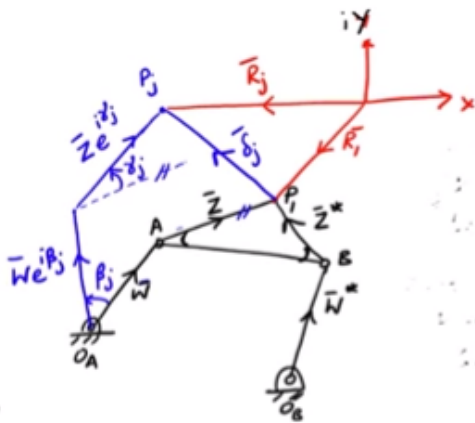


**Theory of Mechanisms**

**Lecture 16**

**Dyad Form Synthesis: Motion Generation**

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$$\bar{W}e^{i\beta_j} + \bar{Z}e^{i\beta_j} - R_j + R_j - \bar{Z} - \bar{W} = 0$$

$$\bar{W}(e^{i\beta_j} - 1) + \bar{Z}(e^{i\beta_j} - 1) = \bar{R}_j - \bar{R}_1 = \bar{\delta}_j$$

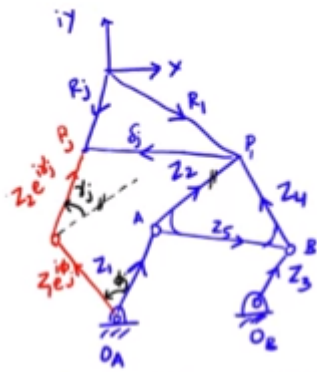
$$\bar{W}(e^{i\beta_j} - 1) + \bar{Z}(e^{i\beta_j} - 1) = \bar{\delta}_j$$

Standard or dyad form equation

$$W(e^{i\beta_j} - 1) + Z(e^{i\beta_j} - 1) = \delta_j$$

Okay, so last class we were looking at the dyad or the standard form for these, this is called the standard form for the synthesis equation using complex numbers, and essentially we say that a four-bar can be represented as two dyads, and we looked at just one side of the dyad right, and I'll probably skip using the bar. You know from now on it's understood that if I write this okay, this is understood that these are vectors or complex numbers. The reason I want to avoid using the bar is, in complex numbers, the bar indicates the conjugated, so I don't want confusion with that. The textbook, they can make it bold, but you know, but in the context of what we are doing you should know that this is a vector equation, so it's an equation, its two scalar equations and this is called the dyad or the standard form. So how do we apply this to a four bar? That's what we will look at today and then the different types of synthesis problems that we have seen.

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4-bar linkage seen as two dyads

$Z_1, Z_2$  and  $Z_3, Z_4$   
 left right

Path point P moves along a path from position  $P_1$  to  $P_j$  defined by  $R_1$  &  $R_j$ , resp.

Prescribed two positions :  $R_1, R_j, \phi_j, \gamma_j$

$$Z_1 e^{i\phi_j} + Z_2 e^{i\gamma_j} - R_j + R_1 - Z_2 - Z_1 = 0$$

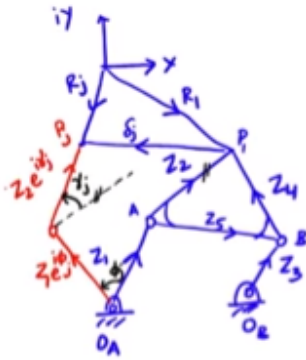
$$Z_1 (e^{i\phi_j} - 1) + Z_2 (e^{i\gamma_j} - 1) = R_j - R_1 = \delta_j$$

