

Solar Energy Technology
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Lecture - 40
Passive Architecture Overhangs and Wing Walls (Contd.)

So, we were considering the passive architecture and we considered number of devices like solar cooker solar steels etcetera. And then we also were considering the so called overhangs and wing walls.

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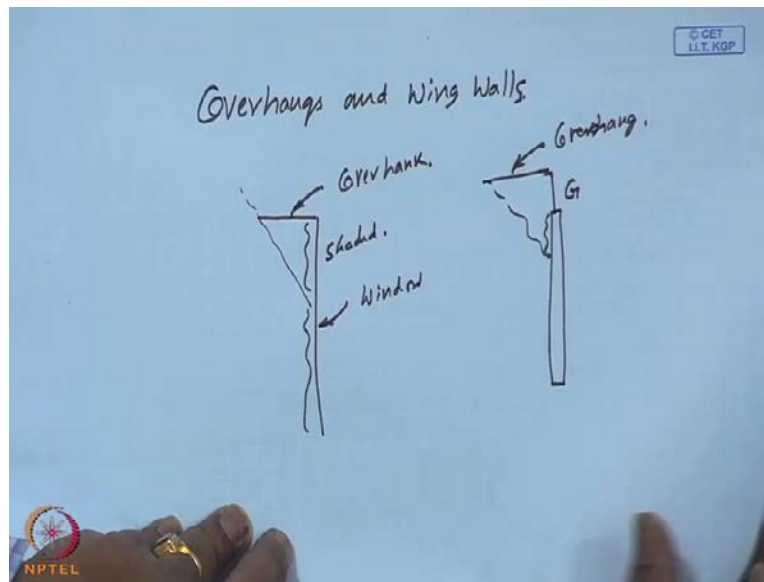
Lecture 40 Overhangs and wing walls

. or a direct gain window, the concept of
“unutilizability” is introduced

Un-utilizability may be defined as the ratio
of solar radiation below a certain critical
level to the total solar radiation. This critical
level, as has been defined earlier, is the solar

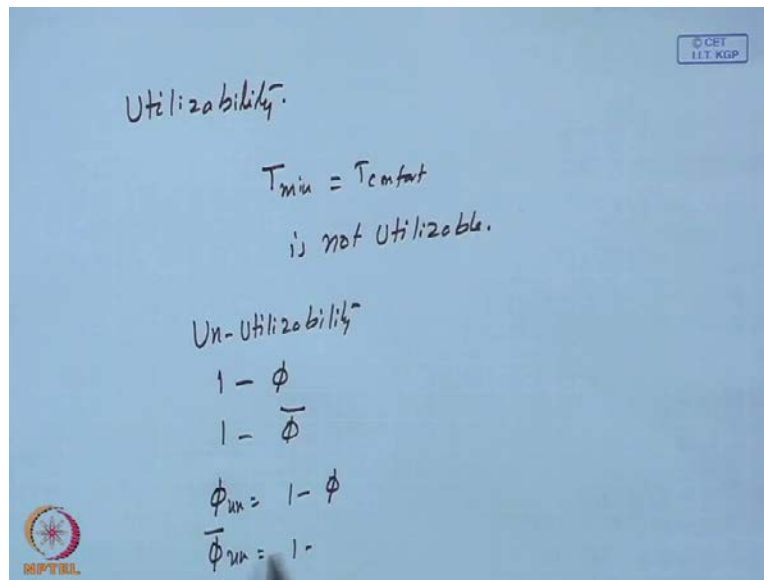


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The whole the idea of if you have got a in the end view, this is the window and this is called the overhang. So, this will not let the sun shaded. Over a certain area, the remaining thing can be lit; and of course you may have also have window certain thing, then a wall and your hang maybe after a certain gap G . Still this may cause the shadow over certain part of the window, and consequently this could be useful in summer and particularly in tropical climates in stopping the solar radiation entering the room, and in winter because the sun is pretty low as I have explained in the last lecture, it will allow the sun's rays to enter the room.

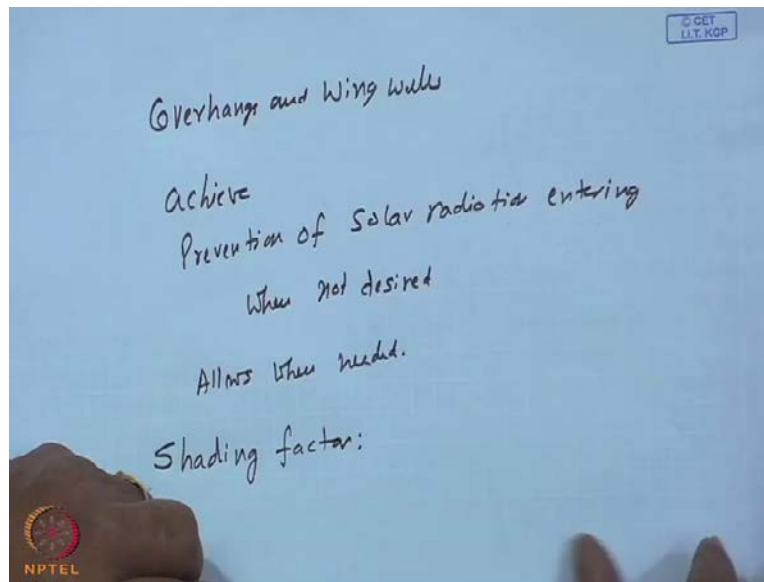
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Now in the context of so called utilizability, which we set that the solar radiation intensity above a certain critical level shall be useful for meeting the energy demand above a particular specified minimum temperature. But, in the case of passive heating the solar radiation above a certain level comparable come to the T_{min} equal to $T_{comfort}$ is not utilizable in other words

