

Advanced Composites
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Lecture - 32
Generalized Solution for Semi-Infinite Plate (Part-II)

Hello, welcome to Advanced Composites. Today is the second day of the ongoing week which is the second week of this course which is the 6th week; I am sorry 6th week of this particular course. And yesterday, we just started solving these 3 important governing equations for laminated composite plates in context of semi-infinite plates.

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SOLVE THE PROBLEMS TO A POINT TILL NO BC'S ARE APPLIED

$$\frac{\partial}{\partial y} = 0 \quad \frac{\partial}{\partial x} = \frac{d}{dx}$$

GOVERNING DIFF EQNS

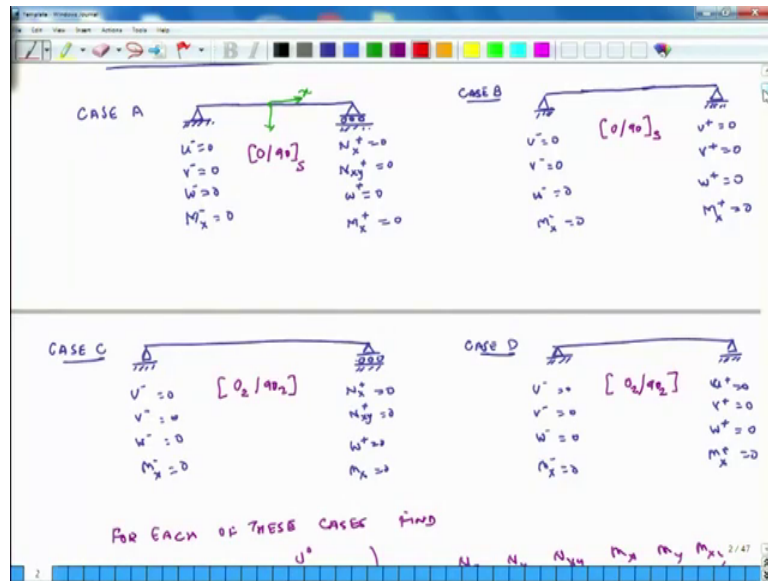
$$\frac{\partial N_x}{\partial x} + \frac{\partial N_{xy}}{\partial y} = 0 \rightarrow \frac{dN_x}{dx} = 0 \rightarrow N_x = C_1 \quad \textcircled{1}$$

$$\frac{\partial N_{xy}}{\partial x} + \frac{\partial N_y}{\partial y} = 0 \rightarrow \frac{dN_{xy}}{dx} = 0 \rightarrow N_{xy} = C_2 \quad \textcircled{2}$$

$$\frac{\partial^2 M_x}{\partial x^2} + \frac{\partial^2 M_{xy}}{\partial x \partial y} + \frac{\partial^2 M_y}{\partial y^2} + \rho(x) = 0 \rightarrow \frac{d^2 M_x}{dx^2} = -\rho \rightarrow M_x = -\frac{\rho x^2}{2} + C_3 x + C_4 \quad \textcircled{3}$$

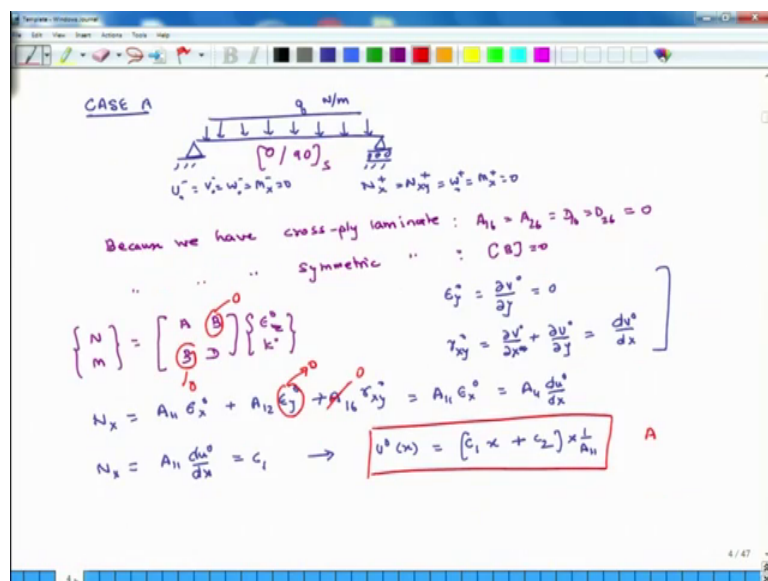
And what we had developed yesterday is first we developed 3 relations for N_x , N_{xy} and M_x and what we saw is that N_x equals C_1 and N_{xy} equals C_2 and M_x equals minus ρx^2 over 2 plus $C_3 x$ plus C_4 . And these 3 equations are valid for all the 4 cases which we had discussed earlier.

