

## Power Electronics

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Lecture - 34

### Dynamic Model of Induction Motor Part – II

Last class we derived the real and the imaginary component of the stator and rotor voltage equation with respect to a general rotating DQ reference phase and the general rotating with a speed of  $\omega_{\rho}$ ; if you see here,  $d\rho$  by  $dt$  is equal to  $\omega_{\rho}$ . So with respect to,  $\rho$  is measured with respect to our stationary alpha beta axis. Now, based on this equation, let us format our dynamic dq equivalent circuit.

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The image shows a screenshot of a presentation slide with handwritten mathematical equations. At the top right, it says  $\frac{d\rho}{dt} = \omega_{\rho}$ . Under the heading "STATOR", the equations are:

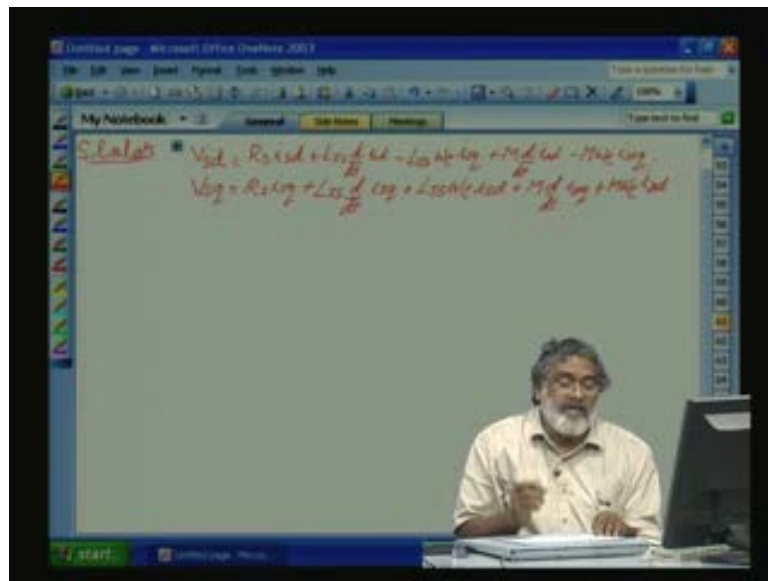
$$V_{sd} = R_s i_{sd} + L_{\sigma s} \frac{d i_{sd}}{dt} - L_{\sigma s} \omega_{\rho} i_{sq} + \frac{M}{L_r} \frac{d i_{rd}}{dt} - \omega_{\rho} \frac{M}{L_r} i_{rq}$$
$$V_{sq} = R_s i_{sq} + L_{\sigma s} \frac{d i_{sq}}{dt} + L_{\sigma s} \omega_{\rho} i_{sd} + \frac{M}{L_r} \frac{d i_{rq}}{dt} + \omega_{\rho} \frac{M}{L_r} i_{rd}$$

Under the heading "ROTOR", the equations are:

$$0 = R_r i_{rd} + L_{\sigma r} \frac{d i_{rd}}{dt} - L_{\sigma r} (\omega_{\rho} - \omega_m) i_{rq} + \frac{M}{L_s} \frac{d i_{sd}}{dt} - \frac{M}{L_s} (\omega_{\rho} - \omega_m) i_{sd}$$
$$0 = R_r i_{rq} + L_{\sigma r} \frac{d i_{rq}}{dt} + L_{\sigma r} (\omega_{\rho} - \omega_m) i_{rd} + \frac{M}{L_s} \frac{d i_{sq}}{dt} + \frac{M}{L_s} (\omega_{\rho} - \omega_m) i_{sq}$$

So,  $d\rho$  by  $dt$  is  $\omega_{\rho}$ ; this is the general rotating reference frame speed. So, V is again, we will rewrite this one and formulate our dynamic equivalent circuit model.

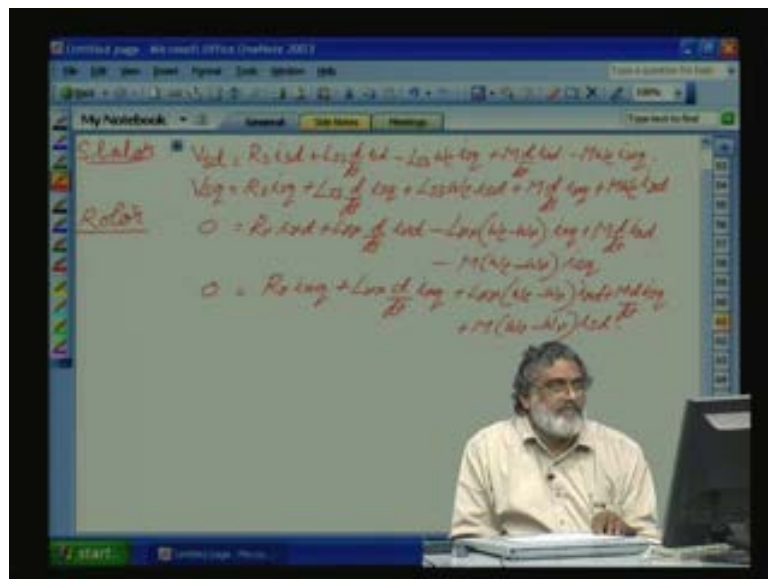
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So, let us write down. Stator  $V_{sd}$  is equal to  $R_s i_{sd}$  plus  $L_{sd} \frac{d i_{sd}}{dt}$  minus  $L_{sm} \omega_r i_{sq}$  plus  $M \frac{d i_{sd}}{dt}$  minus  $M \omega_r i_{sq}$ ; this is the stator  $V_{sd}$ . Then stator  $V_{sq}$ ,  $V_{sq}$  is equal to, see if you see here the stator, the  $d$  by  $dt$   $i_{sd}$ , this will take care of the magnitude variation and this will take care of the speed variations.

