

Advanced Composites
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Lecture - 08
General Anisotropic Material

Hello welcome to Advanced Composites. Today is the second day of this ongoing week which is the second week of the course. Yesterday we introduced you with all the sign convention for stresses, strains and we also introduced the notion of a tensor.

Further, we explained how stress is the second order tensor, a strain is also second order tensor because in both these cases the quantities stress and strain are associated with 2 mutually independent sets of directions. In case of stress these 2 directions correspond to the direction of the plane on which the force is acting and also the direction of the force and in the case of strain these 2 sets of directions correspond to the direction of displacement and the direction in which its partial difference is been calculated.

We also saw yesterday that the mathematical relationship between stress and strain is through a fourth order elasticity tensor which is E_{ijkl} . So, now, we will further discuss this particular tensor in context of anisotropic materials ok.

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The image shows a whiteboard with handwritten mathematical derivations. At the top, the stress tensor σ_{ij} is defined as a double sum over indices k and l from 1 to 3: $\sigma_{ij} = \sum_{k=1}^3 \sum_{l=1}^3 E_{ijkl} \epsilon_{kl}$. A red box highlights the E_{ijkl} term, with a red arrow pointing to the number 6 below it, indicating 6 independent components. To the right, a list of indices i, j, k, l is shown with a bracket indicating they range from 1, 2, 3. Below this, the strain tensor ϵ_{kl} is defined as $\epsilon_{kl} = \epsilon_{lk}$. The strain tensor is also expressed as $\epsilon_{kl} = \left(\frac{\partial u_l}{\partial x_k} + \frac{\partial u_k}{\partial x_l} \right) \times \frac{1}{2}$. At the bottom, the symmetry $\epsilon_{kl} = \epsilon_{lk}$ is boxed in red, and a large red bracket is drawn to the right.

So, what we had developed yesterday was $\sigma_{ij} = \text{double summation } E_{ijkl}$; ϵ_{kl} and here we are summing on these indices. So, l equals 1 to 3 and k equals 1 to 3. So, once again here indices $ijkl$ all of them could assume values of 1 2 and 3 and 1 2 3 are basically axis 1 could be x axis, 2 could be y axis and 3 could be z axis.

Now, if you look at E_{ijkl} tensor; it could have 81 different values why? Because we will have 81 different combinations of E_{ijkl} because i can assume 3 different values 1 2 3; j can assume 3 different values 1 2 3 and so on and so forth. So, the total number of combinations of E_{ijkl} would be 3 times 3 times 3 times 3 and that corresponds to 81 ok. So, in general this relation between stresses and strains involves 81 different elastic constants. So, for an isotropic material we are starting with the situation where there are 81 different elastic constants ok.

So, the next now we start simplifying this. So, the first simplification we do is based on the fact that $\epsilon_{kl} = \epsilon_{lk}$; why is that? So, the definition of a strain tensor is $\epsilon_{kl} = \frac{1}{2} (\frac{\partial u_k}{\partial x_l} + \frac{\partial u_l}{\partial x_k})$ ok. So, x_k ; x_1 would be x, x_2 will be y, x_3 will be z and so on and so forth.

So, this is $\frac{1}{2} (\frac{\partial u_k}{\partial x_l} + \frac{\partial u_l}{\partial x_k})$ and this entire thing into 1 by 2 ok. So, this is the definition of strain and when you; so, this comes from mathematics we will not go into that and what you find is because of this $\epsilon_{kl} = \epsilon_{lk}$ is equal to ϵ_{lk} right.

So, what; that means, is that if $\epsilon_{lk} = \epsilon_{kl}$ then the number of independent constants in this block k, l ; will not be 9, if it they were if this equivalence was not true; then this would be the number of independent constants involved with subscripts k and l would be 9; 3 into 3, but now if there is 3 by 3 matrix; then this matrix will be symmetric which means that there will be 6 different possible combinations not 9.

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$\epsilon_{kl} = \sigma_{lk}$
 $\epsilon_{kl} = \left(\frac{\partial U_0}{\partial x_k} + \frac{\partial U_0}{\partial x_l} \right) \times \frac{1}{2}$

$\epsilon_{kl} = \epsilon_{lk}$

No. of ind. elastic constants : $3 \times 3 \times \frac{6}{\uparrow k_l} = 54$

So, if that is the case when the number of elastic constants; number of independent elastic constants it comes down to 3 times 3 times 6. So, this is because k_l is symmetric matrix; epsilon k_l is symmetric matrix. So that means; it is 54. So, all of a sudden the requirement that we have to find out 81 elastic constant it drops down and it comes to 54.

