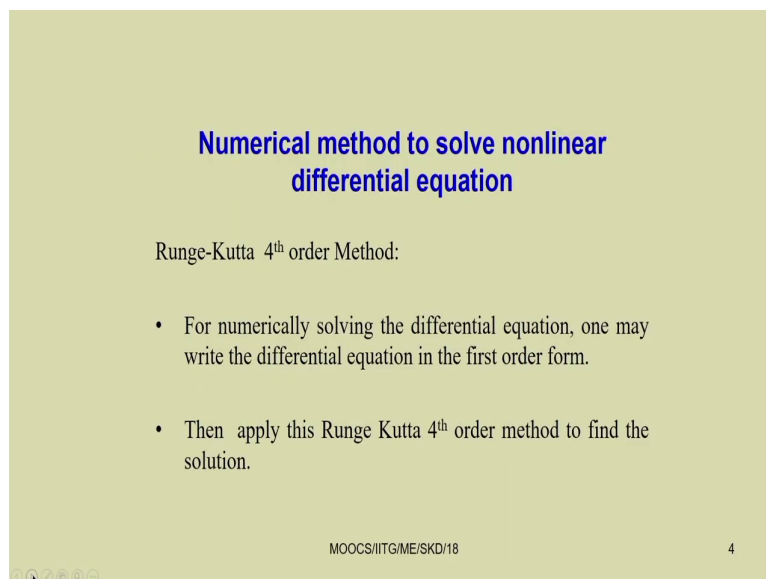


**Nonlinear Vibration**  
**Prof. Santosha Kumar Dwivedy**  
**Department of Mechanical Engineering**  
**Indian Institute of Technology, Guwahati**

**Lecture - 18**  
**Bifurcation Analysis of Fixed-Point Response**

Welcome to today class of Non-linear Vibration. Last class we have discussed regarding the stability and bifurcation of the non-linear systems two different type of bifurcations we have studied or we have discussed. So, one is static bifurcation and other one is dynamic bifurcation. So, today class we will deliberate more on the static and dynamic bifurcations along with stability analysis.

(Refer Slide Time: 00:57)



**Numerical method to solve nonlinear differential equation**

Runge-Kutta 4<sup>th</sup> order Method:

- For numerically solving the differential equation, one may write the differential equation in the first order form.
- Then apply this Runge Kutta 4<sup>th</sup> order method to find the solution.

MOOCS/IITG/ME/SKD/18 4

And we have taken the example of these duffing equations and also to study whether a system is stable or not, we should also know the numerical methods to solve the differential

equations. Already we have discussed this thing many times in this course. So, for example, so you have to use this Runge-Kutta 4th order method.

Either you can use the codes available in different software packages, like in MATLAB, you can use this ode four five if you have stiff equation then you can ode 2 3 or other software's also you can use for different types of non-linear equation solvers.

(Refer Slide Time: 01:45)

For an initial value problem

$$\frac{dy}{dx} = f(x, y), y(a) = y_0, x \in [a, b]$$

The (k+1)th Solution is related to the kth solution which is derived by using Taylor's series

$$y_{k+1} = y_k + (k_1 + 2k_2 + 2k_3 + k_4) / 6$$

$$k_1 = hf(x_k, y_k)$$

$$k_2 = hf(x_k + h/2, y_k + k_1/2)$$

$$k_3 = hf(x_k + h/2, y_k + k_2/2)$$

$$k_4 = hf(x_k + h, y_k + k_3)$$

MOOCS/IITG/ME/SKD/18 5

In case of you are using this Runge-Kutta method you can write your own code also. So, where you can use in this 4th order Runge-Kutta method. So, you can write these solution in this form  $y_{k+1} = y_k + (k_1 + 2k_2 + 2k_3 + k_4) / 6$ , where  $k_1 = hf(x_k, y_k)$ ,  $k_2 = hf(x_k + h/2, y_k + k_1/2)$ ,  $k_3 = hf(x_k + h/2, y_k + k_2/2)$  and  $k_4 = hf(x_k + h, y_k + k_3)$ , where h is the time interval.

So, if you take this time interval very small your accuracy of the solution will be more or it will be more accurate solution you can get. So, after choosing these  $h$  and the initial condition. For example, so you can start with a initial condition taking these initial condition  $y_k$  you can find the next  $y_{k+1}$  what is the response after the time interval  $h$ . So, in that way you can write down this code of your own and you can solve this equation.

(Refer Slide Time: 03:11)

• Example

$$\ddot{x} + x = 0 \quad \checkmark$$

$$y(1) = x; \quad dy(1) = \dot{x}$$

$$y(2) = \dot{x}; \quad dy(2) = \ddot{x}$$

```
function dy = tfl(t,y)
w=10;
dy = zeros(2,1);    % a column vector
dy(1) = y(2);
dy(2) = -w^2*y(1);
```

Handwritten notes:

$$\ddot{x} + \omega_n^2 x = 0$$

$$x = A \sin(\omega_n t + \phi)$$

$$x = A \sin \omega_n t + B \cos \omega_n t$$

$$a_0 = B$$

$$\dot{x} = A \omega_n \cos \omega_n t + a_0 \omega_n \sin \omega_n t$$

$$0 = A \omega_n \rightarrow A = 0$$

$$x = B \cos \omega_n t = a_0 \cos \omega_n t$$

MOOCS/IITG/ME/SKD/18

6

Previously also we have taken these perturbation methods. So, by using the perturbation methods you can get the reduced equations. Those reduced equations also you can use this Runge-Kutta method because these those reduced equations are first order equation.

So, for steady state as they will not be function of time directly you can get a set of algebraic or transcendental equations which you can solve. Otherwise you can use this Runge-Kutta method to solve this first order differential equations to find the solution.

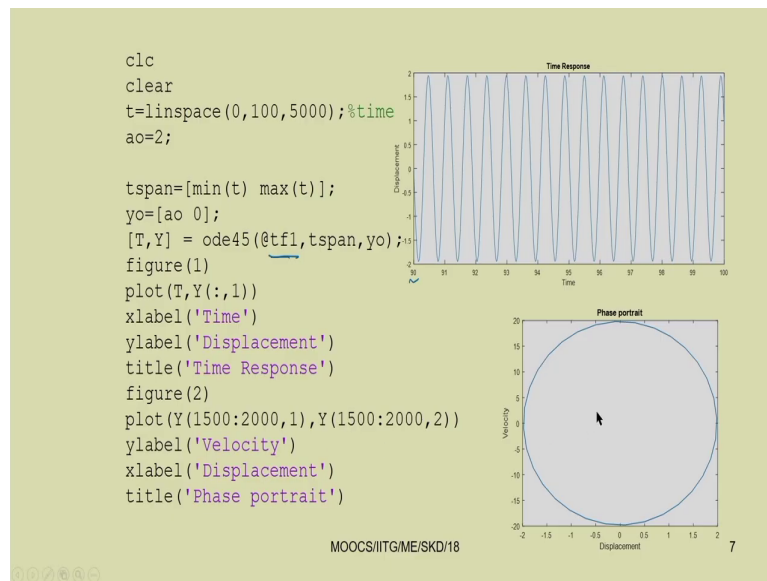
If you have a secondary differential equation for example,  $x'' + x = 0$ . So, in that case you know the closed form solution of this thing which can be written as  $A \sin t$  here  $\omega^2 = 1$ . So,  $\omega^2 = 1$ , so this equation can be written in this form  $x'' + \omega^2 x = 0$ .

So, this is the equation of a spring mass system where  $\omega = \sqrt{k/m}$  or  $\omega^2 = k/m$ , but its solution already you know it is equal to  $x = A \sin(\omega t + \phi)$ . So,  $A \sin(\omega t + \phi)$ , here  $A$  and  $\phi$  depends on the initial condition. So, you can take the initial displacement and initial velocity as initial conditions and you can find  $x$ .

So, here to write down the code in MATLAB. So, you have to initially you just assume let your  $y_1 = x$  and  $dy_1 = x'$ . Similarly  $y_2$  will be equal to  $x'$ . So,  $dy_2 = x''$ , but your  $x''$  is nothing but in this case equal to  $-x$ . So, you can write your equation in this form that is  $dy_1$  in the function file you can write. So, here the code is written below.

So, you can see the code. So, in the function file it is written for example, so you have taken two equations. So, initially you just initialize with 0. So,  $dy = \text{zeros}(2, 1)$ . So, this is two row and one column. So, your  $dy_1 = y_2$  and  $dy_2 = -\omega^2 y_1$ . So, this is the function file.

(Refer Slide Time: 05:52)



And in the main file you can call the function to find. So, this is the main file. So, here you have to decide or you just declare the time space  $t$  equal to line space 0 to 100. So, if you have to do it up to 100 with 5000 divisions it has been taken initial  $a_0$  equal to taken 2. So,  $tspan$  minimum time and maximum time you can specify. So,  $y_0$  initial conditions for example,  $y_0$  equal to  $a_0$  0; that means, initial displacement equal to  $a_0$  and initial velocity equal to 0.