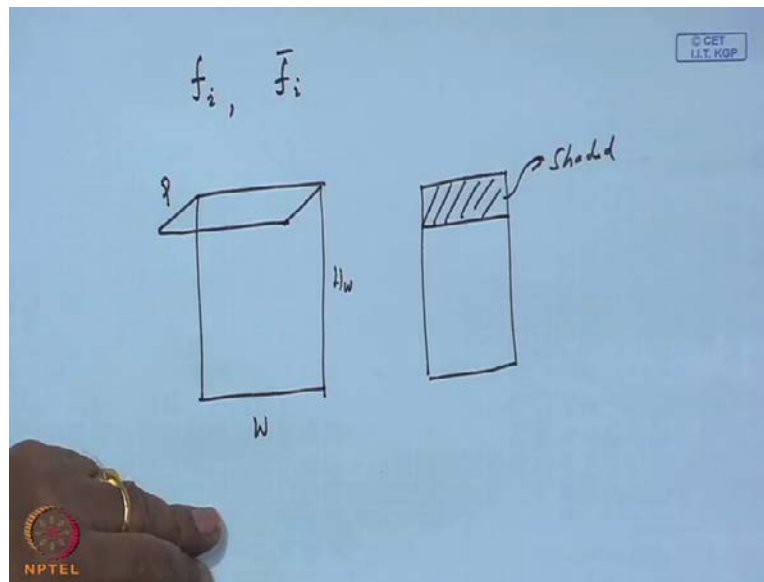
When once the room is at $T_{comfort}$ level any solar radiation above that level shall not be utilized and hence the concept of un-utilizability. So, this sun different times scales will be simply one minus phi or one minus phi bar if you have calculated utilizability unutilizability will be simply one minus that utilizability. So, that is what I have put down here $\phi_{un} = 1 - \phi$ or $\bar{\phi}_{un} = 1 - \bar{\phi}$ and we know the method to calculate phi or phi bar of a monthly average or daily or a hourly average. So, in that context the solar radiation available to you above a particular critical level shall not be utilizable to heat the room because it over heats beyond the comfort condition. The concept is the same the methodology of calculating phi bar remains the same however that energy is not useful for contributing to heating the room. Because, it over heats

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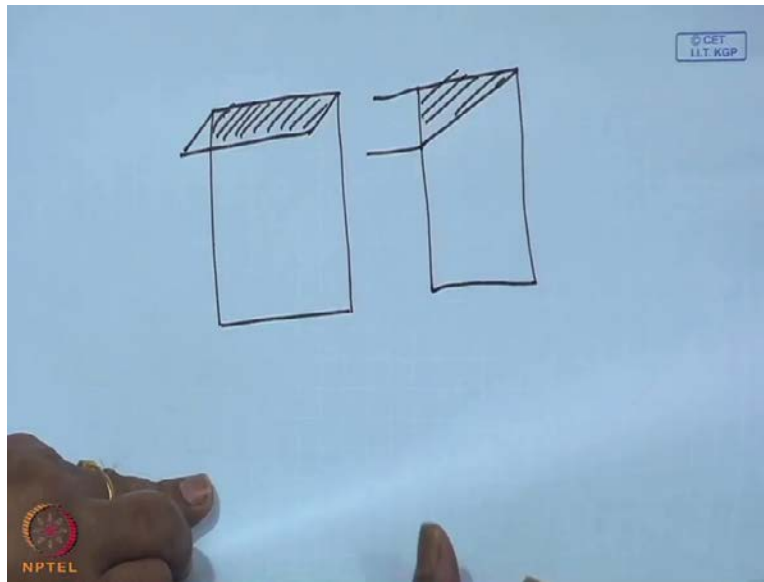
So, these overhangs and wing walls achieve prevention of solar radiation entering when not desired or desired it can be interpreted both ways and allows when needed. And there a number of calculations number of concepts and one of the references is 57 which I will give you at the end of these lectures and then 58 our own work contains the method of calculation of what we call the shading factor which will come just now. So, now you have got a what is called a shading factor. When the window is shaded by the overhang or the wing wall a part of it will not receive the direct solar radiation. Consequently the radiation that this likely to enter through the transmittance of the glass cover will be impaired by the factor which we call the shading factor since the entire window is not exposed to sun's radiation.

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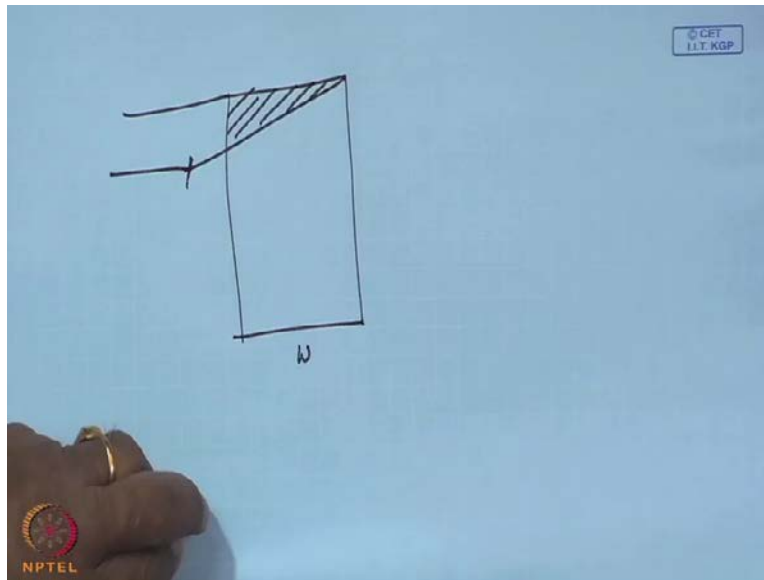
So, now you can have that shading factor just to distinguish between our a solar load fraction and this is actually I stands for illuminated area it can be short term like an hour or a long term over a period of one month or a day. So, we have also described in the last class the types of shadows that can be formed the overhang in general is at least the width of the window where H_w is height this could be the projection p . So, this without showing the clumsy way that is a shadow right when the sun is in front of it like this shaded this is only to recapitulate.

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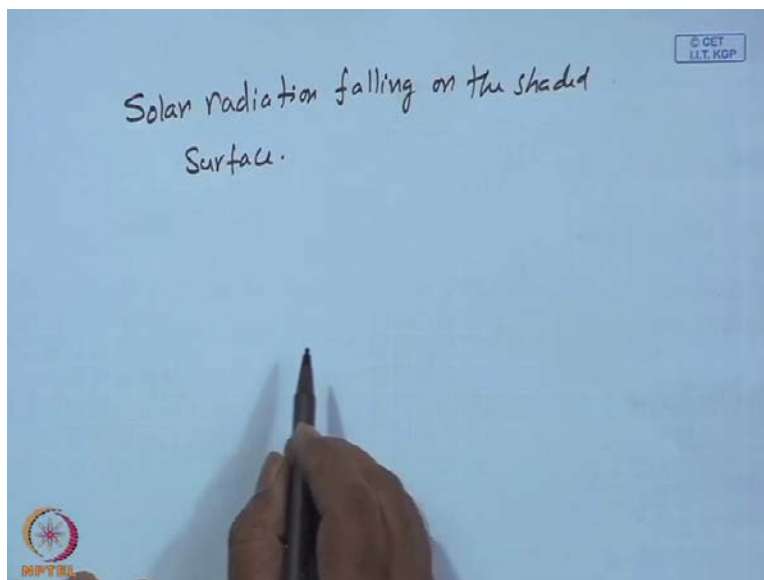
What we did earlier and to more to emphasize the complexity involved in calculating the shading factor though it is very easy to understand that the projection will cast shadow. And it could be like this is the shaded area it is not the overhang but the shadow shape goes beyond the window. And I can have a degenerate case that this line shall be up to here and then proceeds we are not really interested in what happens further. So, this a triangular shape where the end of it edge of it just coincides with the edge of the window.