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So, these are the 24 cases which we had explained earlier in case A and case B, we have a symmetric laminate; in case C and case D, we have an un symmetric laminate and case A and case C have similar boundary conditions actually same boundary conditions that is pinned and fixed on one end and fixed and roller on the other end while case B and case D have pinned and fixed and so on both the ends. So, these are the 4 different cases we would like to solve. So, the first step was that we solved for $N \times N \times y$ and $M \times x$ and these solutions are same for all the 4 cases.

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And then, we started applying the lamination sequence. So, by virtue of lamination sequence, so, we still have not yet applied the boundary conditions by virtue of lamination sequence. We have seen that $\epsilon_y = 0$ $\gamma_{xy} = 0$ $\nu = \frac{dv}{dx}$. And when we do all the math, we also find out that $u = C_1 x + \frac{C_2}{A_{11}}$.

So, this is what we had accomplished till that point of time and what we will do is actually we will name this equation as equation 4. So, this is 4 equation number 4. So, we will proceed and we will continue to solve for u , v and w . So now, we will try to find out the value of v . So, how do we do that?

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The image shows a whiteboard with handwritten mathematical derivations. At the top, it says "Symmetric". The main equations are:

$$\begin{Bmatrix} N \\ M \end{Bmatrix} = \begin{bmatrix} A & B \\ B & D \end{bmatrix} \begin{Bmatrix} \epsilon \\ \kappa \end{Bmatrix}$$

Boundary conditions are given as $\epsilon_y = \frac{\partial v}{\partial y} = 0$ and $\gamma_{xy} = \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} = \frac{dv}{dx}$.

The normal stress N_x is derived as:

$$N_x = A_{11} \epsilon_x + A_{12} \epsilon_y + A_{16} \gamma_{xy} = A_{11} \epsilon_x = A_{11} \frac{du}{dx}$$

This is equated to C_1 , leading to the displacement function:

$$u^0(x) = \left(\frac{C_1}{A_{11}} x + C_5 \right) \frac{1}{A_{11}} \quad (4)$$

The normal stress N_y is derived as:

$$N_y = A_{12} \epsilon_x + A_{22} \epsilon_y + A_{26} \gamma_{xy} = \dots \quad (5)$$

The shear stress N_{xy} is derived as:

$$N_{xy} = A_{16} \epsilon_x + A_{26} \epsilon_y + A_{66} \gamma_{xy} = A_{66} \frac{dv}{dx} = C_2$$

This leads to the displacement function:

$$v^0 = \left(\frac{C_2}{A_{66}} x + C_6 \right) \frac{1}{A_{66}} \quad (6)$$

So, we know that $N_x = A_{12} \epsilon_x + A_{22} \epsilon_y + A_{26} \gamma_{xy}$ ok. And all the other terms are 0 which involved the B matrix. So, I have only considered A_{12} , A_{22} and A_{26} terms. I have not included B_{11} , B_{12} , B_{22} and B_{26} terms because they are identically 0 because the matrix is symmetric. And also, we know that $\epsilon_y = 0$ and $\gamma_{xy} = 0$; oh I am sorry, not γ_{xy} . This A_{26} is 0 because the laminate is cross ply and symmetric and because it is cross ply, then A_{26} will be 0.

So, the second 2 later 2 terms in this whole equation becomes 0 and ϵ_x is already there in place. So, this ϵ_x when we see it is equal to C_1 / A_{11} how do

we get C_1 over A_1 from this equation ok. Here, $\frac{du}{dx}$ is ϵx . So, ϵx is equal to C_1 over A_1 ok.

So, what this gives us is that $N_x y$ is equal to A_2 over A_1 times C_1 . So, this is another relation we get and that is 5.