$j \geq 2$

So let's say a four bar is represented by two dyads. I say this is  $Z_1$ . This is  $Z_2$ . This is  $Z_3$ . And  $Z_4$  is a point P, and this coupler okay? I can, once I know  $Z_1, Z_2, Z_3, Z_4$ , then this  $Z_5$  can be expressed in terms of the other two. It's nothing but  $Z_2$  minus  $Z_4$ . If this is  $Z_5$  right, so the four bar linkage is seen as two dyads,  $Z_1, Z_2$ , and  $Z_3, Z_4$ . So let's say the point P from the first position, it moves to some other point. Let me draw the coordinate system.  $iy$ , so I have, this is  $R_1$  and then at some other  $J$ th position point P, so let's say this moves by an angle  $\Phi_j$ , draw that. That means like that, and so this, so this is being the first position, this will be in the  $J$ th position and if this, this is them, so these two are parallel okay? So let's say this has rotated by  $\gamma_j$ , this has rotated by  $\Phi_j$ , so this one here, the red one, this vector is  $Z_1 e^{i\Phi_j}$ , this vector is  $Z_2 e^{i\gamma_j}$  and this is  $P_j$ , then this is  $R_j$ , go A,B, OA,OB So  $z_1, z_2$  form the left dyad. This is the right side of the four bar  $Z_3$  and  $Z_4$ . So the point P on the part on the coupler path, the path point P moves along some path from position  $P_1$  to  $P_j$ . The positions are defined by  $R_1$  and  $R_j$  respectively. So that means we have prescribed two positions here. So if you have the case where two positions are prescribed, which means, I know  $R_1, R_j, \Phi_j$ , and  $\gamma_j$ , well, I don't necessarily know all of them. Let's say, okay, these are the quantities that I require okay? So based on this, so now I can write like we did when we derived the standard form. I'll just write down the loop closure equation for this loop here. So I have  $Z_1 e^{i\Phi_j} + Z_2 e^{i\gamma_j} - R_j + R_1 - Z_2 - Z_1 = 0$ . So all these are vectors okay, or I have  $Z_1 (e^{i\Phi_j} - 1) + Z_2 (e^{i\gamma_j} - 1) = R_j - R_1$ , which is nothing but  $\Delta_j$ . That is  $\Delta_j$  okay, so this is how we got the standard form  $j \geq 2$ . Now let's look at the case of motion generation okay?

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Motion generation :  $R_1, \dots, R_j$  or  $\delta_2, \dots, \delta_j$  prescribed  
 $\gamma_2, \dots, \gamma_j$  prescribed



# of positions	# of scalar eqns	Unknowns	# of scalar unknowns	# free choices	# solutions for unknowns
2	2	$Z_1, Z_2, \phi_2$	5	3	$\infty^3$
3	4	" + $\phi_3$	6	2	$\infty^2$
4	6	" + $\phi_4$	7	1	$\infty$
5	8	" + $\phi_5$	8	0	finite

$$Z_1(e^{i\phi_j} - 1) + Z_2(e^{i\gamma_j} - 1) = \delta_j \quad j \geq 2$$

For right-side dyad,  
 $Z_3(e^{i\psi_j} - 1) + Z_4(e^{i\gamma_j} - 1) = \delta_j$

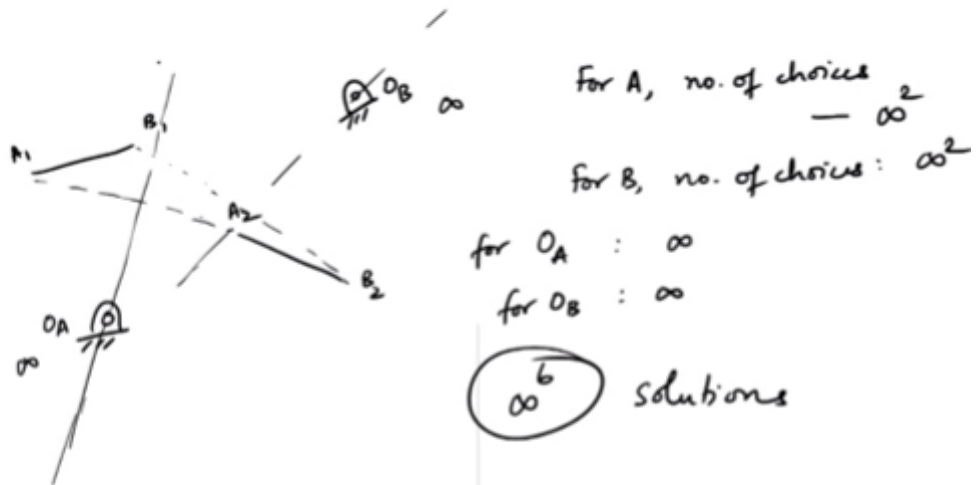
2-ppm  
 $Z_1(e^{i\phi_2} - 1) + Z_2(e^{i\gamma_2} - 1) = \delta_2$