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And the third last could be it may go like this. So, looks triangular but the again it becomes horizontal beyond the window width w . So, it is a complex thing it depends upon the time of the day of course then the location the day of the year.

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So what is it we want to do is solar radiation falling on the shaded surface. Whatever I have illustrated are also true for the wing wall.

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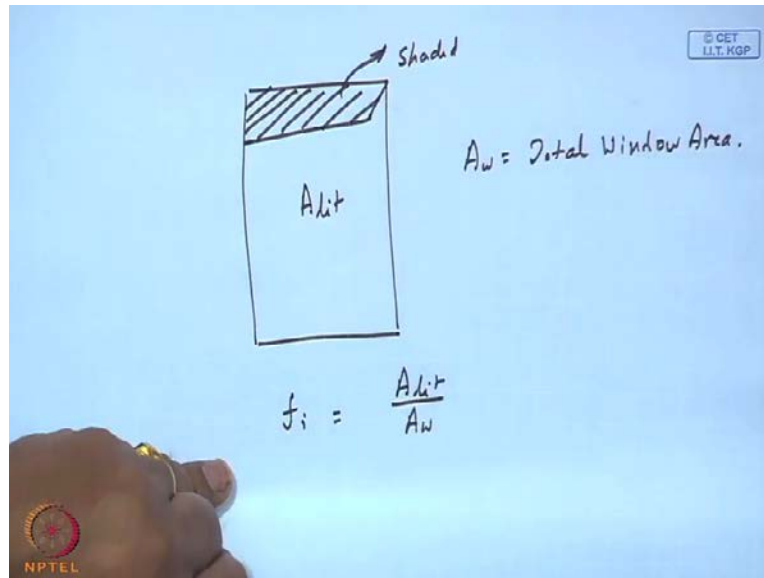
The procedure simply involves estimating the solar radiation falling on an unshaded surface and multiplying the value with a 'shading factor'.

Shading factor can be defined as the ratio of the lit area of the surface by the total area of the surface.



If this is the window I may have a wing wall like this and another one like this. So, if tentatively I assume this is south and this is east and hence this should be waste either this or this will cast shadow depending upon it is forenoon or the afternoon. So, the shading factor can be define as the ratio of the if you look at it like this I am interested in this part

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This is shaded and the remaining area is lit by the sun and A_w is the total window area. So, we might define f_i the instantaneous shading factor so this is what I tried to do it in terms of the figure that hatched portion represents the shadow and the now hatched one is the actual projection so this will be equal to a lit by A_w so this written in such a manner that actually it may be the instead of the shading factor it could be the lit factor if a lit is equal to A_w f_i is equal to one if f_i is equal to one that means the window is not shaded in f_i is equal to 0 it is completely shaded. So, if you want a long term ...

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The image shows a person's hands writing two equations on a light blue surface. The first equation is $\bar{f}_i = \frac{\int I_b R_b f_i d\omega}{\int I_b R_b d\omega}$. The second equation is $\bar{R}_b = \frac{\int I_b R_b d\omega}{\int I_b d\omega}$. In the top right corner, there is a small logo that says '© CET I.I.T. KGP'. In the bottom left corner, there is a logo for NPTEL.

You can always have \bar{f}_i integral $I_b R_b f_i d\omega$ upon $\int I_b R_b d\omega$ just like we have defined your \bar{R}_b as integral $I_b R_b d\omega$ by $\int I_b d\omega$ this is the total amount of solar radiation falling on re-collector which is shaded by factor with changes with time by the total solar direct radiation that is like to fall on the window or the surface if there has been no shading.

So, the shapes we have already described it could be triangle rectangle or trapezoidal. So, this is the equation which I have already written if \bar{f}_i now both the numerator and the denominator will be from apparent sun rise to apparent sun set angles relevant to the particular window under consideration.

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$$I_T A_w = I_b R_b A_{lit} + I_d \left(\frac{1 + \cos \beta}{2} \right) A_w + \rho I \left(\frac{1 - \cos \beta}{2} \right) A_w$$

$\beta \approx 90^\circ$ in general

$$I_T = I_b R_b \frac{A_{lit}}{A_w} + I_d \left(\frac{1 + \cos \beta}{2} \right) + \rho I \left(\frac{1 - \cos \beta}{2} \right)$$
$$= I_b R_b f_i + I_d \left(\frac{1 + \cos \beta}{2} \right) + \rho I \left(\frac{1 - \cos \beta}{2} \right)$$

So if I try to write the solar radiation received by the window per unit area of the window so I_T into A_w is the total quantity of the solar radiation that the window is receiving should be equal to $I_b R_b$ multiplied by only the A_{lit} because the beam radiation does not fall on the shaded area times the diffused radiation $1 + \cos \beta$ by 2 times A_w plus ρ ground reflectance multiplied by I into $1 - \cos \beta$ by 2 into A_w where β in general equal to 90 degrees not approximately let me put it this way in general but it's not the essential that β be 90 there are quite a few architectural buildings where the window or the class frames or not yet 90 degrees they are at a particular angle. So, if I try to calculate I_T per unit area of the window that will be equal to $I_b R_b \frac{A_{lit}}{A_w}$ plus the diffuse component plus the ground reflected component.

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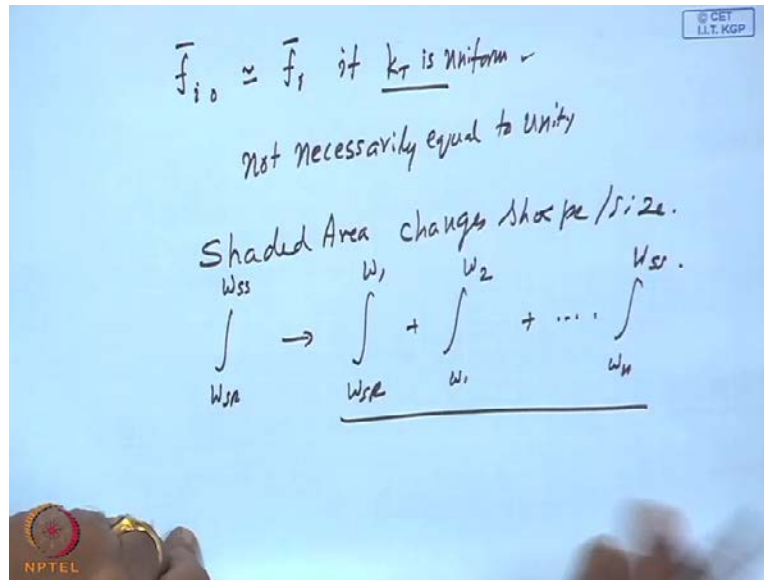
$$H_T = H_b \bar{R}_b \bar{f}_i + H_A \left(\frac{1 + \cos \beta}{2} \right) + \rho H \left(\frac{1 - \cos \beta}{2} \right)$$

