for  $M_1$   $V_{CM,in}$ . So, the gate voltage is increasing whereas, this is constant at  $V_{B3} - V_{GS3}$ . So,  $M_1$  enters triode when  $V_{CM,in}$  is one threshold voltage larger than  $v_t$ . So, in other words. So, the maximum value of  $V_{CM,in}$  is  $V_{B3} - V_{GS3} + V_{T1}$ . So, so the input common mode range. So, the input common mode is  $V_{Dsat} + V_{GS1}$  comma  $V_{B3} - V_{GS3} + V_{T1}$ .

So, please note that the input common mode range is slightly different from the from that for the one stage opamp; now what about the output common mode range so.

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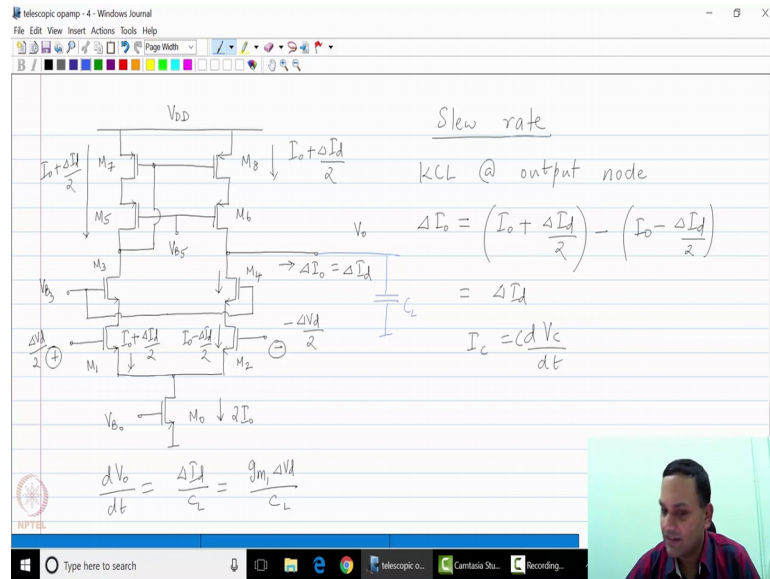


Let us again take the same opamp, but now we are now going to see what happens you know what is the maximum voltage at the output versus the minimum voltage at the output. So, of course, as let us call the output common mode as the OCM. So, as  $V_{OCM}$  increases you will find that  $M_6$  has a constant gate voltage  $V_{B5}$  whereas, its drain voltage is increasing  $M_6$  moves closer and closer to the triode region and therefore, the maximum value of  $V_{OCM}$  is nothing, but  $V_{B5}$  plus  $V_{T6}$ .

Similarly, as  $V_{OCM}$  decreases you will find that the gate of  $M_4$  is constant and  $M_4$  moves closer to triode region this means that the minimum value of the o c M is nothing, but  $V_{B3}$  minus  $V_{T4}$  therefore, the output common mode range is  $V_{B3}$  minus  $V_{T4}$  comma  $V_{B5}$  plus  $V_{T6}$  as you can see this depends on  $V_{B3}$  and  $V_{B5}$  numbers, but in general you will find that the output common mode range of the telescopic op amp is smaller than that for the one stage opamp.

Naturally because you now have large number of transistors and you cannot support a large enough common mode range or spin at the output node.

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Finally we will look at the slew rate of the telescopic op amp. So, we are now interested in slew rate. So, to find out the slew rate. So, we will now apply increments of  $\Delta V_D$  by 2 and minus  $\Delta V_D$  by 2 at the inputs as you might imagine the currents are now  $I_D + \frac{\Delta I_D}{2}$  and downwards and  $I_D - \frac{\Delta I_D}{2}$  from downwards to  $M_2$  and these are the incremental currents  $\frac{\Delta I_D}{2}$  and minus  $\frac{\Delta I_D}{2}$  are the incremented currents through  $M_1$  and  $M_2$ .

Now what happens to these incremental currents. So, these currents flow through the other transistors. So,  $I_D + \frac{\Delta I_D}{2}$  through  $M_3$ ,  $M_5$  and  $M_7$  is  $I_D + \frac{\Delta I_D}{2}$  and this gets mirrored through between  $M_7$  and  $M_8$  to give you  $I_D + \frac{\Delta I_D}{2}$  by through by 2 through  $M_8$  and  $M_6$ . Now what happens to this current flowing through  $M_2$  that current flowing through  $M_2$  flows through  $M_4$  also.

So, if you were to find out the total  $\Delta I_o$  you do that by applying kcl at output node you find that  $\Delta I_o$  is the total current leaving the node should be the sum of the currents entering the node the sum of the current entering the node from  $M_6$  is  $I_D + \frac{\Delta I_D}{2}$  and the current entering the node from  $M_4$  is minus of  $I_D - \frac{\Delta I_D}{2}$ .

So, this is nothing, but  $\Delta I_D$ . So, the current  $\Delta I_D$  flows through the output now where does this current flow of course, the output will have a load capacitance  $C_L$  and therefore, this  $\Delta I_D$  current charges the load capacitance. So, therefore, for the

capacitance you write  $i_c$  is  $DVC$  by  $dt$  times  $C$ ; this means that the value of  $dv$  by  $dt$  is nothing, but  $\frac{\Delta i_D}{C}$  and this of course, for small signals is nothing, but  $\frac{M_1 \Delta V_D}{C_L}$  now if you start increasing the value of  $\Delta V_D$  you will find that since  $M_1$  carries  $i_{D1} + \Delta i_D$  the current through  $M_1$  increases and the current through  $M_2$  decreases.

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as  $|\Delta V_D| \uparrow \Rightarrow I_{D1} \uparrow \text{ \& } I_{D2} \downarrow$   
 eventually  $2I_o$  flows through  $M_1$  &  $0$  flows in  $M_2$   
 $\Delta I_o = 2I_o$   
 $\Rightarrow \frac{dV_o}{dt} = \frac{2I_o}{C_L} = \text{positive slew rate}$   
 $= \text{negative slew rate}$

So, as the magnitude of  $\Delta V_D$  increases. So,  $i_{D1}$  increases and  $i_{D2}$  decreases eventually  $2i_{D1}$  current flows through  $M_1$  and  $0$  current flows through  $M_2$ . So, all the current has shifted into transistor  $M_1$ . So, in this case you will find that the in this case let us write down the expression for the total current flowing into the output node. So, that is  $\Delta i_o$ . So, if you were to apply a really large step at the input. So, so you would find that you would have a current  $2i_{D1}$  would have  $0$  current therefore,  $M_2$  and  $M_4$  would be cut off this current  $i_{D1}$  flows through  $M_3$   $M_5$  and  $M_7$  and this gets mirrored into  $M_8$  and  $M_6$ .

Again if you apply  $kcl$  at the output node it is clear that  $\Delta i_{D1}$  is equal to  $2i_{D1}$  this means that  $V_{D_o}$  by  $dt$  is  $2i_{D1}$  over a  $C_L$ . Now if you were to increase the input step any further the output cannot rise any faster because the op amp can only source a maximum current of  $2i_{D1}$ . So, this is turn the positive slew rate of the op amp now you can apply a negative slew rate you can apply a negative step to the op amp and in that case  $M_1$   $M_3$   $M_5$  and  $M_7$  are cut off and. So, are  $M_6$  and  $M_8$  and  $M_2$  and

M4 carry the full current of  $2I_{bias}$  and discharge the load capacitance. So, it turns out that this is also equal to the negative slew rate. So, the positive slew rate is equal to the negative slew rate for the telescopic opamp also.