Student: Sir, can you put at the place of (Refer Time: 03:49) 4 (Refer Time: 03:50) $C_1 x$ plus S_2 and you already use (Refer Time: 03:54) another constant (Refer Time: 03:56) 4.

[FL] 4 or 5.

Student: 4

Oh [FL].

Student: (Refer Time: 04:02) [FL] (Refer Time: 04:03) $N_x y$ (Refer Time: 04:05).

Oh yeah, yeah yes. So, one thing we did earlier is that we have used this constant C_2 , but C_2 has already been used earlier. So, instead of C_2 , we will use a new constant. We will call it C_5 ok. This relation for $N_x y$ I mentioned is incorrect. So, this should be for N_y ok. This should be for N_y N_y is equal to $A_2 \epsilon x$ plus $A_2 \epsilon y$ and so on and so, forth. And so, likewise this relation gets changed and corrected and this is actually for normally the third relation is.

So, we have N_y N_x N_y and the third relation is for $N_x y$, third relation is for $N_x y$ and what it tells us is that this is equal to $A_1 \epsilon x$ plus $A_2 \epsilon y$ plus $A_6 \gamma x y$. Now, once again A_1 is 0 A_2 is 0 and $\gamma x y$ is $\frac{dV}{dx}$ in our case which we have developed here ok. So, if that is the case, so, this simplifies to $A_6 \frac{dV}{dx}$ and we have seen that $N_x y$ from equation 2 is equal to C_2 . From this equation, it is equal to C_2 .

So, we will use that here. So, what I get is and I when I integrate it I get V is equal to $C_2 x$ plus C_6 into $\frac{1}{A_6}$. So, this is I will call it equation 6. So, we have developed an expression for U we have developed an expression for V and what is remaining is an expression for W .

So, for W, let us look at it further M x using the A B D relation. So, when we see from this equation M is equal to B times epsilon naught plus D times K naught, but B is 0. So, the only terms which matter are terms related to D in this thing.

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$$N_{xy} = A_{16} \epsilon_x + A_{26} \epsilon_y + A_{64} \kappa_y$$

$$V^0 = (c_2 x + c_6) \times \frac{1}{A_{66}} \quad (6)$$

$$M_x = D_{11} \kappa_x + D_{12} \kappa_y + D_{16} \kappa_{xy} = -D_{11} \frac{d^2 w}{dx^2} = -\frac{q x^2}{2} + c_3 x + c_4$$

$$\frac{dw^0}{dx} = \frac{-1}{D_{11}} \left[-\frac{q x^2}{6} + c_3 \frac{x^2}{2} + c_4 x + c_7 \right]$$

$$w^0(x) = \frac{-1}{D_{11}} \left[-\frac{q x^3}{24} + \frac{c_3 x^3}{6} + c_4 \frac{x^2}{2} + c_7 x + c_8 \right]$$

So, M x is equal to D 1 1 K x plus D 1 2 K y. So, these are all mid plane strains mid plane curvatures plus D 1 6 K x y. Because we have the laminate which is having all cross ply layer 0 degrees and 90 degrees D 1 6 is 0 also, because K y is the second derivative of w with respect to y direction. So, this is also 0. So, the only thing which I am left with is D 1 1 times K x. So, this is equal to minus D 1 1 del 2 W naught over del x square and because it is a very long plate. All the second derivatives with respect to x are actually we can consider them as total derivatives. So, I call this as D 2 W over d x square ok.

And now, we have seen from equation 3 that M x is equal to minus q x square plus C 3 x plus C 4. So, I use bring that relation down here. So, this is equal to minus q x square over 2 plus C 3 x plus C 4. So now, what I do is I integrate this equation twice. So, I get d W naught over d x equals minus 1 over D 1 1 and I am integrating this relation for the first time. So, I get minus q x cube over 6 plus C 3 x square over 2 plus C 4 x plus C 7 and if I integrate it one more time, this is what I get minus q x 4 over 24 plus C 3 x cube over 6 plus C 4 x square over 2 plus C 8. So, this is my

Student: (Refer Time: 11:19).

Yes, plus $C_7 x$ plus C_8 . So, this is my relation W , ok. So, we will do as we will summarize all these relations.