But due to the speed variation; it will go to the, time will go to the  $q$  axis. So,  $V_{sq}$  is equal to  $R_s i_{sq}$  plus  $L_{sd} \frac{d i_{sq}}{dt}$  plus  $L_{sm} \omega_r i_{sd}$  plus  $M \frac{d i_{sq}}{dt}$  plus  $M \omega_r i_{rd}$ ; this is the stator. Now, let us take the rotor.

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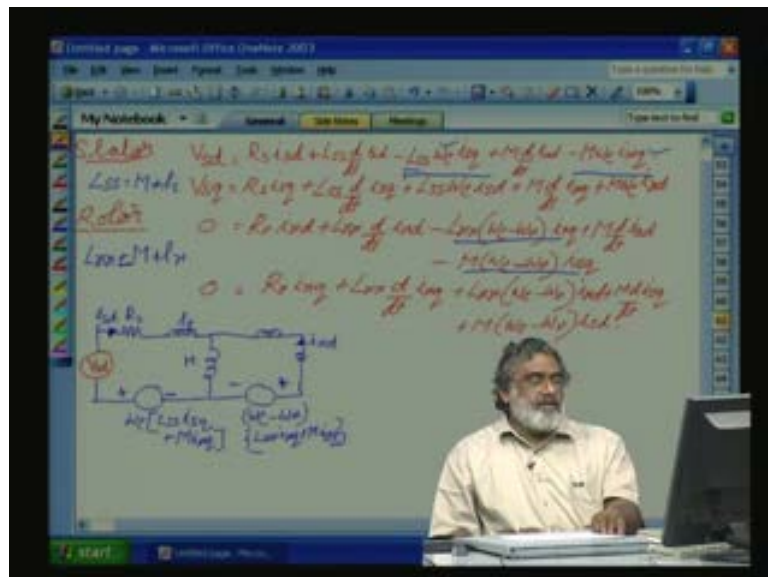
So here,  $dq$  axis is applied voltage is zero. So, that is equal to  $R_r i_{rd}$  plus  $L_{rr} \frac{d i_{rd}}{dt}$  minus  $L_{rsm} \omega_r i_{sq}$  minus  $M \frac{d i_{rd}}{dt}$  minus  $M(\omega_r - \omega_r) i_{sq}$ . See, the voltage time due to the rotation at the rotor is the relative speed. Rotor is already rotating with  $\omega_r$  and our rotating reference

frame is  $\omega_r$ . So, relative speed is  $\omega_r$  by  $\omega_r$ . But if you see the stator, it is  $\omega_r$  because stator is stationary. So the rotating voltage, the voltage due to the rotation,  $\omega_r$  is depending on the speed of our reference frame.  $\omega_r$  minus  $\omega_r$  into  $i_{rq}$  plus  $M$  into  $d$  by  $dt$   $i_{sd}$  minus  $M$  into  $\omega_r$  minus  $\omega_r$  into  $i_{sq}$ ; this is the rotor  $d$  axis.

Now, let us take the rotor  $q$  axis. This is equal to zero is equal to  $R_r i_{rq}$  plus  $L_{rr} d$  by  $dt$   $i_{rq}$  plus  $L_{rr}$  into  $\omega_r$  minus  $\omega_r$  into  $i_{rd}$  plus  $M$  into  $d$  by  $dt$   $i_{sq}$  plus  $M$  into  $\omega_r$  minus  $\omega_r$  into  $i_{sd}$ . Now, let us based on this dynamic equation  $d$  and  $q$ ; see, what we did? First we defined the voltage and voltage space vector for the stator as well as the rotor with respect to the  $\alpha\beta$  reference frame axis. Then we transferred whole voltage turn to the general rotating reference frame axis  $dq$ , the speed is the position of the general rotating reference frame axis with respect to  $\alpha\beta$  axis is  $\theta$  at any instant and  $D\theta$  by the speed of rotation is  $\omega_r$ . Then we separated into real and imaginary component; the  $d$  and  $q$  component.

Now, we got the dynamic equation control conditions. That means when the amplitude as well as the speed or the frequency varies. Let us take the first stator equation. So, there is a  $V_{sd}$  voltage we are applying.

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So, this is  $V_{sd}$ . Here, maybe we will use a different colour, so it will be clear, applied voltage. So here, there is a drop  $R_s i_{sd}$ ; this is  $R_s$ ,  $i_{sd}$  is this one,  $i_{sd}$  is flowing like this. Then  $L_{ss} d$  by  $dt$   $i_{sd}$ ; so  $L_{ss}$  is equal to, if you see  $L_{ss}$  is equal to  $M$  plus leakage inductance  $L_s$ . So, let us draw the leakage inductance here. This is  $L_s$  and there is  $L_{ss}$  into  $i_{sd}$ . So, this  $i_{sd}$  is going to the mutual inductance also, then only you can say  $L_{ss}$ . So, mutual inductance here, this is  $M$ ,  $L_{ss} i_{sd}$ .