$$\bar{f}_{i0} = \frac{\int_{\omega_{sR}}^{\omega_{sS}} G_{0R} R_b f_i d\omega}{\int_{\omega_{sR}}^{\omega_{sS}} G_{0R} R_b d\omega}$$

$$G_{0R} = G_{0n} \cos \theta_z$$

So, this we shall call it $I_b R_b f_i$ the shading factor plus these are very familiar terms for us should be by now. So, that is it here yeah I have dived throughout by A_w so, this is if I extend this just like we have done it for the hmm just simple radiation un-shaded. H_T should be equal to $H_b R_b \bar{f}_i$ it is something like absorbed radiation except that this is a shade impact times the diffused radiation plus the ground reflected radiation. So, under extra terrestrial calculations just like we have done for R_b bar. So, which I will indicate by suffix additional o will be ω_{sR} to ω_{sS} $G_{0R} R_b f_i d\omega$ upon ω_{sR} ω_{sS} $G_{0R} R_b d\omega$ right. So, G_0 is something like G_0 we know equal to $G_{0n} \cos \theta_z$ right that analytical expression is known and still we don't know f_i though R_b is known for us.

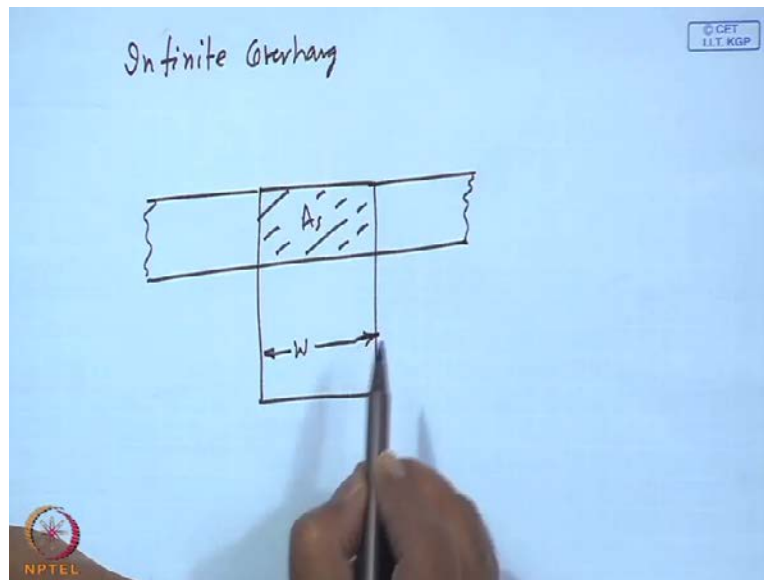
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So, this \bar{f}_{i0} will be if very close to \bar{f}_i if k_T is uniform not necessarily equal to unity. This we have proved in the case of R_b looking at the success why the terrestrial calculation is yielding sufficiently accurate results as the extra terrestrial calculation the other way around extra terrestrial assumption is good enough for the terrestrial conditions also and we found that if k_T not necessarily be equal to unity but if it is uniform I will be quite acceptable and it will be exactly equal to the calculations we made under extra terrestrial conditions. Right and k_T is more or less uniform when the solar radiation is high in general let us say 10 to 2 p m consequently this will be acceptable as a good approximation. Now you have the problem of that shaded area changes shape and of course size.

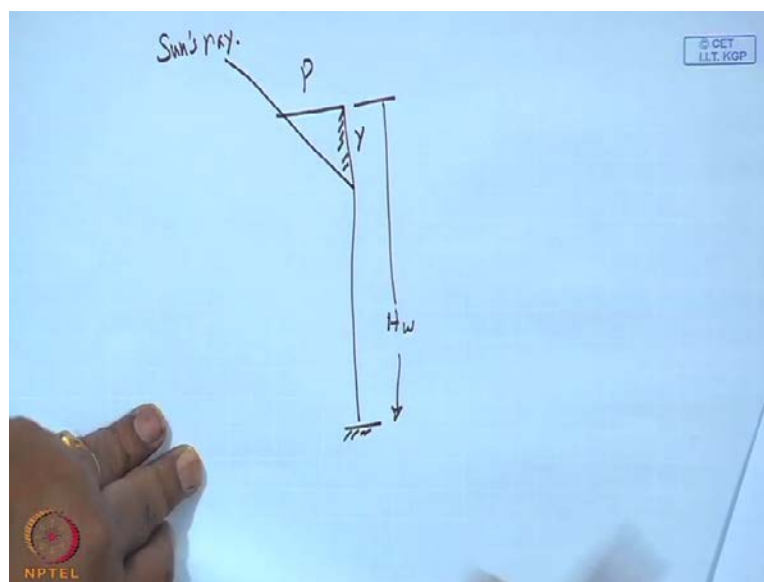
So, that in other word this so called ω_{sR} to ω_{sS} may have to be split up into ω_{sR} ω_1 plus ω_1 to ω_2 plus ω_n to ω_{sS} . So, it keeps changing from rectangle to trapezium to triangle just truncating at the edge of the window and going beyond. So, this is a little complicated issue and we need a thorough perfect algorithm to find out the area. On that and if your windows are not vertical if they are at an angle the problem is even more compounded.

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But, if you have an infinite overhang as I have shown over here. So, this may be 2 to 5 times the window the shaded area A_s is all ways a rectangle. So, this gives us some respite. So, this I think something wrong with the screen

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See if I show this in the side view this is the projection p and you have got H of the window height over a certain level and then this is the sun's ray. So, you have got a y it is not that it is uniform throughout. But, nevertheless because this sun's ray could be towards me away but in the projection looks like a line it could be a pencil or in other words moving like this to like this. So, consequently how much is the lit area will depend upon the time of the day and the position of the sun.