So, you can take different things also. For example, if the system is subjected to some impulse type of forcing then the displacement you can take 0, but the velocity will be equal to  $f \Delta t$  by  $m$ , you can find the initial velocity and you can put it. So, depending on the application, so you have to choose these initial condition here by taking these initial condition  $y_0$  equal to  $a_0$  0 you can take. So, you can write this ode  $T Y$  equal to ode 4 5 at the rate  $tf1$ .

So, you just see this tfl is the function filename. So, tfl tspan y0 you can write. So, there are some other options also available. So, we can check this is the simplest one you can put, you can write in for example, in figure 1 let you plot the time response in figure 2 let you plot the phase portrait in figure 1. So, plot T Y colon 1, so that means, in Y.

So, you are storing the first column you are storing this Y and in second column you are storing this Y dot. That means, you are storing this x and x dot that is displacement and velocity in these two column. The first column of Y you will store the displacement the second column you storing the velocity. So, when we are plotting this phase portrait that time you can plot Y1 comma Y2. So, you can see here then this ylabel. So, you can put plot T comma Y colon 1.

So, that means, give you the first column. So, all the first column that is displacement. So, this plot you can see displacement versus time. So, already you are familiar with the solution y equal to Y 0 sin omega t, here by putting these t equal to 0 displacement equal to 2. So, it will start from.

So, you have to put that equation. So, a0 equal to A sin omega t. So, two way you can write this you just see the closed form solution either you can write it in this way or you can write x equal to A sin omega n t.

So, if you want to compare your result with respect to the analytical solution this way you can do also. So, B cos omega n t, so at t equal to 0. So, we have taken x equal to a 0, so a 0 equal to, so a 0 equal to B now you can put x dot. So, x dot equal to A omega n A omega n cos omega n t plus for B it can be a 0 a 0. So, for cos differentiation equal to a 0 omega n sin omega n t. So, at t equal to 0. So, as it is equal to 0 you are taking. So, 0 will be equal to A omega n.

So, A omega n equal to 0. So, as omega n is not 0 so A equal to 0. So, the solution becomes x equal to B cos omega n t B cos omega n t where B equal to a 0. So, this becomes a 0 cos

$\omega n t$  the solution becomes a  $0 \cos \omega n t$ . So, you can compare this thing with the solution what you have obtained by using this Runge-Kutta method.

Here you just see it has been plotted from 90 that is why you have not seen at  $t$  equal to 0. So, what is the values by changing this axis property. So, it has been said from 90 to 100 to the response to be periodic. So, here also the phase portrait is not plotted for the whole range 0 to 100. So, it has been plotted from only 90 to 100.

So, you can choose. So, for example, here you just see the plot command. So, plot Y 1500 to 2000. So, you have taken only the data available from 1500 to 2000 column 1 comma Y 1500 to 2000 column 2 that is this is displacement versus this velocity we are plotting. So, you can label these xlevel as ylevel as velocity xlevel as displacement then title phase portrait. So, this is the phase portrait we have seen.

(Refer Slide Time: 11:16)

```

function dy = tf1(t,y)
w=10;
dy = zeros(2,1); % a column vector
dy(1) = y(2); ✓
dy(2) = -w^2*y(1);

```

*Duffing eq<sup>n</sup>*

$$\ddot{x} + \omega_n^2 x + \alpha x^3 = f \cos \omega t$$

$$\ddot{x} = f \cos \omega t - \omega_n^2 x - \alpha x^3 - 2\mu \dot{x}$$

$$= f \cos \omega t - \omega_n^2 y(1) - \alpha y(1)^3 - 2\mu y(2)$$

MOOCS/IITG/ME/SKD/18 8

So, now, as an assignment, so you can check by using this way. So, you can check the duffing equation also. So, in this duffing equation if you want to find the response. So, in that case only these function has to change. Here the first one will remain same also your duffing equation let you right the duffing equation in this form that is  $x \ddot{x} + \omega_n^2 x + \alpha x^3 + 2\zeta \text{ or } 2\mu \dot{x}$  you can put  $2\mu \dot{x}$  will be equal to  $f \sin \omega t$  or  $f \cos \omega t$  let us put, you can put  $f \sin$  or  $f \cos \omega t$ .

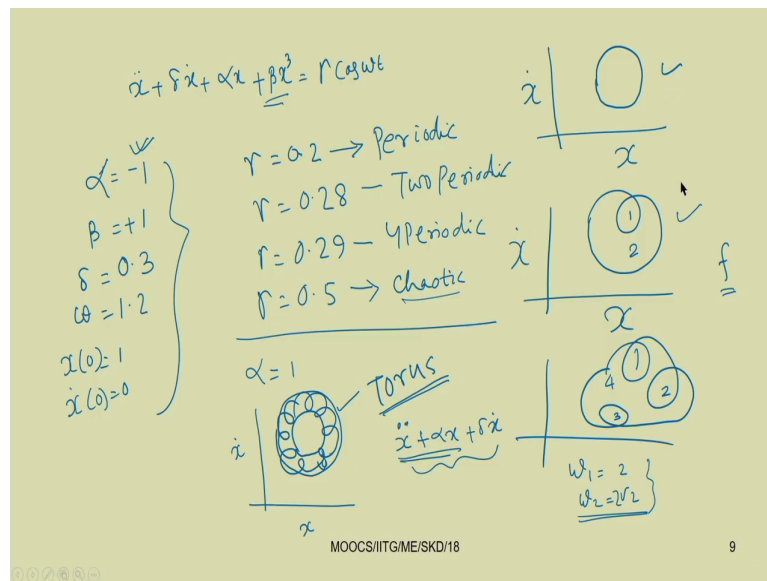
So, in this case, so your first equation will remain same, second equation is nothing but. So, this part will be replaced by  $x \ddot{x}$ . So,  $x \ddot{x}$  in this case equal to  $x \ddot{x}$  equal to  $f \cos \omega t - \omega_n^2 x - \alpha x^3 - 2\mu \dot{x}$  here. So, you have to substitute this is equal to  $f \cos \omega t - \omega_n^2 x$ .

So, for  $x$ , so  $x$  equal to your  $y_1$ , so  $1 - \alpha x^3$ . So, this becomes  $y_1$  whole cube you just see  $y_1$  whole cube you can put, whole cube. So, minus  $2\mu$  for  $x \dot{x}$ . So, it can be so it is equal to  $y_2$ . So, this way you can write your function 2. So, this function 2 can be written  $y_2$  can be replaced by this one and you can use this same ode 4 5 function to find the different solution for a duffing equation.

So, different solution for duffing equation. So, you can verify for different value of different coefficients the response may be periodic, sometimes it will be periodic.



(Refer Slide Time: 13:39)



So, in case of the periodic if you plot the displacement versus  $x$  versus  $\dot{x}$ . So, in case of periodic, so you can see the phase portrait will be. So, the phase portrait will be a closed solution. So, in case of for some other value of the system parameter. So, you can see the phase portrait maybe may contain two loops.

So, for some other value if you go on changing your system parameter for example, if you go on changing this value of forcing  $f$ . So, amplitude of forcing parameter if you go on changing. So, you can see it will go on. So, this is periodic, this is two periodic then you can have 4 periodic. So, in case of 4 periodic, so there will be 4 loops. So, here you just see this is loop 1, this is loop 2.

Similarly, you can have 4 loops. So, for example, this is one, this is the second one, another one and this one. So, you can have 4 loops. So, this is 1 loop, this is the 2nd loop, this is the

3rd loop and the whole thing is itself is a loop, so that is 4 loops. So, by changing the system parameter if you write the equation particularly. So, if you write this equation in this form.

For example let me write and you can verify this thing. So, the equation if it is written  $x'' + \delta x' + \alpha x + \beta x^3 = \gamma \cos \omega t$ . So, if you take the value for example, take the value of  $\alpha$  equal to minus 1, then  $\beta$  equal to plus 1,  $\delta$  equal to damping  $\delta$  equal to let you take equal to 0.3.

So, damping equal to 0.3, then  $\omega$  let us take  $\omega$  equal to 1.2 and initial condition, let me take  $x(0)$  equal to 1 and  $x'(0)$  equal to 0, displacement equal to 1 and velocity equal to 0. So, if you take these parameters. So, for you can see for  $\gamma$  equal to 0;  $\gamma$  equal to 0 you can see the response or  $\gamma$  equal to 0.2,  $\gamma$  equal to 0 is the free vibration response.

So,  $\gamma$  equal to 0.2, if you put then you can check that the response is periodic, the response is periodic like these things, so you can get a response. So, if you take this  $\gamma$  equal to 0.28 for example, 0.28. So, you can find this is two periodic. Similarly if you take  $\gamma$  equal to for example, you just take  $\gamma$  equal to 0.29;  $\gamma$  equal to 0.29, so it is 4 periodic.

And if you take higher value of  $\gamma$  for example, you just take  $\gamma$  equal to 0.5. So, you verify this thing  $\gamma$  equal to 0.5, so the response will be chaotic.