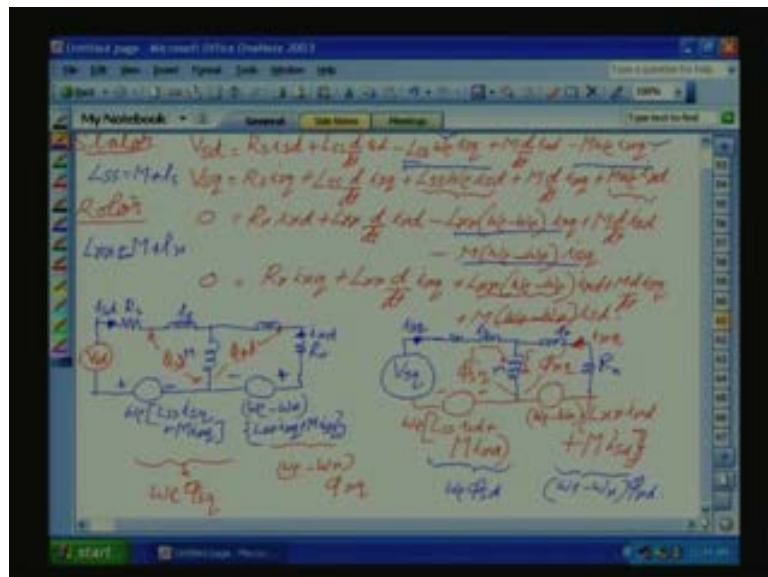
Now, if you see here, these are voltage terms due to the rotation that means this one and this one that is this one and this one. This we can write down; if you see here,  $L_{ss}$  plus  $\omega_r i_{sq}$  plus  $i_{rq}$ , so this is due to the  $q$  axis. So, the rotational voltage due to the current in one axis will appear at the other axis, other orthogonal axis. So, before coming

to that one, let us take the rotor term also. Rotor term  $R_r i_{rd}$ ; so we have  $R_r$  here,  $R_r i_{rd}$  here also plus  $L_{rr} \frac{d}{dt} i_{rd}$ .  $L_{rr}$  is equal to  $M$  plus  $L_r$ , leakage inductance. So, we have the leakage inductance here. So, this also comes here. So, through the mutual inductance term here, both  $i_{sd}$  and  $i_{rd}$  is flowing. So,  $i_{rd}$  is here.

Now, what is this  $L_{ss} \omega \sigma i_{sq}$  plus  $i_{rq}$ ? This is we can say, the flux  $\sigma i_{sq}$ . So, we will come to that one now so that we will follow. So, there is a rotational voltage term appearing at the stator due to the  $i_{sq}$  and  $i_{rq}$ . That means current flowing through the q axis equivalent circuit, these two and this is minus, that shows; see, we have taken current entering as positive, so this is minus means current comes,  $i_{sd}$  it comes like this. So, we can take this time as negative positive. So, current entering is taken as positive, so the term is like this. So, this is a function of  $\omega \rho$ ,  $\omega \rho$  multiplied by  $L_{ss} i_{sq}$  plus  $M$  into  $i_{rq}$ . What is this one? It will come to that one.

Similarly the rotor circuit, the D axis,  $L_{rr}$  that is this term,  $i_{sq}$ ; here also it is negative, so with respect to  $i_{rd}$  if it is a negative means we will put it like this and go. So, this is negative, this is positive because  $i_{rd}$  is going like this,  $i_{rd}$  is entering the negative side; so that conversion we follow. So, this will be equal to, this also rotational voltage term that is also equal to  $\omega \rho$  minus  $\omega r$  into  $L_{rr} i_{rq}$  plus  $M$  into  $i_{sq}$ ; this is the d axis.

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Similarly, we can write the q axis. Let us start with the  $V_{sq}$ , applied voltage  $V_{sq}$  and this is the  $i_{sq}$ . So, we have the  $R_s$  term here,  $R_s i_{sq}$ , again the leakage  $L_s$  and the mutual  $M$  here. Similarly, for the rotor side also you have leakage inductance  $L_r$  and the resistance term  $R_r$ , this is  $R_r$ , rotor resistance. Here also the voltage term, so the voltage term polarity if you see here; for the q axis, this is the one and the next one is due to the rotational. So  $i_{rq}$ ,  $M$  into  $i_{rq}$ ;  $i_{rq}$  is coming in this way,  $i_{sd}$   $i_{sq}$  is coming there,  $i_{sq}$  it goes through  $L_s$  plus  $M$  that is why  $L_{ss}$ .