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No. of ind. elastic constants : $6 \times 6 = 36$

$E_{ijkl} \epsilon_{kl} = \sigma_{ij}$

$\tau_{12} = \tau_{21}$ $\tau_{23} = \tau_{32}$ $\tau_{13} = \tau_{31}$

No. of elastic constants : $6 \times 6 = 36$

$81 \rightarrow 54 \rightarrow 36$

Next look at E_{ijkl} and this is multiplied by epsilon k_l . So, that equals sigma i_j ; now we know from principles of mechanics that tau 1 2 equals tau 2 1 tau 2 3 equals tau 3 2 and tau 1 3 equals tau 3 1.

1123 and 1131. Likewise, the second row will have 2211, 2222, 2233, 2212, 2223, 2231 and so on and so forth.

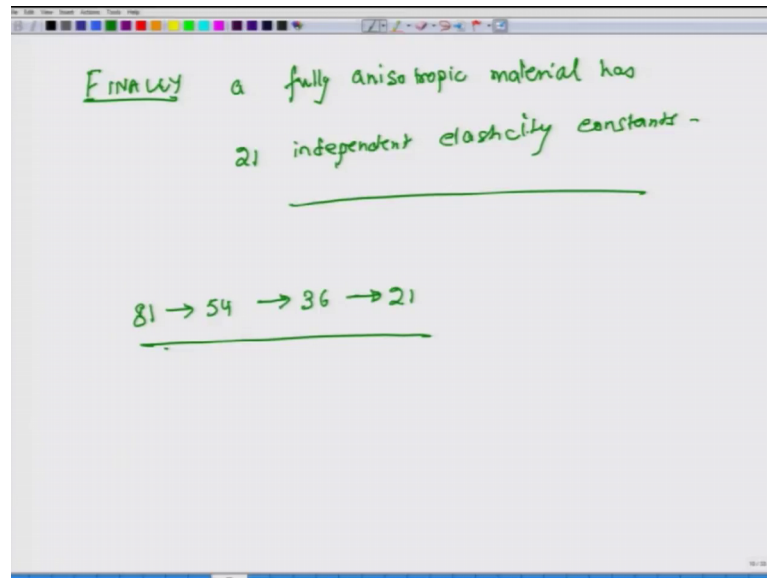
So, you can use this concept you can develop the whole matrix, you can develop the whole matrix. So, will just write one more row; so the next row will be 3311, 3322, 3333, 3312, 3323, 3331 ok. And then we have fourth row, fifth row, sixth row; the sixth row will be 3131 last element.

Now, based on thermodynamic considerations which are related to a strain energy density and the description for this and justification for this has been explained in our introductory course; these are overall 36 independent constants, these are overall 36 independent constants ok. So, these 36 constants come down to 21 because based on thermodynamical considerations which we are not going to explain, there are further simplifications and those simplifications involve imply that this entire matrix is symmetric.

So, this E matrix is symmetric which means; so, if it has to be symmetric then this number should be same as this, this number should be same as this, this number should be same as this, this number should be same as this number should be same as this and so on and so forth ok.

So, a 6 by 6 matrix initially has 36 independent constants, but now because of symmetry, the total number of constants it drops down to 30 it drops down to 21; why it is 21? Because there are 6 independent constants in the first row, 5 independent constants in the second row, 4 independent constant in the third row plus 3 plus 2 plus 1 and so on and so forth. So, if you add these up together it is 21.

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So, this is the final answer; so finally, we can say finally, we can say that a fully anisotropic material has 21 independent elasticity constants it has 21 independent elasticity constants.

So, how did we get here? We started with 81 constants because of symmetry of strain tensor, it came down to 54, because of symmetry of stress tensor it came down to 36. And because of thermo dynamical considerations involving strain and energy density function, it comes to 21. So, this concludes our discussion for today; tomorrow we will continue this discussion and we will show that the number of elastic constants drops down further is the material was specially orthotropic which we have discussed what it means yesterday.

So, for that kind of a situation we will make some more simplifications, but if the material is not specially orthotropic and fully anisotropic; then what it means is that they will be 21 independent elastic constants which will relate stresses and strains. So, that concludes our discussion and I look forward to seeing you tomorrow.

Thank you.