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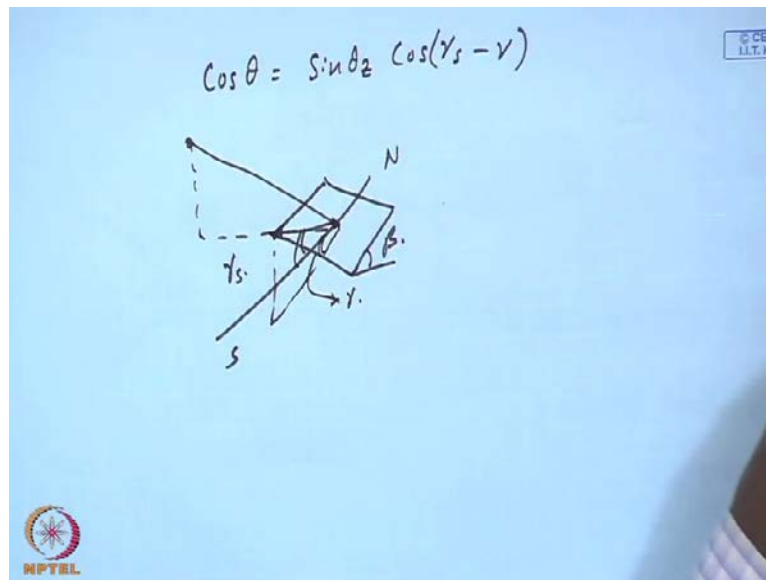
$A_s = YW$
 if the overhang is infinite.

$$Y = \frac{P}{\tan \theta_z \cos(\gamma_s - \gamma)} = \frac{P \cos \theta_z}{\sin \theta_z \cos(\gamma_s - \gamma)}$$

$\gamma_s =$ solar azimuthal angle
 $\gamma \rightarrow$ azimuthal angle.

A_s will be y into w if the overhang is infinite. So, it is a rectangle no matter how much more than the width of the window it is going to have and that you can write y will be equal to the projection p upon $\tan \theta_z \cos \gamma_s$ minus γ I shall explain which you can easily find out figure out from the trigonometry $p \cos \theta_z$ because this is $\sin \theta_z$ by $\cos \theta_z$ goes up. So, this is your $\sin \theta_z$ into $\cos \gamma_s$ minus γ . Where γ_s is the solar azimuthal angle. We have recall introduced the azimuthal angle for the surface as a angle between the north south axis and the projection of the outer normal to the surface on the horizontal plane whatever is the angle that.

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So, similarly I can take the sun's ray and its projection on the horizontal plane and that shall be your solar azimuthal angle. Which I think can be easily shown your angle of incidence $\cos \theta$ is related to $\sin \theta_z$ times $\cos \gamma_s - \gamma$. I think the next picture should be you have got the tilted surface with an angle β and the sun's rays coming something like this if I take the projection of the sun's ray and if this is your south north then this should be your γ_s . Whereas we have taken the out projection of the surface and this we defined as γ . So, you can the same picture is show over here where it looks like a α but that should be γ it's a γ_s R_s is γ_s that is the sun's azimuthal angle. So, my shaded area for the rectangular shape because the overhang is infinitely long.

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$$A_s = \frac{P W \cos \theta_z}{\cos \theta}$$
$$f_i = 1 - \frac{A_s}{A_w} = 1 - \frac{P \cos \theta_z}{H_w \cos \theta}$$
$$= 1 - \frac{\tan \psi}{R_b}$$

P w simple trigonometry upon cos theta. So, my f i is 1 minus a s upon A w equal to 1 minus p cos theta z by H w cos theta. Because, A w is H w into p so that is what you will get a s is equal p into whatever is y equal to one minus tan si by R b. Because, cos theta by cos theta z is nothing but R b and p by H w of the window is nothing but a tan psi where that angle size shown this is the sun's ray sun this is the projection this is y and this is H w and if I draw a line like this will be psi.

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$$\bar{f}_{i\infty} = \frac{\int_{\omega_s}^{\omega_s} I_b R_b \left[1 - \frac{\tan \psi}{R_b} \right] d\omega}{\int_{\omega_s}^{\omega_s} I_b R_b d\omega}$$

$$= \frac{\int_{\omega_s}^{\omega_s} I_b [R_b - \tan \psi] d\omega}{\int_{\omega_s}^{\omega_s} I_b R_b d\omega}$$

So, to indicate that it is for an infinitely long overhang... So, we $\bar{f}_{i\infty}$ equal to integral ω_s R_b ω_s $I_b R_b$ times $f_{i\infty} - \tan \psi$ by R_b $d\omega$ upon the total radiation $\int_{\omega_s}^{\omega_s} I_b R_b d\omega$. Which shall be ω_s R_b ω_s I_b times $R_b - \tan \psi$ $d\omega$ by integral $\int_{\omega_s}^{\omega_s} I_b R_b d\omega$ in the limits ω_s R_b to this we have done number of times and R_b size fixed for a given geometry. So, consequently it is not difficult to analytically evaluate this expression. Which has been done only thing is the assumption is that the overhang is infinite long.

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$$I_b R_b f_i = I_b [R_b - \tan \psi]$$

$$= I_b \left[\frac{A + B \cos \omega + C \sin \omega}{\cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta} - \frac{\sin \psi}{\cos \psi} \right]$$

$$I_b [R_b - \tan \psi] = \frac{I_b}{\cos \psi} \left[\frac{A^* + B^* \cos \omega + C^* \sin \omega}{\cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta} \right]$$

$$\beta^* = \beta + \psi$$

$$A^* = \sin \delta (\sin \phi \cos \beta^* - \cos \phi \sin \beta^* \cos \gamma)$$

$$B^* = \cos \delta (\cos \phi \cos \beta^* + \sin \phi \sin \beta^* \cos \gamma)$$

So, you have got $I_b R_b f_i$ is $I_b R_b$ minus $\tan \psi$ which shall be I_b times in general $a + b \cos \omega + c \sin \omega$ it need not be south facing by $\cos \theta z \cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta$ minus $\sin \psi$ by $\cos \psi$.

So, what I can do is I_b times R_b minus $\tan \psi$ that is what you have here should be equal to I_b by $\cos \psi$ times $a^* + b^* \cos \omega + c^* \sin \omega$. But, it is not difficult I am re-writing $\sin \omega$ upon your $\cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta$. So, β^* is $\beta + \psi$ and a^* is same as you are $A B C$ except that β is equal to β^* you recall. The fundamental definition $\sin \delta$ times when we expressed $\cos \theta$ is $a \cos \omega + b \sin \omega$ and that is what we have done here $\sin \phi \cos \beta^* - \cos \phi \sin \beta^* \cos \gamma$. And here I am somewhat doing little faster than what I have done so far because by now you should be similar with the angles and this is nothing but just mathematical manipulation. So, we start with the equation put $a \cos \theta \cos \phi \cos \delta \cos \omega + \sin \phi \sin \delta$ etcetera.