Now, that voltage time, we will put it like this here, due to rotation. Stator side it is  $\omega \rho$  into  $L_{ss} i_{sd}$ ,  $L_{ss} i_{sd}$  plus  $M i_{rd}$  plus  $M$  into  $i_{rd}$ ; this is the term and polarity this is positive that means current is entering the positive terminal notation like this. Here

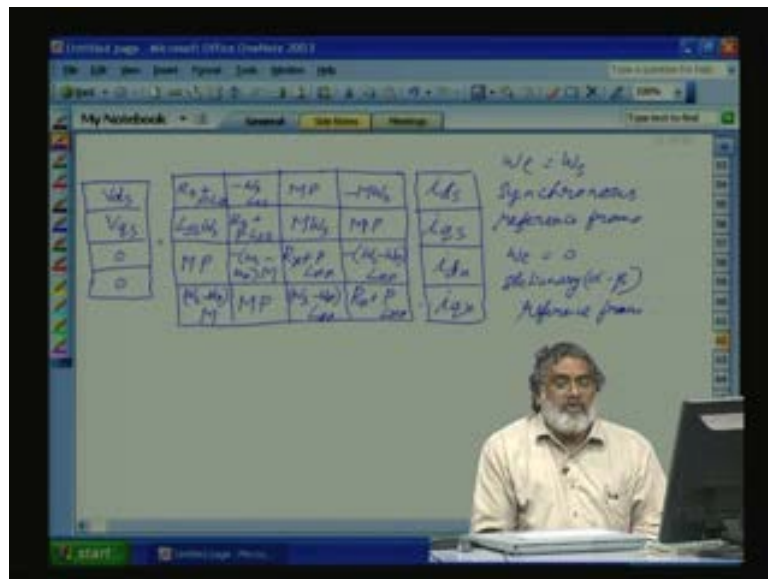
also, rotor side also  $i_{rq}$ , there is  $\omega \sigma - \omega_r$ ,  $\omega \rho - \omega_r$  that is this two terms  $L_{rr} i_{rd}$  plus  $M$  into  $i_{sd}$ , this is the term. So, if you see here,  $L_{ss} i_{sq}$ ,  $L_{ss} i_{sq}$  is this one,  $L_s$  plus  $M$  and  $i_{sq}$  is flowing here, then  $M$  into  $i_{rq}$ ,  $i_{rq}$  is here. So, there is a current  $i_{rq}$  flowing here and  $i_{sq}$  flowing here.

So, if you see here, what is this one? This is called that is  $i_{sq}$  plus  $i_{rq}$  that is called  $i_{s\phi}$  flux  $i_{s\phi}$ ,  $\phi_{sq}$ . Similarly, this one is equal to  $\phi_{s\phi}$ ; this is the flux coupling, this mutual and this is  $L_r$ . Similar way, we can say this one is  $\phi_{rd}$  flux, this is  $\phi_{sd}$ , the flux which is coupling this  $L_s$  and due to this  $L_s$  and the current flowing through it, this is  $\phi_{sd}$ .

So, if you see here, what is this equation?  $\omega \rho$ , this equation is equal to  $\omega \rho$  into  $\phi_{sq}$ , this one. And, what is this one?  $\omega \rho - \omega_r$  into  $L_{rr} i_{rq}$ ,  $L_{rr} i_{rq}$  means plus  $M i_{sq}$ ;  $L_{rr} i_{rq}$  is this one total flux plus  $M$  into  $i_{sq}$ . So, this is  $i_{s\phi}$ ; this is equal to into  $\phi_{rq}$ . So, due to the flux and the rotation, in the  $q$  axis, there is a voltage time in the  $d$  axis stator and the rotor.

Similarly here, what is this term? This term will be if you see here, this is  $\omega \rho$  into  $L_{ss} i_{sd}$  that is this one plus  $M$  into  $i_{rd}$  that is this is  $\phi_{sd}$ ,  $\omega \rho \phi_{sd}$  and similarly we can find out this term will be  $\omega \rho - \omega_r$  into  $\phi_{rd}$ . So, our dynamic equivalent circuit is ready. This can also we can represent in this, in a matrix form. See, using this equation, let us say, let us go to the next page now.

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See we have, let us take  $\omega \rho$  is equal to  $\omega_s$  if you put it our dynamic equivalent circuit will be with respect to synchronous reference frame.  $\omega \rho$  is equal to zero, then it will be stationary reference frame, stationary that means  $\omega \rho$  is equal to zero means  $dq$  will be aligned with  $\alpha\beta$  that is stationary  $\alpha\beta$  the reference frame.

So, let us write down in matrix form, the equation. This will be we have four stator voltages that is  $V_{ds}$   $V_{qs}$  and the rotor zero is equal to you have four currents also, so this



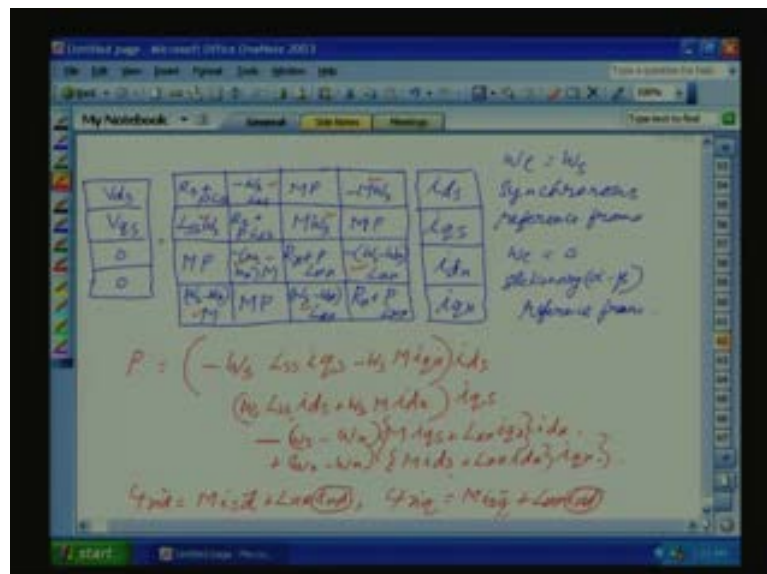
is a 4 by 4 matrix; 1 2 3 4, here also 2 3 4, this is our  $i_{ds}$ ,  $i_{qs}$ ,  $i_{dr}$ ,  $i_{qr}$ . So  $V_{ds}$ , the first term;  $R_s$  plus  $d$  by  $dt$  of  $L_{ss}$ ,  $d$  by  $dt$  we will say  $P L_{ss}$ ,  $P$  is an operator,  $P$  is equal to  $d$  by  $dt$ . Then this one will be minus  $\omega_s L_{ss}$ , term will be here. Here will be  $M$  into  $P$ ,  $P$  is  $d$  by  $dt$ ; then minus  $M \omega_s$  that is a stator  $d$  voltages.