3-ppm  
 $Z_1(e^{i\phi_3} - 1) + Z_2(e^{i\gamma_3} - 1) = \delta_3$

So I have the equation, the standard form  $Z_1, e^{i\phi_j} - 1$ , plus  $Z_2, e^{i\gamma_j} - 1$ , equal to  $\delta_j$  okay? This is my standard form equation for the left dyad. Now let me look at the case for motion generation, let me see whether I should do this okay, so for motion generation, what would be the quantities that would have to be prescribed? You need the location of a point on the coupler and you need the orientation of the coupler. Those are the two things for motion generation, so I need  $R_1$  to  $R_j$  depending on the number of positions they should be given okay? Similarly  $\gamma_1$ , the orientations, corresponding orientations of the coupler are also given. So if I am given, so if I'm given these two, then the synthesis I have to perform is form a motion generation problem, okay? That's what I am trying to find. I need to find the vectors which will give me this, which will solve this motion generation problem. So anyway, when when we write it okay,  $\gamma$  is  $J$  is greater than or equal to 2. It's always with respect to, so I should say yeah,  $\gamma_2$  - you will need  $R_1$  because you will, you use  $\delta_2$  to determine from the first position, but  $J$  greater than or equal to 2 means,  $\gamma$  is always from the first position okay? So let's say, let's make a table where I have number of positions, then number of scalar equations for the dyad. It's actually, this will be  $\gamma_2$  to  $\gamma_j$ , yeah, number of scalar equations and then the unknowns, the scalar unknowns, or first we look at the vector unknowns, then the number of scalar unknowns. Number of free choices scalars and then number of solutions for the unknowns, okay? So you can also look at this as  $R_1$  to  $R_j$ , prescribed or  $\delta_2$  to  $\delta_j$  prescribed okay? the displacements of that and  $\gamma_2$  corresponding orientations. So let's say it's a two position problem, that we are trying to solve. We know this and we know that, so how many scalar equations? So if I write the standard form, okay my  $j$  is two position problem. I have position 1 and position 2, so the equations that I get will be, for the two position problem, I have  $e^{i\phi_2} - 1$ , plus  $Z_2, e^{i\gamma_2} - 1$  equal to  $\delta_2$ , are there any other equations? It's a two position problem. I get this, a single vector equation which corresponds to, two scalar equations, what are my unknowns? I have  $Z_1, Z_2$ , okay? In this equation  $\gamma_2$  is given,  $\delta_2$  is given, because that's my design condition. I don't know  $Z_1, I$

don't know  $Z_2$ , I don't know  $\Phi_2$  okay? So of these  $Z_1$  and  $Z_2$  are vectors or complex numbers. So I need, so if I look at the number of scalar unknowns I have 5. I have two equations, five scalar unknowns, so how many free choices do I have? Three, the number of free choices is three, which means number of solutions that I have is infinity okay? Take three positions. Now what happens? I have this equation, I have in addition to that I also have this plus, I mean I'm using plus rather loosely here, but I have that equation. I will also have this equation for the third position here. What are the specified quantities?  $\Gamma_2$ ,  $\Gamma_3$ , and  $\Delta_2$ ,  $\Delta_3$ , that's my three position problem. 3 position motion generation problem okay? So here now I will have number of scalar equations becomes four, unknowns,  $Z_1$ ,  $Z_2$ . So I have all these. Basically these three are unknown, so I'll just put a little plus in addition to that. What else is unknown?  $\Phi_3$ ,  $\Phi_3$  is the only other unknown because again  $\Gamma_2$ ,  $\Gamma_3$ ,  $\Delta_2$ ,  $\Delta_3$ , are given, so the number of scalar unknowns is now 6. My number of free choices come down to 2 and I have infinity square solutions that are possible for position scalar equations. One more the equations go up by two, I have six. The unknowns, all these data plus five, four okay? So this is seven number of free choices goes down to one and I have an infinity of solutions. Five positions, this goes up to eight, this goes up to eight again okay? So I am no longer left with any free choices and we say there are a finite number of solutions okay? Not necessarily a unique solution, you would have a finite number of solutions, you don't have an infinite. I will see later when we do that, this is only for one dyad we are talking about, only one side of the four bar right? For the other side of the four bar you again have for the right side dyad,  $Z_3 e^{i\theta}$ , let's say the angle is,  $\theta$ , like we've been using plus,  $Z \Phi e^{i\theta}$ , What would be the power  $Z_4 e^{i\theta}$ ? What would be the angle of  $Z_4$ ? you're trying to form a four bar? It'll still be  $\Gamma$ , that is what links the two Dyads are linked together because  $Z_2$  and  $Z_4$  are going to be part of the same rigid body and they're going to undergo the same rotation. That's how you're building the 4 bar, with this dyad form, so  $e^{i\theta}$ ,  $\Gamma J - 1$  and it's still the same point P equals  $\Delta J$  okay? So here the unknown, so I can write, make a similar table like this okay, and in those cases instead of file it's going to be safe, otherwise the form stays the same, that's why it's called the standard form okay? So so this gives me what for, if I want to create a 4 bar with these two dyads it's infinity cube for one dyad. This one also, it has the same form, so, another infinity for a two-position problem right? So I get infinity cube infinity cube. I can, so it's infinity to the power 6. Now go back to our graphical synthesis that we did okay, and see if it is, if you got the same result there. What did we do with the graphical synthesis?