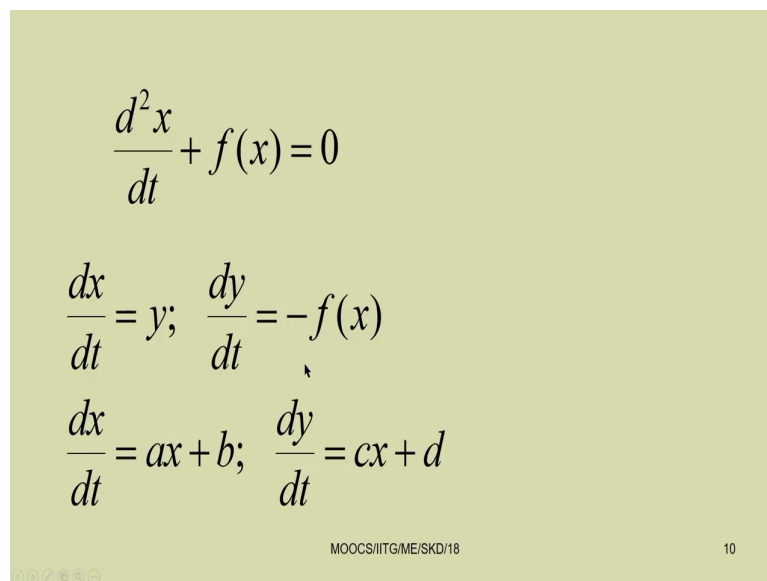
Chaotic means, it contains many harmonic terms more than 16 times or more than around 30 harmonic terms it will contain, so the response is chaotic. So, the chaotic response are deterministic response, but it will contain many harmonics and you cannot distinguish from the time response and from the phase portrait.

So, we can easily check that the response to be chaotic. This chaotic response, in case of chaotic response it depends on the initial condition by changing these initial condition so you can check that. So, you can get different type of attractors, in one case for example, by taking

1 0 you will get one type of attractor. By changing that initial condition you can verify that you are getting different other attractor the attractor will not be same.

So, you can verify these thing another conditions also you can take and check. So, if alpha equal to 1.

(Refer Slide Time: 18:23)


$$\frac{d^2x}{dt^2} + f(x) = 0$$
$$\frac{dx}{dt} = y; \quad \frac{dy}{dt} = -f(x)$$
$$\frac{dx}{dt} = ax + b; \quad \frac{dy}{dt} = cx + d$$

MOOCs/IITG/ME/SKD/18 10

In this case in this particular case you just see alpha you have taken to be minus 1. So, in this case you have taken alpha equal to minus 1, particularly if you see this equation  $x$  double dot minus alpha  $x$ . So, you just see the system is unstable, so in case of a linear system. So,  $x$  double dot minus alpha  $x$  alpha is positive or you just take this plus and now alpha is negative.

So, if  $\alpha$  is negative plus  $\delta \dot{x}$  in linear case actually the system to be in the linear case the system is unstable, but by adding these by adding these cubic non-linearity and applying some force. So, you can see it yields two different type of other different type of responses. We now understand that in addition to fixed point response.

So, there are other type of responses also available in our system. So, the they are periodic response. These periodic may be single frequency it may be multi frequency. So, in case of single frequency this is single period you got. So, in case of 2 frequency, so you can get this type of 2 lobes in case of 4 frequency 4 lobes. So, in all these cases if you check carefully. So, the frequency ratio are in the form of integer numbers.

So, this let it is  $\omega_2$  and  $\omega_1$ . So,  $\omega_2$  by  $\omega_1$  must be in the form of integer, but if they are irrational number, so let us check take some irrational number. For example, 1 frequency  $\omega_1$  equal to 2 and other frequency  $\omega_2$  equal to  $\sqrt{2}$   $\sqrt{2}$  times 2,  $2\sqrt{2}$ . So, in that case you can verify; you can verify that the phase portrait will no longer be similar to these, what it will be similar to a torus. So, it will be similar to a torus. So, what is a torus? So, you can check in case of a torus.

So, the you have two circles which are connected by so connected by this. So, this way they will be connected, so this is torus. So, we will study more regarding this torus when we will discuss regarding the quasi periodic response. So, now let us again come back.

So, these are the different type of response you can get. So, given a differential equations. So, now, you can use this ode 4, 5 from the MATLAB to get different type of response. So, these response you can try and you can find.

(Refer Slide Time: 21:26)

$$x(t) = A \exp(\lambda t); \quad y(t) = B \exp(\lambda t)$$
$$\begin{vmatrix} a - \lambda & b \\ c & d - \lambda \end{vmatrix} = 0 \quad \lambda^2 - \text{tr} \lambda + \text{det} = 0$$
$$\lambda = \frac{\text{tr}}{2} \pm \sqrt{\left(\frac{\text{tr}}{2}\right)^2 - \text{det}}$$
$$\text{tr} = a + d; \text{det} = ad - bc$$

MOOCs/IITG/ME/SKD/18 11

So, let us come back to. So, again so let us briefly again check that, if we have a equation. So, we can study the stability of that equation by studying or by finding the trace and determinant also. So, this part already we have discussed.

(Refer Slide Time: 21:44)

- **Hyperbolic fixed point:** when all of the eigenvalues of  $A$  have nonzero real parts it is known as hyperbolic fixed point.
- **Sink:** If all of the eigenvalues of  $A$  have negative real part. The sink may be of stable focus if it has nonzero imaginary parts and it is of stable node if it contains only real eigenvalues which are negative.  $Im = 0$
- **Source:** If one or more eigenvalues of  $A$  have positive real part. Here, the system is unstable and it may be of unstable focus or unstable node. ✓
- **Saddle point:** when some of the eigenvalues have positive real parts while the rest of the eigenvalues have negative.
- **Marginally stable:** If some of the eigenvalues have negative real parts while the rest of the eigenvalues have zero real parts

MOOCS/IITG/ME/SKD/18 12

So, now let us see few definitions. So, one is this hyperbolic fixed point. So, we know now. So, given an equation for example, let we have a equation  $\dot{x}$  equal to  $f(x)$ . So, this is the given equation and we want to study the stability of this equation. So, in that case, so we know the equilibrium point or the fixed point.

So, when the equilibrium point is said to be. So, there are several definitions are there. So, one is hyperbolic fixed point when all the eigenvalues of  $A$ . So, we can find these  $DF(x)$ . So, you can find these  $DF(x)$  these  $DF(x)$  can be written as  $AX$ . So, this a matrix is the Jacobian matrix.

So, when all the eigenvalue of the Jacobian matrix have nonzero real parts, it is called or it is known as hyperbolic fixed point. So, already we have discussed regarding these eigenvalue and we have seen. So, if all the eigenvalues. So, if you plot this is the real part of the

eigenvalues, this is the imaginary part. So, you take all the eigenvalues for different system parameter, if the eigenvalues are in the left hand side of the  $x$  plane.

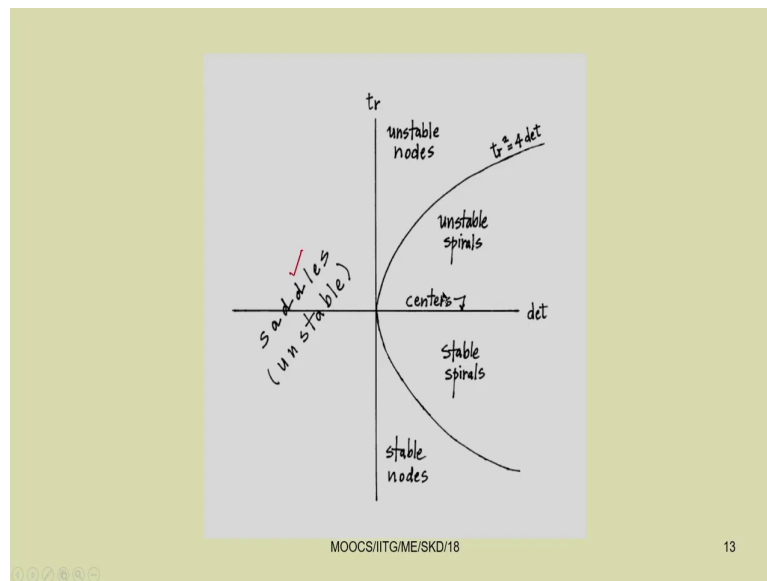
So, if they are on the left hand side of the  $x$  plane then the system is stable, here the hyperbolic fixed points. So, when all the eigenvalues of  $A$  have nonzero real parts. So, it may be in the right hand side or in the left hand side of the  $x$  plane, but if it is nonzero real part then they are known as hyperbolic fixed point.

So, sink if all the eigenvalues of  $A$  have negative real parts if all the eigenvalues of  $A$ . So, they are negative real parts, so then it is known as sink. So, that means so if they have negative real part, that means, the system is stable. So, if the system is stable. So, it is known as sink the sink may be stable focus if it has nonzero imaginary parts and if it is node if it contains only real eigenvalues which are negative. So, out of all these eigenvalue if all the eigenvalues are only. So, it has 0 imaginary parts then we can get ignored.

So, if they are complex conjugate then we will get oscillatory motion. So, that time it will be. So, it may have nonzero imaginary part. So, in that case we will get focused. So, it is known as stable focus and in case of only node so, we will get stable node if it contains. So, if it contain only the real part if the imaginary part is 0.