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$$C^* = \cos \delta \sin \beta^d \sin \gamma^d \leftarrow$$

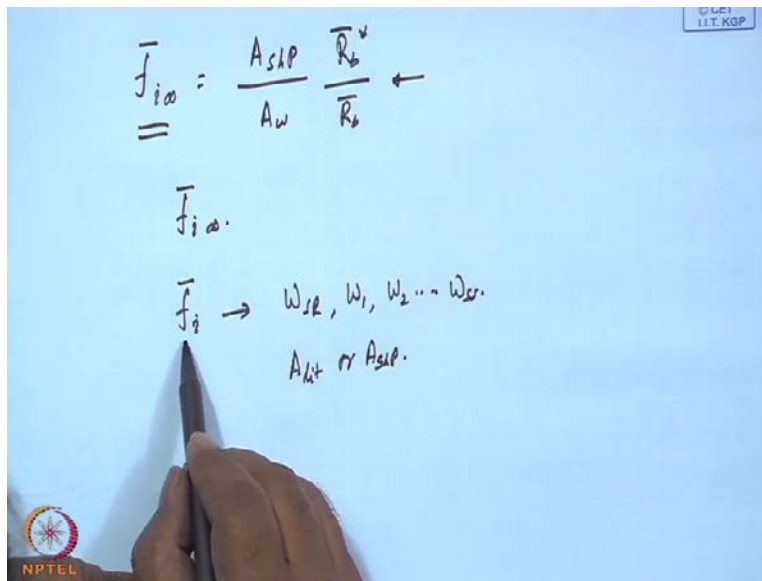
$$I_b [R_b - \tan \psi] = \frac{I_d}{\cos \psi} \cdot \frac{\cos \theta^d}{\cos \theta_z} = \frac{I_b}{\cos \psi} R_b^d$$

$R_b^d \rightarrow$ tilt factor for the "shading plane"

You will get this result and the final answer will be so simple you really don't have to calculate all these things. But, this shows the basis I have put it in terms of a star b star c star where your slope is not beta but beta plus psi that is the whole idea and you have got I_b times R_b minus $\tan \psi$ from the previous equation I_b by $\cos \psi$ $\cos \psi$ is that angle you remember that $\cos \theta^d$ by $\cos \theta_z$ which will be equal to I_b by $\cos \psi$ times R_b star. So, this R_b star is the tilt factor for the what we call the shading plane. If this is an overhang this is the window this will be the $A_s H_p$ the. So, called shading plane. Right it is nothing to not the sun's ray casting a shadow just draw the tip of the projection to the base of the window you will get the shading plane.

The whole idea physically is whatever is the radiation entering through this will reach the window. So, you estimate the solar radiation based upon $A_s H_p$ or the area of the shading plane that if it is converted back into the per unit area of the window you have your answer.

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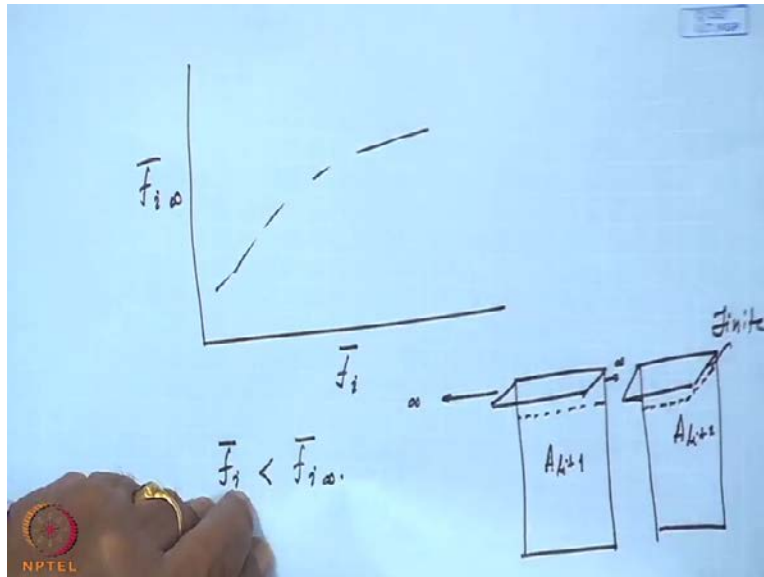


So, this $\bar{f}_{i\infty}$ is one by $\cos \psi$ integral $\int \int \frac{R_b^v}{R_b} d\omega$ by integral $\int \int \cos \psi d\omega$. And where your $\cos \psi$ is nothing but the height of the window by the diagonal p squared plus H^2 squared. Which is nothing but the area of the window by area of the shading plane. A_{shp} right. So, that is what I have shown in this picture the sun's rays will hit the window at some y distance away total height of the window is w and the angle subtended between the projected projection and the base of the window is the shading plane of the area is A_{shp} which can be given in terms of the geometry p and H and w . So, this you can write it as a shading plane by $A_w \bar{R}_b^v$ star upon \bar{R}_b . So, in another words the concept of the shading plane or the shaded area has been brought into the average daily or monthly average daily shading factor $\bar{f}_{i\infty}$ which should be the ratio of the shading plane to the window area which is purely geometry. And \bar{R}_b^v will represent the how long the projection is and what is the height of the this thing it will window and \bar{R}_b is for the simple window.

So, with this you can calculate your $\bar{f}_{i\infty}$. And if you want to calculate \bar{f}_i I have already mention the problem of integrating between ω_1 to ω_2 we don not know how many up to ω_s these ψ 's. And then the corresponding

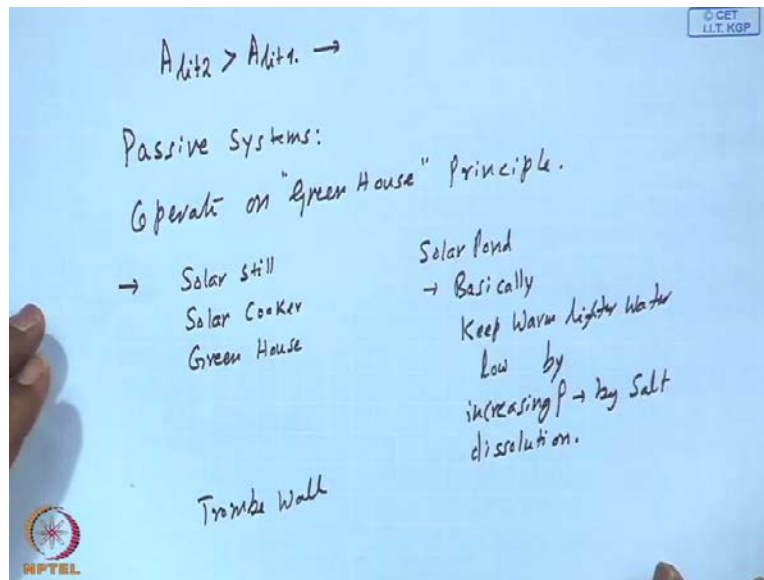
a lit or a s H p. It will depend upon the shape of the shadow on the window. So, this is a little tricky business so what people have done particularly the work at I i T kharagpur.