Then stator  $q$  voltages are  $L_{ss} \omega_s$ , then  $R_s$  plus  $P L_{ss}$ ,  $P$  means  $d$  by  $dt$ ,  $d$  by  $dt$  of  $i_{qs}$ . Then  $M$  into  $\omega_s$ , see that is we are taking everything into synchronous reference frame that is the subscript  $s$ , synchronous reference  $\omega_s$ . Then  $M$  into  $P$ ,  $P$  is the  $d$  by  $dt$ . Again here,  $M$  into  $P$ , rotor the relative speed is  $\omega_s$  minus  $\omega_r$  minus of  $\omega_s$  minus  $\omega_r$  into  $M$ . Then rotor resistance and the self-inductance term  $R_r$  plus  $P$  into  $L_{rr}$ , then minus  $\omega_s$  minus  $\omega_r$  into  $L_{rr}$ . So, rotor  $d$  axis voltage term is over.

Now, rotor  $q$  axis; this is  $\omega_s$  minus  $\omega_r$  into  $M$ , then  $M$  into  $P$ ,  $\omega_s$  minus  $\omega_r$   $L_{rr}$ . Then  $R_r$  plus  $P L_{rr}$ ,  $P$  is the  $d$  by  $dt$  is an operator. See, we have the, we got the machine dynamic voltages within matrix form. So here, we can either use equivalent circuit or this one. If you see here, what is the torque produced? The torque produced is power divide by the frequency of the operation.

So, if you see here, in this equation, the power, the torque is power divide by the speed. So, power means voltage into current. So, the torque produced and that voltage which is responsible for the torque is due to the rotational voltage because of the rotation, we get the torque. So, all the rotational voltage is multiplied by current that is the power which is responsible for the torque production. So, if you see here, which are the ones here in the equation? One term is here, one term is here, then here, here, then here, from the rotor side this one, this; these are the terms.

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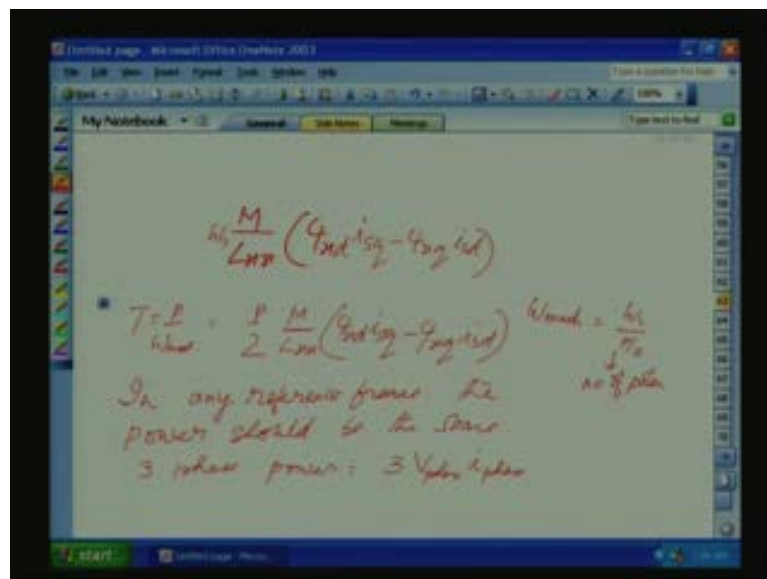
So, let us take out the power;  $P$  is equal to we can write minus  $\omega_s$  into  $L_{ss}$ . So, this into  $i_{qs}$ , this the voltage at the  $d$  axis, then there is another voltage time minus  $M \omega_s$  into  $i_{qr}$  that is minus  $\omega_s$   $M$  into  $i_{qr}$ . So, this is the voltage term occurring at  $d$  and the current at the  $d$  is  $i_{ds}$ . So, we have to multiply this one with  $i_{ds}$  to get the power at

the d axis. Then the q axis stator, again, this will be equal to  $\omega_s L_{ss} i_{ds}$  that is this voltage term. There is another voltage time here, plus  $\omega_s M$  and the current is  $i_{dr}$ , this is the voltage term, so multiply it by  $i_{qs}$ ; this is the power at the stator.