So, we can have two options either imaginary part is 0. So, if imaginary part is 0 then we will have the stable node, if imaginary part is 0 then we can have stable node. So, this is imaginary part 0.

(Refer Slide Time: 25:18)



So, if imaginary part is there then we can have if imaginary part is there, then we can have stable focus. So, here so it will spiral actually, it will spiral down to get the response. So, already we have plotted those things and we will see it again. So, then source if one or more of the eigenvalues of  $A$  have positive real parts. So, then some of the roots or some of the eigenvalues will be in the right hand side of the  $x$  plane.

So, in that case it is known as source, so we will have source. So, if one or more of the eigenvalue of  $a$  have positive real parts, here the system is unstable and maybe unstable focus or unstable node. So, if it the complex number that is nonzero imaginary part that case we will get focused unstable focus and if it is 0 imaginary part, but it is in the right hand side then it will be unstable node, saddle point.



So, when some of the eigenvalues have positive real part and some other have negative real part. So, that means, so it is in both the side of the x plane. So, then we can tell it is a saddle node saddle point, this is saddle point. So, in case of saddle point equilibrium point can be told to be saddle point, if some of the eigenvalues have positive real parts while the rest of the eigenvalues have negative real parts.

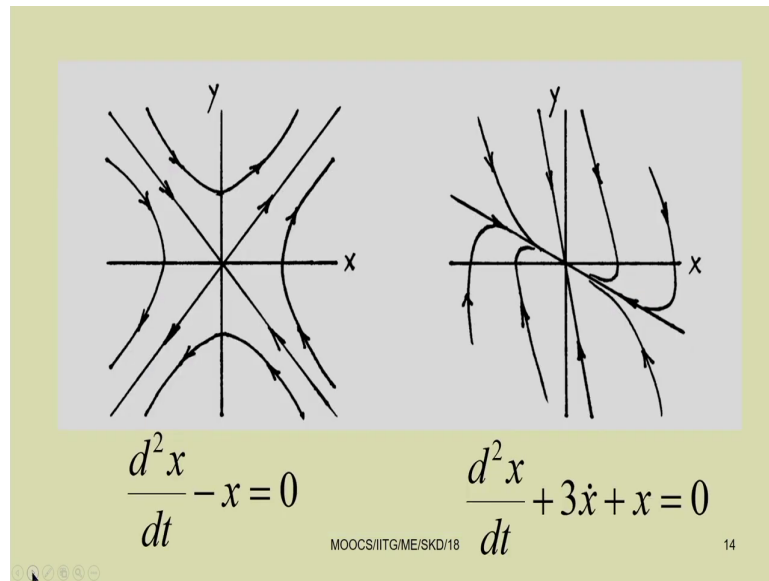
Marginally stable, if some of the eigenvalues have negative real parts, while the rest of the negative eigenvalues have zero real part, it is marginally stable. So, if most of the eigenvalues have negative real part, but some of the eigenvalues have zero real part. So, none of the eigenvalue have real part in the right hand side of the x plane.

So, if some of them are on the right hand side of the x plane then it will be source or the system will be unstable with these things. So, we know when the system will be stable. That means, when the system response will be bounded and unstable when the system response will be unbounded. So, from the trace and determinant also we can get the same thing. So, we know the saddle point, so the saddle point will be here.

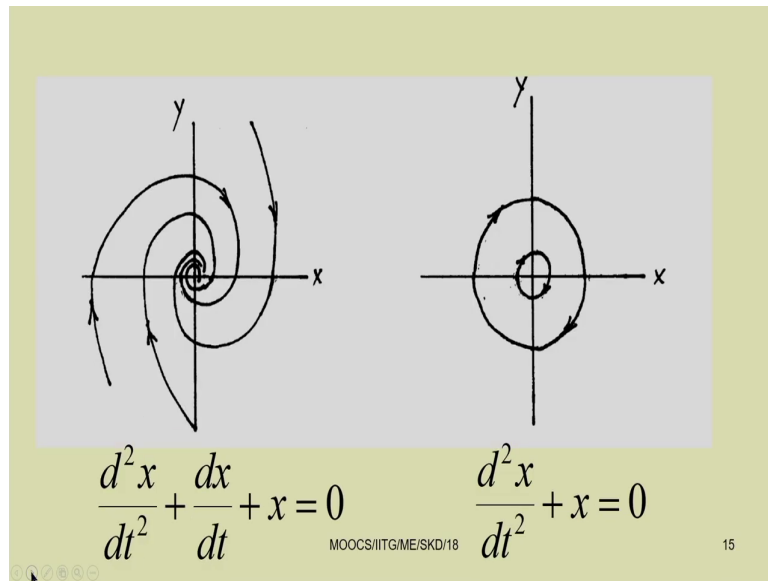
And then so if you plot the determinant versus trace. So, we can see this trace square equal to 4 into determinant, so this curve we can plot. So, here it will be centers on stable spiral stable spiral. So, if it is in this region it will be stable spiral. So, in this region it will be stable nodes above this line.

So, above this line it will be on this line it is center and it is unstable spiral and unstable nodes, nodes is imaginary part equal to 0. So, if the eigenvalue has 0 imaginary part actually you will get that thing.

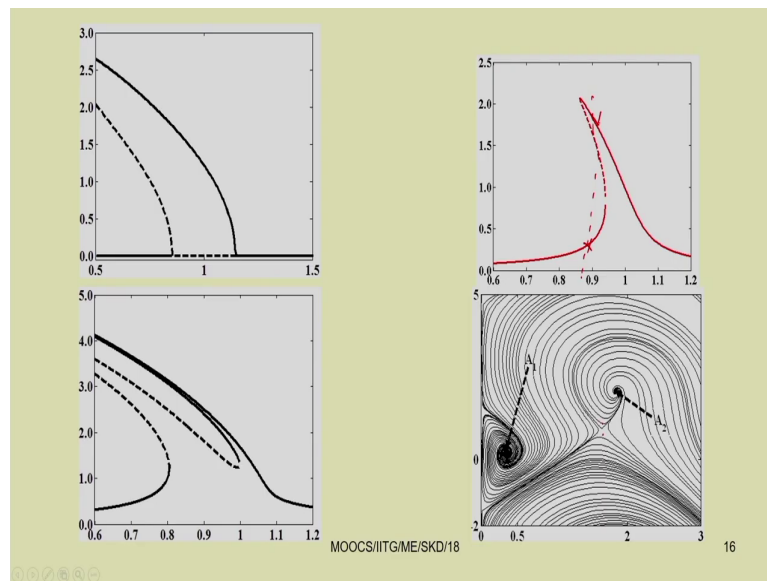
(Refer Slide Time: 28:26)



(Refer Slide Time: 28:28)



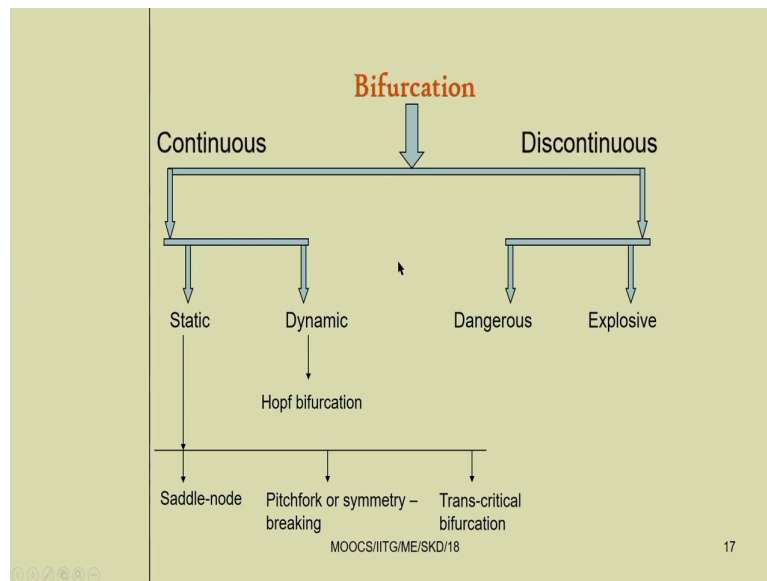
(Refer Slide Time: 28:30).



Already we have plotted this thing and we have seen and these are different examples also we have taken previously and we know regarding the multiple branch in case, multiple equilibrium solutions or multiple equilibrium points in case of the non-linear system. And for these multiple equilibrium points, we must use this basin of attraction method to find for which equilibrium for which initial points. So, one obtain which equilibrium points.