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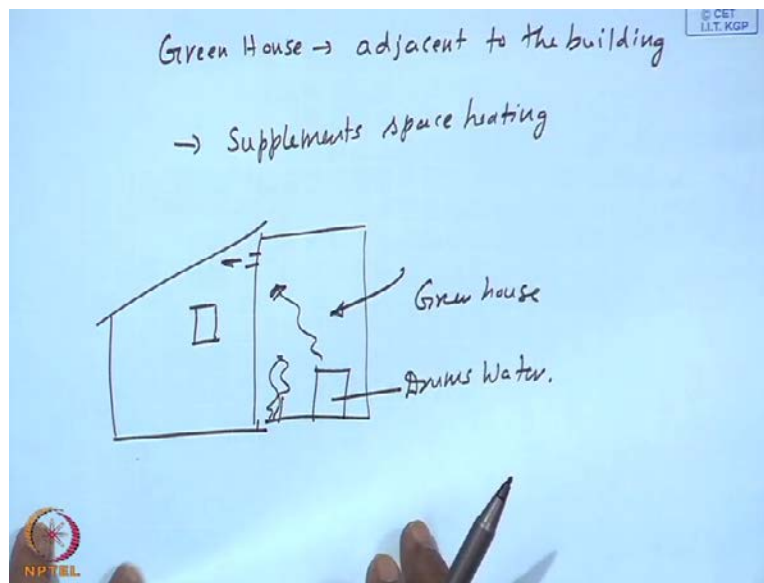
Calculate numerically. This \bar{f}_i versus $\bar{f}_{i\infty}$ some curve will be there I don not know whether it is increasing or decreasing. But, we know that \bar{f}_i should be less then $\bar{f}_{i\infty}$. When the projection is infinitely long it is a complete rectangle or the height or the rather the line. So, it may be rectangular or it may not be rectangular as shown over here. So, but nevertheless this area a lit and a lit one and two. So, this I will say infinity infinity and this is finite

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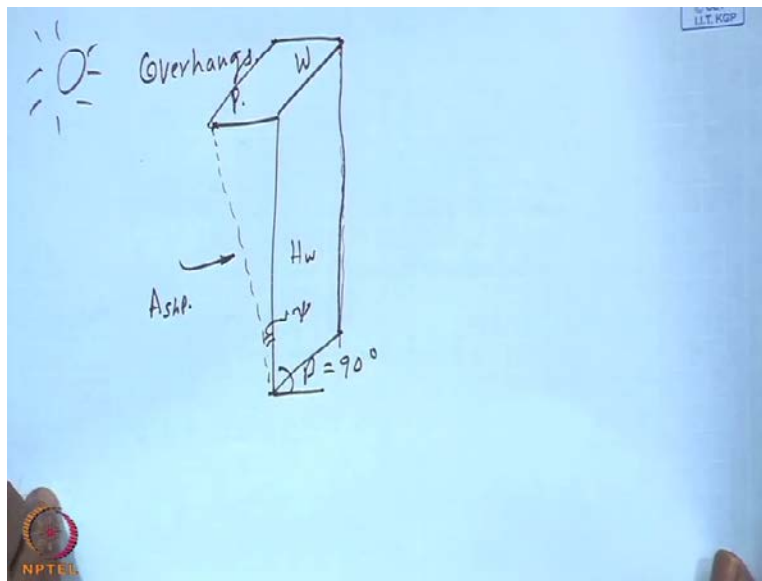
So, a lit two is always greater than a lit one. So, in one sense my shading factor here will be under estimated or rather than over estimated it assumes that more area is covered or rather than the less area. So, that is about it. So, in a nut shell when we are talking about the passive systems most of the operate on green house principal. You let in the solar radiation but let the not emitted radiation at a wave length larger longer it will not escape. Right it could be a solar steel or a solar cooker or the traditional green house itself of course the solar pond comes under different category it is not the green house principal. So, this is basically keeps warm lighter water low by increasing the density by salt dissolution. Then you have got something like a trombe wall. Which is basically a hollow wall where they return air from the room will be circulated and heated by the exposed sun's rays.

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And then your green house can be adjacent to the building, which supports supplements rather space heating. So, you may have a small thing out let over here to the plants or whatever drums of water, which will gain heat during the day will release during the night keeping the room or the house attached house warmer. So, this is a standard practice or you can have a little garden in the winter months it does not die out and you will also have some space heating by this mechanism.

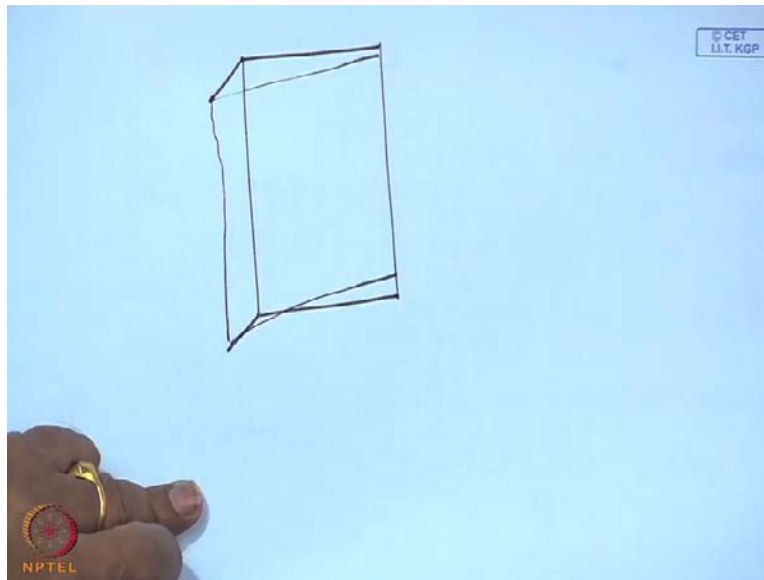
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Then we consider the importance's of overhangs in a nut shell you can calculate the radiation received by a window of height H_w and width w through a overhang of projection p by calculating radiation entering through the shading plane defined as the plane between the tip of the projection to the base of the window. This can be a solid line. So, this is what these and sun is somewhere here.