Now, let us take the rotor, rotor  $d_r$  that is minus of  $\omega_s$  minus  $\omega_r$  into  $M$  into  $i_{qs}$ . Again, there is minus by  $\omega_s$ , so that we can club together plus this term,  $L_{rr}$  into  $i_{qr}$ ; the whole thing is multiplied by - now this current is in the d axis - by  $i_{dr}$ . Then again, the q axis plus  $\omega_s$  minus  $\omega_r$  into  $M$  into  $i_{ds}$  that is this current  $M$  into  $i_{ds}$ , then  $\omega_s$  minus  $\omega_r$  plus  $L_{rr}$  into  $i_{dr}$ , multiply  $i_{qr}$ ; this is the total power. But we know that see this  $i_{qr}$  and  $i_{dr}$ , rotor current is very difficult to measure. So, we have to replace  $i_{qr}$   $i_{dr}$  in terms of rotor flux but rotor flux information we want. But from the previous equation we know that  $\psi_{rd}$  is equal to  $M$  into  $i_{sd}$  plus  $L_{rr} i_{rd}$ . So, from this one; what is  $i_{rd}$ ?

We can find out what is  $i_{rd}$ . We can find out  $i_{rd}$  here in terms of  $i_{sd}$  and the rotor flux. Similar way,  $\psi_{rq}$  is equal to  $M$  into  $i_{sq}$  plus  $L_{rr} i_{rd}$ . So, from here,  $i_{rd}$  we can select based on this one,  $\psi_{rd}$  and  $\psi_{rq}$  because we want the rotor flux information.

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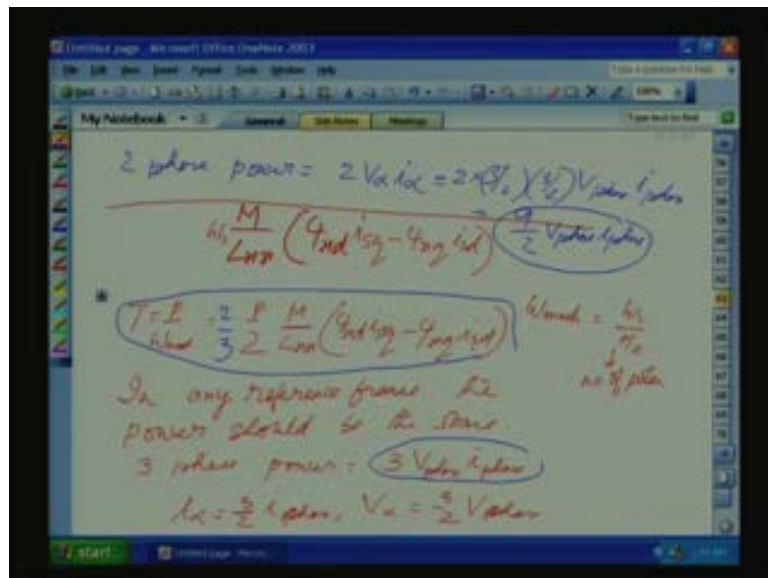
Final power equation will be  $M$  by  $L_{rr}$  into  $\psi_{rd} i_{sq}$  minus  $i_{rq} i_{sd}$ ; this way final equation will come. But if you see here, this has to be and multiplied by  $\omega_s$ ,  $\omega_s$  will come. Now, for the torque, we have to divide by the mechanical speed.  $\omega_{mech}$  is equal to  $\omega_s$  divide by  $P$  by 2. So,  $T$  is equal to  $p$  by  $\omega_{mech}$ ,  $p$  is the number of poles; so  $p$  by 2 will be equal to  $p$  by 2  $M$  by  $L_{rr}$  into  $\psi_{rd} i_{sq}$  minus  $\psi_{rq} i_{sd}$ . It will get in this form, torque; so when we divide by the  $\omega_{mech}$ ,  $p$  is the number of poles number of poles.

Now, let us see, we have transferred everything from the three phase to two phase. So, any transformation, the power balance should be met. That means in any reference frame, the power balance should be equal, the power should be equal. In any reference frame, the power should be the same that is the power balance should be met; the power

should be the same. Let us say whether alpha beta transformation and find it to dq; whether the power balance is met.

Now, for a three phase power based on single phase equivalent quantity is equal to 3 into, for RBC system, 3 into V phase into i phase. Suppose that the same voltage waveform, we are sending it to let us say to a resistive load to make it simple. So, this transformation, the voltage and current transformation, it is not independent of the load. So, let us take a resistive load. So, three phase into i phase; three times for three phase power.

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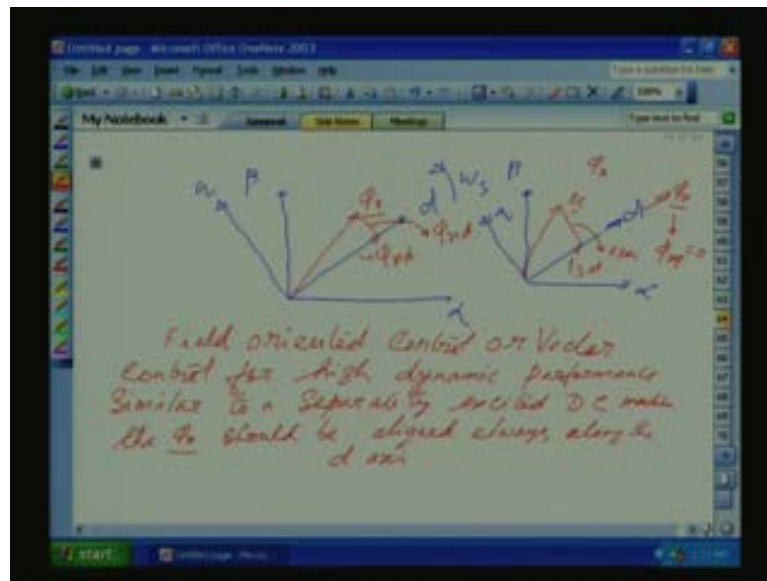