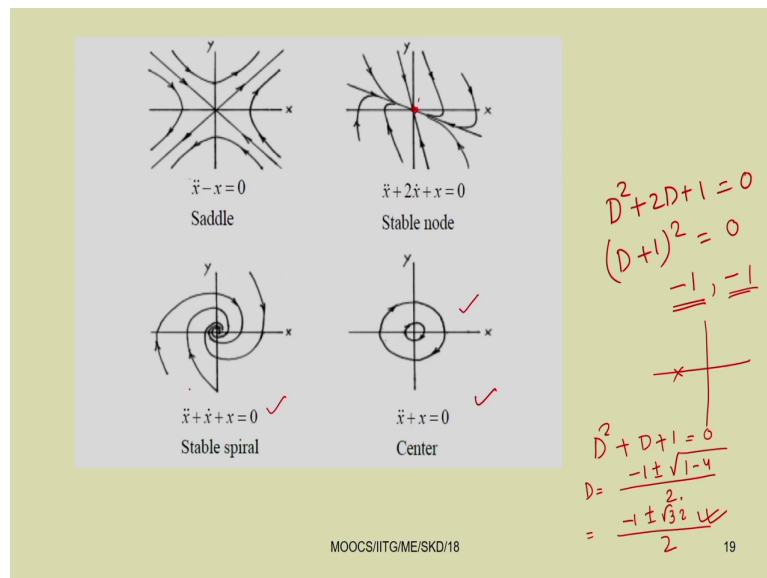
So, for different for example, you can see for all these initial points it is coming to this thing and for all these initial point, so it is coming to  $A_2$ , so  $A_1$   $A_2$ . So, you can have bi stable region here, so if you draw a line here. So, you can get the bi stable region and these in this bi stable region. So, you can find this is one solution bi stable solution. So, bi stable, but three solutions you have. So, out of this thing one is unstable. So, this point is the unstable saddle point.

(Refer Slide Time: 29:38)



So, you can have a saddle point here. Now, let us revise this thing this bifurcation. So, you have continuous bifurcation discontinuous. So, you have static bifurcation dynamic bifurcation. So, in case of static, so you have saddle node bifurcation, pitch fork or symmetry breaking bifurcation and trans critical bifurcation and in case of dynamic. So, you have this hopf bifurcation ok.

(Refer Slide Time: 30:00)



Already we have seen saddle. So, this is the saddle point and this is the saddle  $x$  double dot minus  $x$  equal to 0. So, you just see the roots of the eigenvalue or roots of this equation. So,  $x$  double dot minus  $x$  equal to 0. So,  $x$  double dot will be or this auxiliary equation will be  $D$  square minus 1 equal to 0 or  $D$  square equal to 1. So,  $D$  equal to plus minus 1.

So, the solution will be  $c_1 e$  to the power  $t$  plus  $c_2 e$  to the power minus  $t$ . So, the  $c_1 e$  to the power  $t$  term will exponentially grow the response as  $t$  tends to infinite. So, that is why so the response so you can get. So, one part we will pull it off and the other part  $c_1 c_2 e$  to the power minus  $t$ . So, that will give rise to. So, as  $t$  tends to infinity it tends to 0.

So, these type of response are known as saddle, so this is a saddle point. So, in the saddle you can if you draw these  $x$  versus  $\dot{x}$  versus  $\ddot{x}$ . So, you can see at different region. So, the flow will be like this thing. So, the flow will be, so here the flow will going away.

So, here the flow is this way this direction left side it is in you just see in the left side it is moving in clockwise direction, in right side it is moving in anti clockwise direction and here in the top portion here you just see it is moving in.

So, it is moving in anti clockwise direction and here it is moving in clockwise direction. So, similarly so the stable node you can get  $\ddot{x} + 2\dot{x} + x$ . So, this is similar to that of a this damped. So, this is that of a single degree of freedom system with damping.

So, in case of damping as  $t$  tends to infinite the response tends to 0. So, it tends to, so all the responses you just see all the response to the left hand side is closing to this point and similarly from right hand side also they are closing to the same point.

So, all the in the phase portrait, so all of them are moving to the same point and here. So, this is a stable node point. So, similarly you have a center. So, in this case  $\ddot{x} + x = 0$ . So, the solution becomes  $\ddot{x} - x = 0$  here the auxiliary equation  $d^2 = -1$ . So, as  $D^2 = -1$ , so  $D = \pm i$ .

So, the solution becomes  $a \cos \omega t + b \sin \omega t$ . So, where this  $\omega = 1$  in this case. So, the response is harmonic. So, as the response is harmonic if the displacement is written in terms of for example, in  $\sin$ . So, the velocity will be in  $\cos$  and if you plot this displacement versus velocity, so it will be circle only.

So,  $x^2 + y^2$  will be equal to 1. So, this way so it becomes a circle. So, this is a center in this case this is a center and this is  $a$ . So, in this case you can see that a stable spiral you can get a stable spiral. So, it is spiraling down to, so this is a stable node.

So, stable node means so in this case, so you have in this case you just see the auxiliary equation and you can verify or you just find the roots. So, from the roots you can find that the roots are. So, the roots will be a real root here. So, because you just see. So, your equation becomes. What is the equation?  $D^2 + 2D$ .

So, here the equation is  $D^2 + 2D + 1$ . So, this is the auxiliary equation. So, it should be equal to 0. So, then this is  $(D + 1)^2 = 0$ . So, you have two roots and they are equal roots and the value is minus 1 roots are minus 1 minus 1 and minus 1.

So, these are real roots only real roots and they lie in the left hand side of the  $s$  plane. So, as they are lying in the left hand side of the  $s$  plane, the solution must be stable. So, this is a stable solution you are getting, so it is a node. So, if you have imaginary parts for example, in this case what is the auxiliary equation? Auxiliary equation this is  $D^2 + D + 1$ .

So, this is the thing. So, this should be equal to 0. So, the roots of this equation you can write for example, so  $D$  will be equal to  $\frac{-1 \pm \sqrt{1 - 4}}{2}$ . So, this becomes  $\frac{-1 \pm \sqrt{-3}}{2}$ . So, here the root you just see this becomes  $\frac{-1 \pm \sqrt{3}i}{2}$ .

So, inside this square root we have  $\sqrt{3}i$ . So, it will be  $\frac{-1 \pm \sqrt{3}i}{2}$ . So, it will be  $\frac{-1 \pm \sqrt{3}i}{2}$ . So, we have the imaginary root. So, if we have imaginary root. So, the response will be oscillatory. So, that is why you are getting the spiraling of the solution. So, in this case it will not be spiral. So, it is a stable node, but in this case it will spiral down and finally, it will be at 0.



(Refer Slide Time: 36:00)

**Static Bifurcation**

For a system  $\dot{x} = F(x; \mu)$ , following two conditions to be satisfied at the static bifurcation point.

1.  $F(x_0; \mu_c) = 0$  ✓
2. The Jacobian matrix  $\left( D_x F = \frac{\partial F}{\partial x} \right)$  has a zero eigenvalue while all of its other eigenvalues have non zero real parts at  $(x_0; \mu_c)$ . Hence the point is nonhyperbolic.

$\dot{x} = F(x; \mu)$   
 $0 = F(x; \mu)$   
 $x_0 \quad \mu \rightarrow \mu_c \checkmark$

MOOCs/IITG/ME/SKD/18 20

Finally it will be at 0. Last class we have studied regarding the static bifurcation. So, we can have further discussion on the static and dynamic bifurcation today, given a equation  $x$  dot equal to  $F(x; \mu)$ . So, you just see here we are using semicolon instead of comma as  $\mu$  is a parameter that is why we are using the semicolon here,  $x$  is a variable, but  $\mu$  is a parameter which we are varying or we are changing to get different response, for a given equation  $x$  dot equal to.

So, if we have a equation  $x$  dot equal to  $F(x; \mu)$   $x$  is the variable and  $\mu$  is the parameter. So, for steady state or for equilibrium position or for fixed point position, so this  $x$  dot must be equal to 0. So, we can get all the fixed point response. So, after getting these fixed point response. So, we can study whether the fixed point is stable or unstable or there is some

bifurcation points also to have a bifurcation point late for  $\mu$  equal to  $\mu_c$   $\mu$  critical value let there is a bifurcation point.

So, to find this bifurcation point the first condition must be if  $x_0$  let  $x_0$  is the corresponding value. So,  $F(x_0, \mu_c)$  must be equal to 0. So, this is the first condition and second condition the Jacobian matrix that is  $D_x F$  that is  $\frac{\partial F}{\partial x}$  has a zero eigenvalue while all other eigenvalues have nonzero real parts at  $x_0$  at  $\mu_c$ . So, has a zero, so it must have a zero eigenvalue.

So, the Jacobian matrix  $D_x F = \frac{\partial F}{\partial x}$  has a zero eigenvalue while all of its other eigenvalues have nonzero real parts at  $x_0, \mu_c$ . Hence this point is non hyperbolic equation at bifurcation point for a hyperbolic. So, in case of a hyperbolic fixed point all the real parts of the roots must be must not be 0.

So, it should be nonzero real part of the eigenvalue for hyperbolic fixed point, but if one of these eigenvalue is zero. So, then this becomes non hyperbolic. So, for the static bifurcation these two condition must be satisfied. So,  $F(x_0, \mu_c) = 0$  and this Jacobian matrix must have a zero eigenvalue in case of dynamic bifurcation. So, we can see, so it must have a eigenvalue.