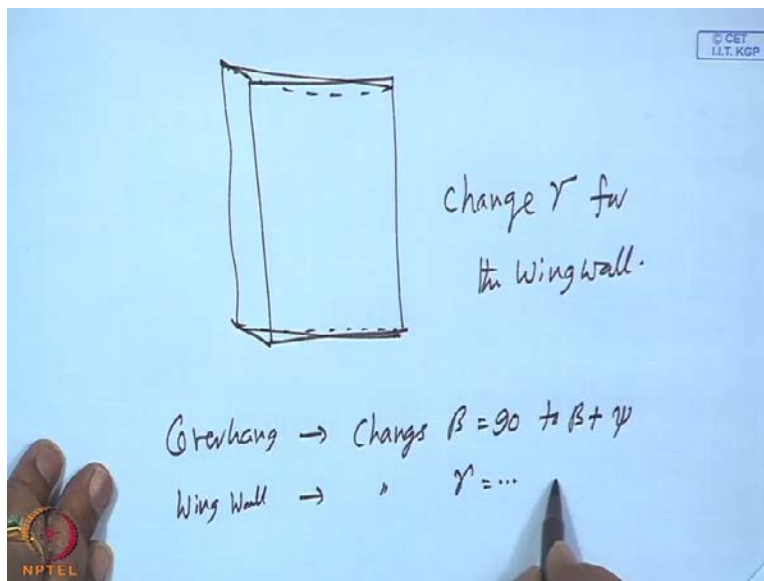
So, your R_b concept and $R_{b\bar{}}$ concept can be extended of course generally this is β is equal to 90 degrees and this is your ψ the additional angle. So, essentially it is a surface tilted with 90 plus ψ or β plus ψ in general and you calculate whatever is the radiation falling through this it will reach the window.

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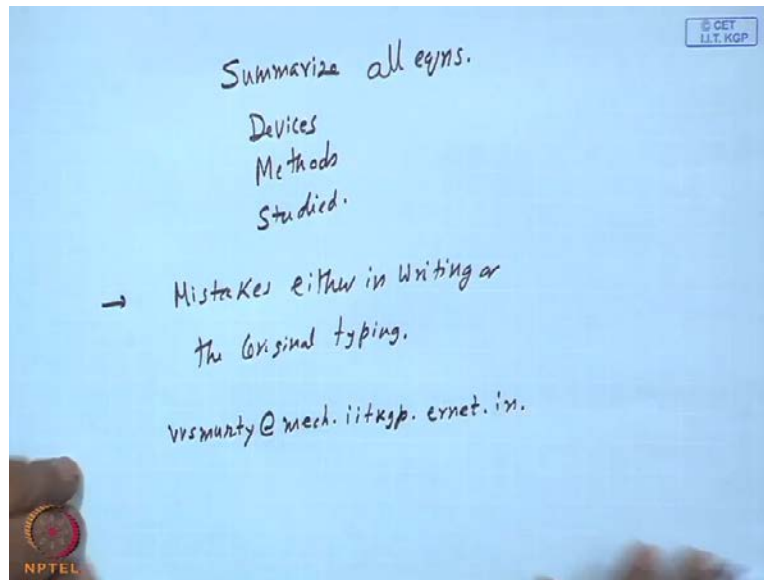
We did not do much about the wing walls that is what I was but you can expect and it has been established if this is the wing wall you make the shading plane from here to the other side of the window. In other words you have a I do not know whether the sketch is giving the impression it should be the other way round perhaps.

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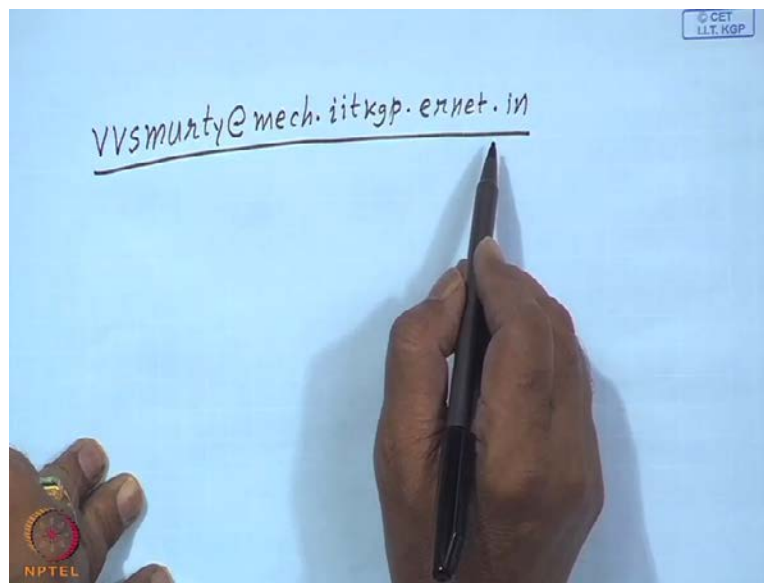
Let me try so, from here you join so this will from the shading plane in the case of a wing wall. So, you can say the same thing in other words you change γ for the wing wall. Essentially you can summarize overhang changes β and the wing wall changes γ equal to whatever it is to some γ dashed which you can easily calculate because you know the projection of the wing wall and width of the window. So, this is what we have achieved in terms of the what shall we say the passive systems.

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So, what we shall do in the next lecture is I will try to summarize all our equations and the devices and the methods we have studied. And one thing you should remember is this could be the topic wise the last lecture the next one will be the summary only. There could be some mistakes either in writing or original typing. So, what I would suggest is in case you find a mistake contact me immediately at your earliest at my email address v v s murty at mech dot I I T dot I I T K G P dot ernet dot in I shall rewrite it in bigger letters.

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So, you can send a email to this address which your specific query and in case there is you find that some formula or some sign is wrong or something like that. Or this not a coaching attempt in other words I will not solve your problems for you I may indicate how you can solve a problem. If when if you write to me with the correct data etcetera and having done your home work but nevertheless the I have to take the responsibility. If there are some mistake either in quickly writing on the paper or in my original cut and paste of from my class notes. So, for that I am answerable and I shall answer you may be if not twenty four hours within forty eight hour.

So, please make use of this and that is the best way I thing we can improve the material and make the corrections where ever they are there and of course one of my professors use to say that he will give a dollar for every mistake but I do not make any such promise because I am likely to go bankrupt if all of you claim a dollar reach for each mistake. So, the feel free to write to me and thus one way I can help you and you help me in correcting if these are any mistakes or also try to present in a alternate manner in case you have got a confusion that will help in the long term for teaching of this course to the future

students thank you very much. And next we shall go to the summary of all what we have done. Thank you.