Now, in our transformation we have found out that  $i_{\alpha}$  is equal to  $\frac{3}{2} i_{\alpha\beta}$ ,  $V_{\alpha}$  phase or  $V_{\alpha\beta}$  is equal to  $\frac{2}{3} V_{\alpha\beta}$ ,  $V_{\beta}$  phase, here also we will say  $i_{\beta}$  phase. Now, alpha beta means two phase power. So, two phase power will be, the two phase power is equal to 2 into  $V_{\alpha}$  into  $i_{\alpha}$ , same resistive load we are trying to find out the power in the alpha beta reference frame. This will be equal to 2 into  $\frac{3}{2} i_{\alpha\beta}$  into  $\frac{2}{3} V_{\alpha\beta}$ ;  $\frac{3}{2}$  by 2 into 3 by 2 into  $V_{\alpha\beta}$  into  $i_{\alpha\beta}$  equal to 9 by 2 into  $V_{\alpha\beta}$  into  $i_{\alpha\beta}$ .

So, the power balance; for the three phase, it is this one and for the two phase, it is this one. So to meet, see here the transformation we have taken, we have not taken into consideration the power balance, you simply assume the number of turns are same for the alpha beta and transfer the voltage and current. Now, to make the power balance in our or to make it 3  $V_{\alpha\beta}$  into  $i_{\alpha\beta}$  in the two phase quantity, we have to multiply by 2 by 3. So correspondingly, torque also we have to multiplied by 2 by 3. So here, in our transformation, this is the final - 2 by 3, p by 2 is the number of M by  $L_{rr}$ , this is the torque developed in the system in terms of rotor flux and the stator currents. See, we got the transformation equation dynamic condition under dq reference frame.



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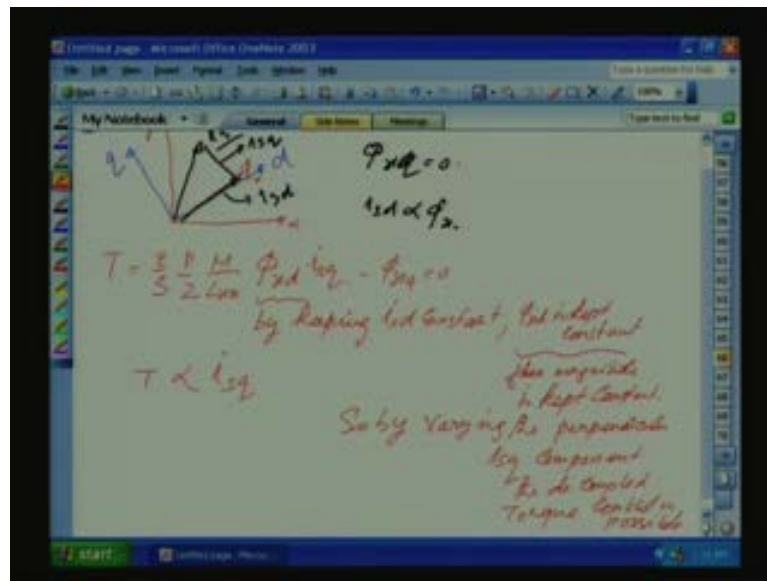
Now, what we want? This is the alpha beta and this is our d and q, dq is rotating, synchronous reference frame we made it. Now, we want to, suppose our  $i_s$  rotor flux is here, somewhere here; this is our  $\psi_r$  flux space phasor that is  $\psi_r$  is equal to  $\psi_{rd}$  plus  $\psi_{rq}$  plus  $j \psi_{rq}$ . So, which is  $\psi_{rd}$ ?  $\psi_r$ , you project the this one to this one, this is  $\psi_{rd}$  and this will be equal to  $\psi_{rq}$ ; this our orthogonal component.

Now, for field oriented control, field oriented control or vector control for high dynamic applications, performance similar to a separately excited DC machine, DC machine; what we want? The  $\psi_r$  flux space phasor should be aligned always along the d axis. So, what is meant by that one? See, if you see here, see we will just rewrite this one here, that means in our new reference frame alpha beta; this is our d, perpendicular to that one we have the q and our  $i_s$ , this is a synchronous,  $\psi_r$  should be always along this one.

So, what is meant by this one?  $\psi_r$  along this one means in the new reference frame and if it is  $i_s$  here, this is our  $i_s$ , this is our new  $i_{sd}$  and this is the  $i_{sq}$ ; in this  $\psi_r$ , the  $\psi_{rq}$  is equal to zero. That means the new reference frame  $\psi_r$  magnitude is equal to  $\psi_{rd}$ . So, we have to beat this condition that means we should know the instantaneous position of the  $\psi_r$  and we have to align the  $\psi_r$  along our rotating, synchronous rotating dq axis.

Now, in this case, let us see what is our equivalent circuit? So, let us go to a new reference frame and find out what happens in the new reference frame. So, we will draw this one here, our alpha beta; alpha, this is beta.