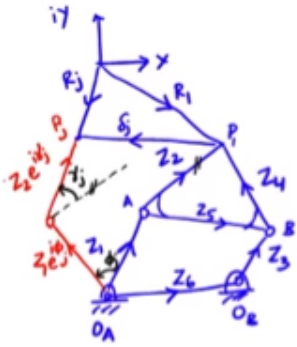
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So you had two positions  $a_1, b_1, a_2, b_2$ , right, and then how, what did I do? I just took the perpendicular bisector of  $a_1, a_2$  okay, and I picked  $O_A$  anywhere on that perpendicular bisector, so that gave me how many solutions infinity for  $b_1, b_2$ ? Pick the perpendicular bisector, I can pick  $O_B$ , anywhere on the perpendicular bisector, that gives me how many solutions? Infinity, so total number of solutions for my 4 bar? yeah, so this is infinity square after I have picked  $A$  and  $B$  to be the moving pivots. It's not necessary, so I have for  $A$  number of choices. I can pick any point in the plane number of choices is infinity square, for  $B$  number of choices is infinity square. Once I picked my  $A$  and  $B$ , I still have infinity into infinity, infinity square, So for  $O_A$  and  $O_B$ , for  $O_A$  infinity, for  $O_B$  infinity. So overall I again have infinity to the power 6 solutions. Got the 2 position, so it does not change okay? The number of solutions that are possible does not change. What may be restrictive is how you can find the solutions because if I'm working, you know if I'm trying to do geometry like for the three position problem we ended up with a unique solution right? Although this tells me here that I would have more,

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Motion generation :  $R_1, \dots, R_j$  or  $\delta_2 \dots \delta_j$  prescribed  
 $\delta_2, \dots, \delta_j$  prescribed



$$Z_1(e^{i\phi_j} - 1) + Z_2(e^{i\psi_j} - 1) = \delta_j \quad j \geq 2$$

$$\text{2-prim} \quad Z_1(e^{i\phi_2} - 1) + Z_2(e^{i\psi_2} - 1) = \delta_2$$

$$\text{3-prim} \quad Z_1(e^{i\phi_3} - 1) + Z_2(e^{i\psi_3} - 1) = \delta_3$$

# of positions	# of scalar eqns	Unknowns	# of scalar unknowns	# free choices	# solutions for unknowns
2	2	$Z_1, Z_2, \phi_2$	5	3	$\infty^3$
3	4	$" + \phi_3$	6	2	$\infty^2$
4	6	$" + \phi_4$	7	1	$\infty$
5	8	$" + \phi_5$	8	0	finite