(Refer Slide Time: 39:03)

**Saddle-node Bifurcation:**

The normal form for a generic saddle-node bifurcation of a fixed point is  $\dot{x} = F(x; \mu) = \mu - x^2$

saddle-node bifurcation as the two branches meeting at  $\mu = 0$  have same tangent

$$\left. \begin{aligned} \dot{a} &= -\zeta a - \bar{\omega}_1^2 \left( \frac{1}{8} a_4 a^2 + \frac{1}{2} \alpha_5 \right) \sin \gamma, \\ a \dot{\gamma} &= a \sigma - \frac{3}{8} K a^3 - \bar{\omega}_1^2 \left( \frac{3}{8} \alpha_4 a^2 + \frac{1}{2} \alpha_5 \right) \cos \gamma. \end{aligned} \right\}$$

MOOCSS/ITG/ME/SKD/18 21

So, which will have the imaginary parts also, so already we have discussed regarding the saddle node bifurcation and the in case of saddle node bifurcation the generic form of this thing equal to mu minus x square. And so, by putting these x dot equal to 0. So, we have the fixed point equal to x square equal to root over mu. So, from that thing if you plot this x versus mu, so we have this curve.

So, now if we can find the slope at each point, so you can see the slope at this bifurcation point. So, before mu equal to 0, so all the points mu less than 0. So, root over mu is imaginary. So, it is not real, that is why the solution does not exist solution does not exist before mu equal to 0. So, after mu equal to 0 we have two solutions. So, out of these two solutions the upper branch you can see. So, it is stable because its eigenvalue will be negative and the lower parts is unstable.

So, if you plot the plot the slope at each point. So, you can see at this bifurcation point or at this point they have the same tangent. So, saddle node bifurcation are the two branches meeting at  $\mu$  equal to 0 have the same tangent. So, here also by taking some other examples. So, you can see, so this for, so we have a saddle node bifurcation point here. So, it is not here. So, we have a saddle node bifurcation point here and also one saddle node bifurcation point here.

(Refer Slide Time: 40:46)

$[D_x F \quad F_\mu] = \begin{bmatrix} 0 & 1 \end{bmatrix}$ , So  $F_\mu$  does not belong to range of  $D_x F$ . Rank of this matrix is 1. So the origin is a saddle-node bifurcation point.

$$F_\mu = \frac{\partial F}{\partial \mu}$$

At a saddle-node point  $F_\mu$  does not belong to the range of  $D_x F$  and for pitchfork and transcritical bifurcation point  $F_\mu$  belongs to the range of  $D_x F$ . It may be noted that the range of an  $n \times n$  matrix  $A$  consists of all vectors  $AZ$  where  $Z \in \mathbb{R}^n$ . Hence  $[D_x F \quad F_\mu]$  has a rank of  $n$  at saddle node bifurcation point and rank of  $(n-1)$  at other static bifurcation point.

$[D_x F \quad F_\mu] = \begin{bmatrix} 0 & 1 \end{bmatrix}$

$F(x) = \mu - x^2$   
 $DF(x) = -2x$   
 $F_\mu = 1$

MOOCS/IITG/ME/SKD/18 22

In this case further you can construct a matrix that is  $D \times F$  and  $F_\mu$  matrix. So, where  $F_\mu$  equal to  $\frac{\partial F}{\partial \mu}$  and  $D \times F$  is nothing but the Jacobian matrix and you just construct a matrix with the Jacobian matrix and  $F_\mu$  and in this particular case. So, in this particular case for example, this is  $F$  equal to  $\mu - x^2$   $F_\mu$  equal to 1. So, as our  $F$  equal to  $F$  equal to  $\mu - x^2$ .

So, our  $D_x F$ , so if you differentiate this thing with respect to  $x$   $D_x F = -2x$  and  $F_\mu = 1$  you differentiate this thing with respect to  $\mu$ . So, this becomes 1. So, if I will construct a matrix. So, for the equilibrium position. So, for the equilibrium position  $D_x F = 0$ . So, this part equal to 0 and  $F_\mu = 1$ .

So, we have a matrix now we have construct a matrix that is  $D_x F$  and  $F_\mu$ . So, these matrix equal to 0 and 1 in this particular case. So, here you can see this  $F_\mu$  does not belongs to the range of  $D_x F$ . So, rank of this matrix is one the origin of the saddle node bifurcation point. So, the origin of those this is the. So, the origin is the, so at  $x = 0$ . So, this origin is the is a bifurcation point.

So, here at this point it satisfy both the conditions and at the same times. So, to distinguish the saddle node bifurcation point with other different static bifurcation point you must have to do these test, just find the rank of this matrix. So, this rank you can see in this case. So, the rank of this matrix is 1 this origin is a saddle node bifurcation point. So, we will see in other cases and a saddle node point  $F_\mu$  does not belong to the range of  $F_\mu$ . So, here  $F_\mu = 1$ .

So, this does not belong to the range of  $D_x F$ . So, in case of  $D_x f$ , so you have only 0. And for pitchfork and trans critical bifurcation point  $F_\mu$  belongs to the range of  $D_x F$ . So, we can see later in this example with the example for this pitchfork and trans critical bifurcation.

So, we will construct this matrix and check. So, what is the range of this matrix? So, it may be noted that the range of an  $n \times n$  matrix  $A$  consist of all vectors  $AZ$  where  $Z$  belongs to  $\mathbb{R}^n$ .

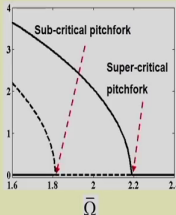
Hence  $D_x F$  has rank of  $n$  at saddle node bifurcation point in this previous case. So, it has a rank of 1 at the saddle node bifurcation point and the rank of  $n - 1$  at other static bifurcation point. So, if you take other static bifurcation point. So, you can find the rank is less than 1. So, that is  $n - 1$ .

(Refer Slide Time: 44:17)

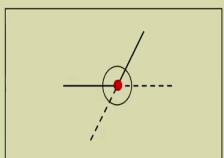
**Pitchfork bifurcation:**  
 The normal form for a generic pitchfork bifurcation of a fixed point is

$$\dot{x} = F(x; \mu) = \mu x - x^3$$

$$\dot{a} = -\zeta a - \frac{\alpha_6}{4} a \sin \gamma,$$

$$\dot{\gamma} = 2 \left( \frac{2 - \bar{\Omega}}{\varepsilon} \right) - \frac{6}{8} K a^2 - \frac{\alpha_6}{2} \cos \gamma.$$


**Trans-critical bifurcation:**  
 The normal form for a generic pitchfork bifurcation of a fixed point is

$$\dot{x} = F(x; \mu) = \mu x - x^2$$


MOOCS/IITG/ME/SKD/18 23

This point has to be remember this point has to be taken care while distinguishing between the saddle node bifurcation point, trans critical bifurcation point and these pitch fork bifurcation point. Particularly from the shape also we can decide that thing. So, in case of a saddle node bifurcation point at the saddle point. So, the two branch are the meeting point of the two branch.

So, they will have the same tangent what in case of pitchfork bifurcation the from the shape itself it can be known that this is pitchfork. So, it is starting, so like a pitchfork. So, pitchfork we know. So, the pitchfork type of bifurcation and here also the generic form is mu x minus x cube.

(Refer Slide Time: 45:12)

$\dot{x} = F(x; \mu) = \mu x - x^3$

So,  $\mu x - x^3 = 0 \Rightarrow x(\mu - x^2) = 0$

the trivial solution i.e.,  $x = 0$  and the non trivial solution  $x = \pm\sqrt{\mu}$

$J = D_x F = \mu - 3x^2$

for the trivial branch  $J = \mu$

$\lambda = \mu.$

nontrivial solution

$\lambda = \mu - 3x^2 = \mu - 3\mu = -2\mu.$

$[D_x F \quad F_\mu] = [\mu - 3x^2 \quad x]$

MOOCS/IITG/ME/SKD/18 24

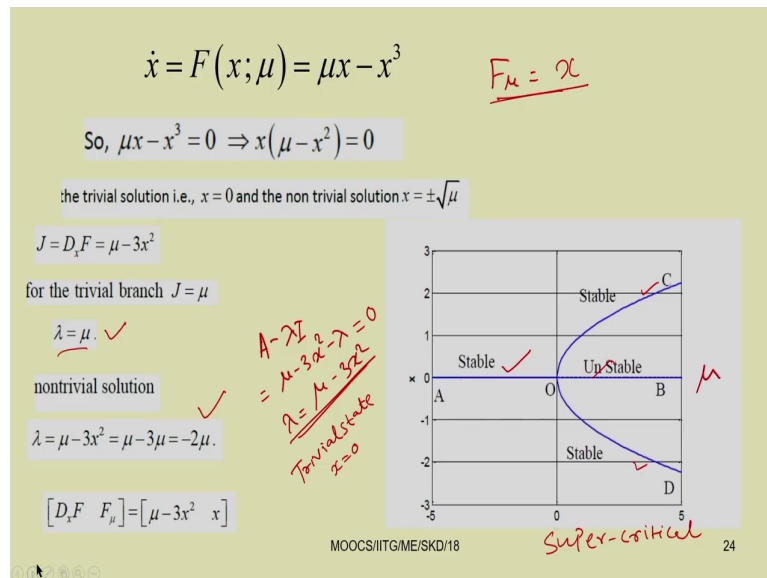
So,  $\dot{x}$  equal to  $\mu x$  minus  $x$  cube. So, in that case let us see. So,  $\dot{x}$  equal to  $F(x; \mu)$ . So, it is equal to  $\mu x$  minus  $x$  cube. So, by putting these  $\dot{x}$  equal to 0. So, we will get the equilibrium position. So,  $\mu x$  minus  $x$  cube equal to 0. So, by taking these  $x$  common. So,  $x$  into  $\mu$  minus  $x$  square equal to 0. So,  $x$  equal to 0 is an equilibrium point and also  $x$  square equal to  $\mu$  is also an equilibrium point.