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$$U'(x) = \frac{C_1 x + C_5}{A_{11}} \quad V'(x) = (C_2 x + C_6) \times \frac{1}{A_{66}}$$

$$W'(x) = -\frac{1}{D_{11}} \left[-\frac{q x^4}{24} + C_3 \frac{x^3}{6} + C_4 \frac{x^2}{2} + C_7 x + C_8 \right]$$

$$N_x = C_1 \quad N_y = \frac{A_{12}}{A_{11}} C_1 \quad M_{xy} = C_2$$

$$M_x = -\frac{q x^2}{2} + C_3 x + C_4 \quad M_y = \frac{D_{22}}{D_{11}} M_x \quad M_{xy} = 0$$

VALID FOR CASE A and CASE B.
 \therefore B Cs have not been implemented yet so far.

So, U naught x is equal to $C_1 x$ plus C_5 over A_{11} , V naught x is equal to $C_2 x$ plus C_6 into 1 over A_{66} and W naught x equals minus 1 over D_{11} minus $q x^4$ over 24 plus $C_3 x^3$ over 6 plus $C_4 x^2$ by 2 plus $C_7 x$ plus C_8 . So, that is the relation for W and so, this is one block of equations which tell us about U , V and W .

And then, we will also write down expressions for M S and N s. So, N_x is equal to C_1 , N_y equals A_{12} over A_{11} C_1 , N_{xy} equals C_2 . M_x is equal to minus $q x^2$ over 2 plus $C_3 x$ plus C_4 and my now if you do the math, what is M_y ? M_y is equal to D_{22} over D_{11} M_x plus D_{26} over D_{11} M_{xy} and if we do the math similarly in the way which we have explained earlier, what we find is that M_y is nothing but D_{22} over D_{11} Times M_x see this relation is very similar to this relation. So, it the mathematics is very similar. So, anyway; so, that is what is M_y and M_{xy} is equal to 0 . So, this is what we find. So, this is the second set of relations.

So now, reveal let us review the first 3 relations which we developed here. These are valid for all the 4 cases because here we never applied any things related to the material. We started with these general differential equations and the only simplification we did in these simply equations was that $\frac{\partial}{\partial y} = 0$ and $\frac{\partial}{\partial x} = D$ over dx and these simplifications are valid for all the 4 cases.

So, if these equations are valid for all the 4 cases, we can use these 4 3 equations for all the 4 cases, then the next thing we started doing was that we considered the laminate is symmetric. And when laminate is symmetric, then we said the D matrix is 0 and also we said that laminate is not only symmetric, but it has all the layers in 0 and 90 degrees direction. So, that means, A_{16} A_{26} D_{16} d_{26} are also 0.

So, using these 2 facts that B is 0 and A_{16} A_{26} D_{16} d_{26} are 0, we again calculated relations for displacements and N_x and N_y and we came up with these equations. So, these equations are valid for case A and case B. Why they are valid for case A and case B? Because, we have not used boundary conditions till so far because B C S have not been implemented till so far.

We have not implemented the B C's and because we have not implemented the B C's. They are valid for case A and case B because both these cases have the same lamination sequence which is 0 90 symmetric and for 0 90 symmetric or laminate which is symmetric and which has z. These lies in 0 and 90-degree direction, these equations are valid. So, these equations are valid for case A and case B.

The last thing I will like to show is that when we came up with these equations, how many constants? We have constants of integration we have ended up with 8 integration constants; C_1 C_2 C_3 till C_8 and we do not know the values of these 8 different integration constants. The way we are going to calculate or find out they are values is from the boundary condition.

Now, let us look at. So, we have 8 integration constants which we do not know, but then you also see that there are 8 different conditions for each case. So, we know 4 conditions at one end of the plate and 4 conditions at the other end of the plate and we will use these 8 different conditions to evaluate the values of these constants. And in that way, we will be able to solve for the actual solution for U V W and also for N_x N_y M_x M_y .

So, that is how we are going to solve this thing. So, we have 8 integration constants which we will find out by implementing 8 boundary conditions. The value of these integration constants may be different for different set of boundary conditions. So, anyway, so, that is what we plan to do next and that is what we will start doing tomorrow. So, I look forward to seeing you tomorrow. Until then, have a great day.

Thank you.