For right-side dyad,  
 $Z_3(e^{i\psi_j} - 1) + Z_4(e^{i\chi_j} - 1) = \delta_j$

Coupler is given by  $Z_5 = Z_2 - Z_4$   
 Fixed link :  $Z_6 = Z_1 + Z_5 - Z_3$

I actually have infinity square choices for the 3 position problem, but because of the way that we do the construction and the way we choose, so when I choose a point I immediately lose two, three choices when we do it analytically. You will see I can possibly choose an angle or I can choose a length. Perhaps you know when we look at solving these equations that gives you more flexibility but the number of free choices does not change fundamentally. The problem will have that many number of free choices because you have so many equations, you have so many unknowns but the method that you use may restrict you in some ways to on what free choices you are allowed to be, okay, and you may have to pick free choices in pairs like as a point for instance, so then that becomes a little bit more restrictive. So it's, it's more the method that restricts the free choices then the problem still has that many number of possible solutions, okay? So that's something if you need to keep in mind okay? So once we solve the right side dyad, okay, then to create the 4-bar the coupler is given by selects. We will do it for a couple of problems. So the coupler is given by  $Z_5$  equal to  $Z_2$  minus  $Z_4$ , so once I solve  $Z_1, Z_2$ , then  $Z_3, Z_4$ , my coupler is given by  $Z_5$  equal to  $Z_2$  minus  $Z_4$  and fixed link will be  $Z_1$ , this will be  $Z_1$ , sorry, I should call it  $Z_6$ ,  $Z_6$ ,  $Z_1$  minus, sorry  $Z_1$  plus  $Z_5$ , minus  $Z_3$ . Just by the loop closure so that completely if I find these two dyads it completely defines my 4 bar. That's, that's the point I'm trying to make, so I can look at the 4 bar as these two separate dyads design, these two separate dyads, put them together to make my 4 bar.

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Synthesis for  
2-position motion generation

Given  $\vec{\delta}_2, \gamma_2$

$$\vec{Z}_1(e^{i\phi_2}) + \vec{Z}_2(e^{i\gamma_2}) = \vec{\delta}_2$$

Unknowns:  $\vec{Z}_1, \vec{Z}_2, \phi_2$  (5 scalar unknowns)

Say, my free choices are  $\vec{Z}_2$  &  $\phi_2$

$$Z_1 = \frac{\delta_2 - Z_2(e^{i\gamma_2})}{e^{i\phi_2}}$$

$$Z_1(e^{i\phi_j}) + Z_2(e^{i\gamma_j}) = \delta_j$$

3-position motion generation

Given  $\vec{\delta}_2, \delta_3, \gamma_2, \gamma_3$

$$Z_1(e^{i\phi_2}) + Z_2(e^{i\gamma_2}) = \delta_2$$

$$Z_1(e^{i\phi_3}) + Z_2(e^{i\gamma_3}) = \delta_3$$

Possible free choices  $Z_1, Z_2, \phi_2, \phi_3$

Linear system of eqns in  
 $Z_1$  &  $Z_2$

So let's look at two position motion synthesis, motion generation. So I have given Delta 2 and gamma 2, Delta 2 is a vector okay? Maybe I'll use the arrow like that so and I have my equation for the dyad, and we'll keep using that. So I'll write it as  $Z_1 e^{i\phi_2}$ , when Delta 2 and gamma 2. I have the equation would be  $\delta_2$ , so what could be my, I know I have three free choices, to solve these equations for  $Z_1$  and  $Z_2$  okay? That, that's my design right? We were finding the dyad is what I am trying to do, so to get that I can say I have to pick three free choices. Now I have only these two equations. I have five unknowns; unknowns are  $Z_1, Z_2, \phi_2$ , okay? So total 5 scalar unknowns, but I have only two equations. So what I could do is I could pick one vector, have a question, second equation they are real and complex. It's a vector equation right? So there are two scalar equations. Ultimately I have to solve for five scalar unknowns, the two components of vector  $Z_1$ , one, two components of  $Z_2$  and  $\phi_2$  yeah, so yeah, just till we get used to it, let me just write out that arrow on top of that okay? so  $Z_1, Z_2$  and  $\phi_2$ , so now I can choose as my free choices. What are the possibilities? I have to choose how many free choices I have to choose, 3 okay, so what could I do? The easiest way would be to either choose  $Z_1$  and  $\phi_2$  or  $Z_2$  and  $\phi_2$ , so let's say I choose, say my free choices are, it's more difficult if I say I will choose  $Z_1$  and one component of  $Z_2$  right? Solving the equation will be more difficult so free choices are this then I get  $Z_1$  equal to  $\delta_2$  minus  $Z_2$  into  $e^{i\gamma_2}$  minus 1, by  $e^{i\phi_2}$  minus. So this defines my left dyad. I can do the same thing for the right dyad and come up with the solution for the 4 bar for motion generation okay? So this is 2 position motion generation 3 infinities of solutions with these two the choices for  $Z_2$  and  $\phi_2$ . Three-position motion generation, I am given Delta 2, Delta 3, gamma 2, and gamma 3. So I get and  $\phi_3$ , delta 3. If I go back to my table how many free choices do I have? I have two free choices. Two free choices, if I do that then what are my possible, possible free choices? Are they  $Z_1$  or  $Z_2$  or  $\phi_2, \phi_3$ ? To solve these equations what would be the easiest choices?  $\phi_2$  and  $\phi_3$  right, because if I choose  $\phi_2$  and  $\phi_3$  it, this just becomes a linear system of equations okay? If I choose  $Z_1$  or  $Z_2$ , one of the two because I'll need two components there right? That would mean that I am solving the equations becomes more than difficult because I have all these sine  $\phi$ , cos  $\phi$ , term Souter, so analytically it's easy to choose these two angles but imagine in the graphical method choosing a point was easier which essentially meant I was actually picking, yeah. So I I was taking two free choices in that manner okay, when I picked a point for the moving pivot