So, you have three equilibrium points one is  $x$  equal to 0 and other  $1 \pm \sqrt{\mu}$  will be another two equilibrium points. By plotting these things we can plot  $x$  versus  $\mu$  that is equal to 0 or  $b$  also  $a$  to  $b$  the trivial state that is  $x$  equal to 0 and this non trivial state.

So, this is  $\mu$  versus  $x$  you can plot  $\mu$  versus  $x$  you can this is  $x$  this is  $\mu$   $x$  axis a  $y$   $x$  axis is  $\mu$   $x$  axis is  $\mu$  and  $y$  axis is  $x$ . So, by plotting these thing, so now, you can see the

Jacobian matrix. So, differentiating these thing mu x minus x cube. So, we will get the Jacobian matrix. So, this becomes mu minus 3 x square, so for the trivial state.

(Refer Slide Time: 46:36)



So, we can find this A minus lambda i. So, we can do A minus lambda i. So, in this case, so A is the Jacobian matrix or j minus lambda i. So, this becomes mu minus 3 x square minus lambda making this thing equal to 0. So, we will get lambda equal to mu minus 3 x square. So, mu minus 3 x square is the. So, mu minus 3 x square, so for trivial state as x equal to 0.

So, lambda equal to mu, so for trivial state. So, this is the trivial state. So, here x equal to trivial state x equal to 0, so as x equal to 0, so we have lambda equal to mu. So, for non trivial state, so for non trivial state, now lambda equal to mu minus 3 x square. So, by putting different value of already we have these x square equal to; x square equal to mu x equal to plus minus root over mu.



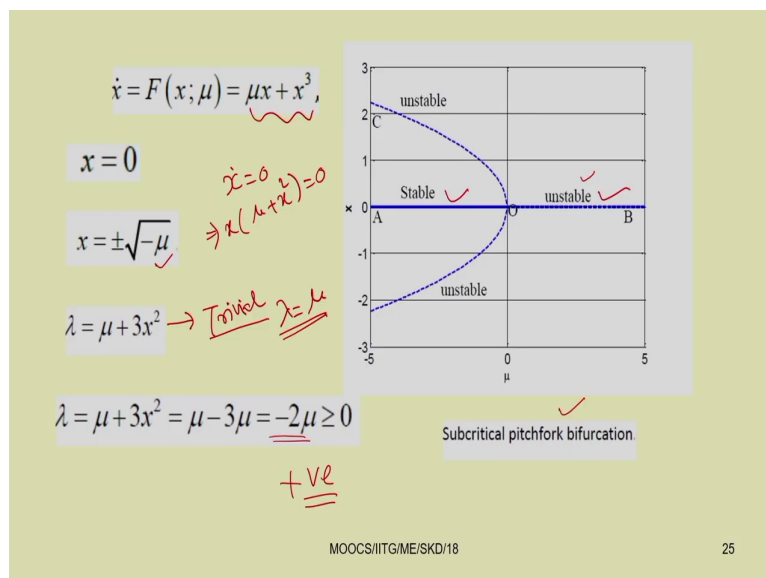
So,  $x^2 = \mu$ . So, by putting these things so we can have  $\mu - 3\mu$  this is  $-2\mu$ . So, you can check for non trivial branch. So, the  $\lambda$  that is the eigenvalue becomes  $-2\mu$ , now by putting this different value of  $\mu$ . So, we can find whether the system is stable or unstable, here from A to 0.

So, from A to 0, so that is  $\mu < 0$ , so this is  $\mu$  value. So, for  $\mu < 0$ , so if  $\mu < 0$  for the trivial branch, so  $\mu$  is negative. So, this part  $\mu = \text{negative}$ . So, eigenvalue is negative that is why this is stable and for 0 to B branch, so  $\mu$  is positive. So, as  $\mu$  is positive  $\lambda$  is positive. So, from this equation  $\lambda$  is positive.

So, as  $\lambda$  is positive the response is unstable, so the system is unstable. So, now, for the other two branches let us see. So, this becomes  $-2\mu$  as to the right hand side for this non trivial branch  $\mu$  is always positive. So,  $-2\mu$  is always negative. So, this branch and this branch, so both the branches are then stable these type of bifurcation.

So, from where, so it is moving from a stable trivial state two stable non trivial state is known as super critical pitch fork bifurcation. So, this is super critical super critical pitchfork bifurcation, in this case  $\mu = x^3$ . So, this is super critical pitchfork bifurcation.

(Refer Slide Time: 49:36)



Similarly we can see here again you just see you can check by constructing this DF x and F mu. So, what is F mu in this cases so F mu, so find F mu. So, if you differentiate this with respect to mu. So, you will get F mu equal to x yes or no. So, F mu equal to x. So, for the trivial state x equal to 0. So, F mu equal to 0 already D x F equal to 0.

So, it has a rank of, so this becomes 0 and this becomes 0, so this is 0 0. So, the rank becomes 0. So, this rank is not one here. So, the rank as we have seen there, so rank is n minus 1. So, in this case we can differentiate or from this thing from the saddle node bifurcation point from or by constructing these D F D x F and F mu matrix.

Now, you just take the other one that is x dot equal to F x mu, but you take x dot equal to mu x plus x cube. So, previously we have taken mu x minus x cube. So, here it is mu x plus x

cube. So, if you take  $\mu x + x^3$ . So, then  $\dot{x} = 0$ . So,  $\dot{x} = 0$  putting  $\dot{x} = 0$ . So, we have this taking this  $x$  common. So,  $x(\mu + x^2) = 0$ .

So,  $x = 0$  is one solution and the other solution becomes  $x = \pm \sqrt{-\mu}$ . So, this is the other two solutions. So, we have three solutions here and if we can plot it. So, we can see this one, similarly for trivial state. So, for trivial branch let us find the Jacobian matrix. So, Jacobian matrix from the Jacobian matrix. So, differentiating this thing with respect to  $x$ .

So, the Jacobian matrix you will get  $\mu + 3x^2$ . So, for trivial state by putting these  $x = 0$ . So,  $\lambda = \mu$ . So,  $\lambda = \mu$  for the trivial state and here  $\mu < 0$ . So, this branch is stable and  $\mu > 0$ . So, this branch is unstable, similarly for the non trivial state our  $\lambda$  becomes  $-2\mu$   $\lambda$  becomes  $-2\mu$ , but in this case this  $\mu$  is negative  $-2\mu$  is positive.

So,  $-2\mu$  is positive as  $\lambda$  is positive that is the eigenvalue is positive. So, these branches are unstable. So, this is unstable branch. So, here that means, these stable and unstable branch.

So, this one non trivial stable and two non trivial unstable leads to, these unstable branches after the bifurcation. So, already we know the bifurcation point at bifurcation point either it change the response in this qualitatively or quantitatively. So, in this case these three branch merge to have a single branch.

So, that is a number. So, the number is changing. So, that is why it is a bifurcation point also the stability type of stability is also changing. So, here as the resulting response is unstable previously we have a stable branch and two unstable branch. Now this becomes completely unstable.

So, this is known as subcritical pitchfork bifurcation which is a dangerous bifurcation because after this thing as there is no solution available the system response may jump to infinite and

the system may tend to an unstable region or it may be; it may be the system may be the system may get damaged.

(Refer Slide Time: 53:39)

**Hopf bifurcation:**  
The normal form for a generic Hopf bifurcation of a fixed point is

$$\dot{x} = \mu x - \omega y + (\alpha x - \beta y)(x^2 + y^2)$$
$$\dot{y} = \mu x - \omega y + (\alpha x - \beta y)(x^2 + y^2)$$

MOOCS/IITG/ME/SKD/18 26

So, let us see the hopf bifurcation this is the dynamic bifurcation.

(Refer Slide Time: 53:45)

1.  $F(x_0; \mu_c) = 0$  ✓

2. The Jacobian matrix  $\left( D_x F = \frac{\partial F}{\partial x} \right)$  has a pair of purely imaginary eigenvalues  $\pm i\omega$  while all of its other eigenvalues have non zero real parts at  $(x_0; \mu_c)$ . Hence, the point is a nonhyperbolic fixed point

3. For  $\mu = \mu_c$ , let the analytical continuation of the pair of imaginary eigenvalues be  $\lambda \pm i\omega$ . Then,  $\frac{\partial \lambda}{\partial \mu} \neq 0$  at  $\mu = \mu_c$ . This condition is known as the transversality condition as the eigenvalue crosses the imaginary axis with nonzero speed.