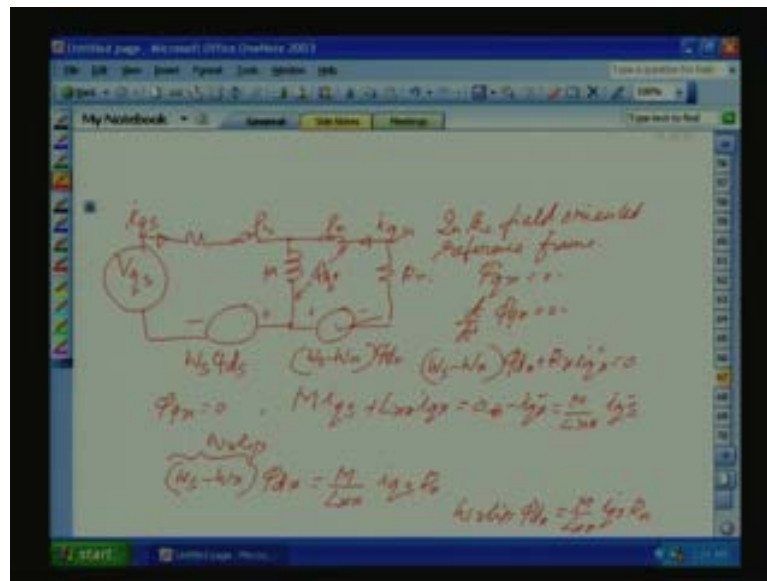
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Now, our d axis, this is our d axis, this is our q axis and  $i_s$  is also along this one,  $\phi_r$ . Now, we have to resolve the current space vector, the current space vector is here. This is our  $i_s$ , will be splitting along d as well as q, this is  $i_{sd}$  and this is  $i_{sq}$ . So,  $i_{sd}$  component will be proportional to the responsible for the flux  $\phi_r$ . Now, in the new one also, here in the new reference frame;  $\phi_{rd} \phi_{rq}$  is equal to zero. So, let us go to our torque equation, original torque equation; torque equation when  $\phi_{rq}$  is equal to 0 is  $\frac{2}{3} \frac{P}{M} P_{rd} i_{sq} - P_{rq} i_{sd} = 0$ . So, let us go to our torque equation, original torque equation; torque equation when  $\phi_{rq}$  is equal to 0 is  $\frac{2}{3} \frac{P}{M} P_{rd} i_{sq} - P_{rq} i_{sd} = 0$ . Final equation will be  $\phi_{rd} i_{sq}$  because  $\phi_{rq}$  is equal to 0.

So, in this equation by keeping  $i_{sd}$  constant,  $\phi_{rd}$  is kept constant. So, flux is flux magnitude is kept constant. So, this shows torque will be proportional to  $i_{sq}$ . So, by varying the orthogonal component, perpendicular  $i_{sq}$  component, the decoupled torque control is possible, torque control is possible. Now we say,  $\phi_{rq}$  is equal to 0. Let us go back to our, now how the equivalent circuit will work? Let us go to our equivalent circuit. Let us go to the next page. So, our equivalent circuit is like this.

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Let us take the q axis,  $V_{qs}$ , this is minus plus omega s si ds, then leakage inductance  $R_r$ , this is our  $i_{qr}$ , this is our  $i_{qs}$ , this is omega s minus omega r into si dr. Now, si qr is equal to zero. In the field oriented reference frame, si qr is equal to zero. Which si qr? si qr is the one due to these two fluxes; this is  $M l_r l_s$ . What it shows? That means d by dt of si qr also zero. So, the voltage coming across the resistance  $R_r$  is equal to the rotational voltage, this one. So, if you write down the voltage loop equation here, let omega s minus omega r into phi dr plus  $R_r i_{qr}$  is equal to zero. That means rotor circuit equation if you take it, your d by dt psi r is equal to zero that means this rotational voltage will be dropped, should be dropped across the resistance  $R_r$ ; so from this one,  $i_{qr}$ .

Now, si qr is equal to zero that is what is si qr?  $M$  into  $i_{qs}$  plus  $L_{rr} i_{qr}$  is equal to zero. From here, from this one, minus  $i_{qr}$  is equal to  $M$  by  $L_{rr}$  into  $i_{qs}$ . So, we got  $i_{qr}$  in terms of  $i_{qs}$ . What is omega s minus omega r? Omega s minus omega r is the slip. So, omega s minus omega r into phi dr is equal to from this equation that is from this equation is substituting  $i_{qs}$  that means  $M$  by  $L_{rr} i_{qs} R_r$ . What is this one? This is slip, this one is the omega slip.

So finally, what we get? Omega slip into phi dr is equal to  $M$  by  $L_{rr}$  into  $i_{qs}$  into  $R_r$ . So, si dr is constant, psi dr is constant; so, that means omega slip is proportional to  $i_{qs}$ , the orthogonal component. Here, omega slip into phi dr is equal to  $M$  by  $L_{rr}$  into  $i_{qs}$  into  $R_r$ . That shows phi dr keeping constant; by keeping the isd component, phi dr is keeping constant, then omega slip is also proportional to  $i_{qs}$ .

Omega slip is proportional to  $i_{qs}$ ; previously we have shown under field oriented control or field oriented equivalent circuit, the torque is proportional to  $i_{qs}$ . That means the torque is slip is proportional to the torque, slip is proportional to the torque by keeping phi dr constant. Then by varying the orthogonal component, we can vary the slip and in turn we can control the torque. So, we will continue this analysis field orient control in the next class.