because when I pick a point for the moving pivot that kind of defines my Z okay? As you mean I start off at the origin so I can say that that is my Z one okay? So that again number of free choices does not change because of the method that you use but what you can pick as your free choices. This is not easy to do, picking the angles and then trying to come up with a graphical solution to find the, to synthesize the linkage so do you see the difference between the graph fundamentally? They are the same. You have the same number of solutions, same number of, same number of free choices. What you can pick as your free choice varies with the graphical lengthy analytical solutions. So once I do this I can solve, it's a linear system of equations, in Z1 and Z2 and MATLAB can easily solve it for me okay, and I can find the two vectors. I repeat that for the other side of the 4 bar and I end up with the whole.

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4-position motion generation

$$z_1(e^{i\phi_2-1}) + z_2(e^{i\delta_2-1}) = \delta_2$$

$$z_1(e^{i\phi_3-1}) + z_2(e^{i\delta_3-1}) = \delta_3$$

$$z_1(e^{i\phi_4-1}) + z_2(e^{i\delta_4-1}) = \delta_4$$

Knowns :  $\delta_2 \dots \delta_4$   
 $\gamma_2 \dots \gamma_4$

Unknowns :  $\vec{z}_1, \vec{z}_2, \phi_2, \phi_3, \phi_4$  (7 unknowns)

One free choice

System of non-linear equations bcos the unknown angles are in transcendental form.

For motion gen : 3 positions are the limit for a linear solution

Four position motion generation. We didn't look at this graphically, but let's say analytically we should be able to solve, Phi 3 minus 1, plus Z2 Phi four minus one okay? This is my fourth position problem, so the known's for motion generation would be Delta 2, Delta 4 and gamma 2, 2 gamma 4 for this problem and therefore there are six equations, seven unknowns. Unknowns are Z1, Z2, Phi 2, Phi 3, Phi 4, 7 unknowns, 6 equations, 7 unknowns, one free choice, say you see here I could pick one of the angles but it will still no longer be a linear system of equations. So up to the 3 position problem the solution is fairly straightforward because you can pick your free choices in such a manner that you only have a linear system of equations to solve. From the 4 position problem onwards It becomes a little bit trickier, you still have an infinity of solutions, so I can pick one of the angles Phi 2, Phi 3, or 5 4 but it's all in transcendental form in the equation, because I can pick Phi 2, but they'll still be cos theta cos Phi 3 cos Phi 4 sine. So if it's not an easy system of equations to solve we look at a method later where we will do that a little bit later, where we will solve this problem for the four-position case. You can do that, maybe the five positions also will do with time permits, but beyond three positions you will not get a linear system of equations. The system of equations becomes a nonlinear

system of equations to be solved. So this is the system, there goes  $r$  in transcendental form okay? Okay, so for motion generation, three positions are the limit for a linear solution. So for the 4-bar once you solve both dyads you get the coupler and  $D$ , so you could have the same routine. Basically we're in MATLAB, you would write a problem to solve the dyad swab for say two position or three position syntheses. Use the call, the same routine again to solve the right side dyad and then put together the four bar, for your solution.