When all the above three conditions are satisfied, a periodic solution of period  $2\pi/\omega$  is developed at  $(x_0; \mu_c)$ . Such bifurcations are called Hopf bifurcation or Poincare'-Andronov Hopf bifurcation.

27

So, in case of the dynamic bifurcation. So, we have this  $F(x, \mu) = 0$  must be equal to 0 this is the first condition and the second condition is the Jacobian matrix  $D_x F$  that is  $\frac{\partial F}{\partial x}$  has a pair of purely imaginary eigenvalues. So, it must you see the real part is 0, but it must have a pair of imaginary eigenvalues that is plus minus  $i\omega$ .

So, it will have plus minus  $i\omega$  while all of its other eigenvalues have nonzero real parts at  $x_0, \mu_c$ . Hence the point is a non hyperbolic fixed point. The third point is for  $\mu$  equal to  $\mu_c$  let the analytical continuation of the pair of imaginary eigenvalues be  $\lambda \pm i\omega$ , then  $\frac{\partial \lambda}{\partial \mu} \neq 0$  at  $\mu = \mu_c$ . So, this condition is known as the transversality condition as the eigenvalues crosses the imaginary axis with nonzero speed.

As they are crossing the imaginary axis with the nonzero speed, so it will give rise to periodic response. So, when all the above three conditions are satisfied a periodic solution of two pi by omega is developed at  $\mu = \mu_c$  such bifurcations are called hopf bifurcation or Poincare Andronov Hopf bifurcation. So, this is hopf bifurcation. So, in case of hopf vibration, so from the fixed point response we are getting the periodic response.

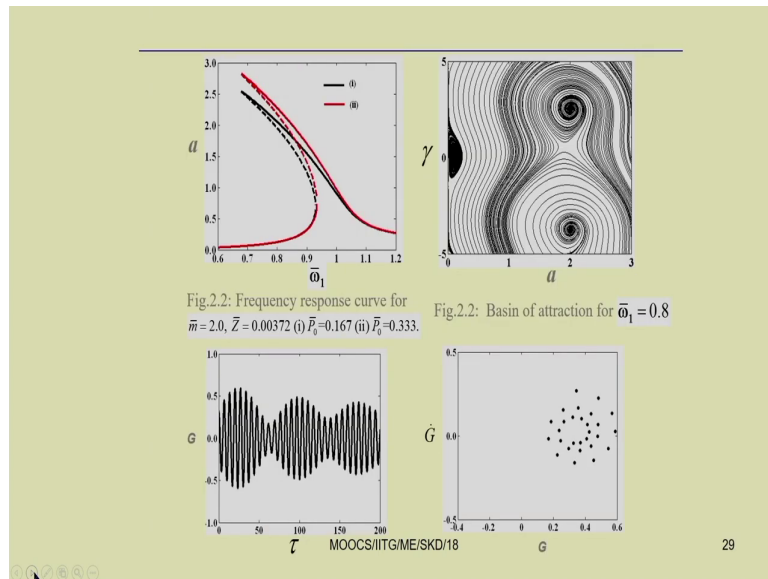
So, if from a stable fixed point we are getting stable periodic response, then it will be known as super critical hopf bifurcation and in case of subcritical hopf bifurcation from a unstable fixed point.

So, we are getting a stable fixed point along with a periodic response we can have supercritical or subcritical hopf bifurcation points. So, the generic form of the hopf bifurcation can be written in this way  $\dot{x} = \mu x - \omega y + \alpha x - \beta y - (x^2 + y^2)$  and  $\dot{y} = \omega x + \mu y + \beta x - \alpha y - (x^2 + y^2)$ .

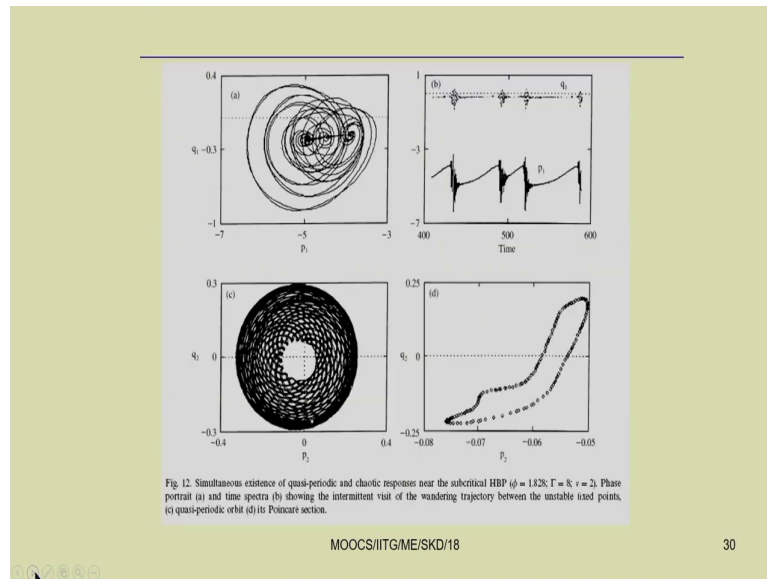
Now, by making this thing equal to 0. So, we can get the equilibrium conditions or equilibrium points and or the fixed points and finding the eigenvalue. So, we can see how by changing the system parameter  $\mu$  how the eigenvalue are varying. So, we can see at the critical point. So, it is crossing the imaginary axis with nonzero real part with nonzero imaginary parts.

So, if they are crossing the imaginary axis with nonzero real part or a nonzero imaginary parts, then we are going to get the hopf bifurcation. So, we will see different examples later how this 3D or all these types of bifurcations are occurring in real systems.

(Refer Slide Time: 56:59)



(Refer Slide Time: 57:03)



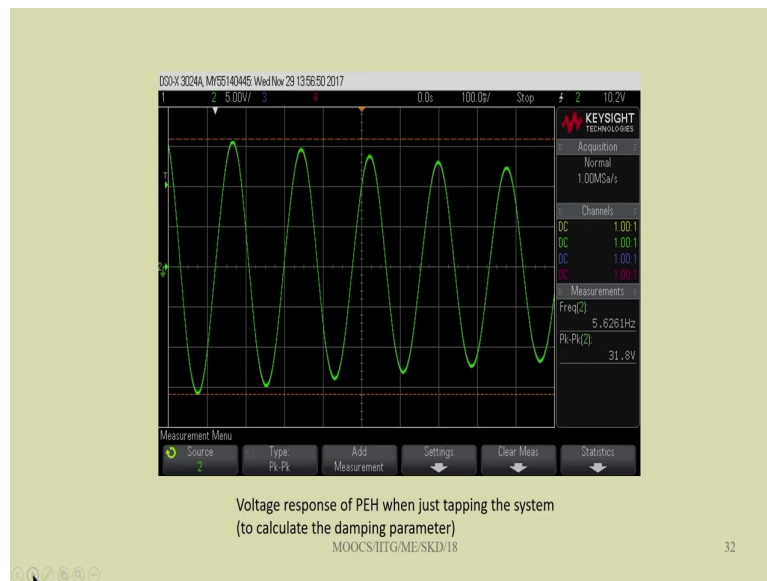


(Refer Slide Time: 57:05)



So, these are some of the examples also you can take. So, where it leads to chaotic response. So, you can see some of the experiments also can be conducted to study all these system for example, let us take a beam. So, this beam can be vibrated to see the response.

(Refer Slide Time: 57:19)



So, some of the response it is. So, by putting this accelerometer or by putting this oscilloscope you can also check the vibration of the system.

(Refer Slide Time: 57:32)

**Duffing equations with Fractional Order Derivative**

$$m\ddot{x} + c\dot{x} + k_d D_t^p [x(t)] - kx + \alpha x^3(t) = F \cos \omega t$$
$$D_t^p [x(t)] = \begin{cases} \frac{1}{\Gamma(1-p)} \int_0^t \frac{x'(\tau)}{(t-\tau)^p} d\tau & 0 < p < 1 \\ \frac{dx}{dt} & \\ \frac{1}{\Gamma(2-p)} \int_0^t \frac{x''(\tau)}{(t-\tau)^p} d\tau & 1 < p < 2 \end{cases}$$

Following Caputo definition of fractional order derivative one may write

- J. Niu, R. Liu, Y. Shen and S. Yang, Chaos detection of Duffing System with fractional-order derivative by Melnikov method, Chaos, 29,123106 (1919) doi:10.1063/1.5124367
- I. Petras, Fractional order Nonlinear systems, Higher Education Press, Beijing, 2011

MOOCS/IITG/ME/SKD/18 35

In addition to duffing equation what you have seen before. So, we can have different other type of duffing equation. So, here is one duffing equation duffing equation with the fractional order derivative. So, here these additional term you can see. So, that is known as the fractional order. So, you can study many different type of duffing equations and their response and which will lead to many different type of bifurcation points also.

So, with this thing we will close this class today and we will study the periodic response which generally occur in case of a parametrically excited system. So, we have finished the fixed, we have finished the force vibration or direct excitation system directly excited systems. Next class we will see the systems which are parametrically excited.

Thank you very much.

