

Orientation of Fibers
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Lecture No. # 06
Pores among Fibers

Let us continue our theme about a yarn retraction, based on the ideal helical model. We spoke about the starting position of fiber bundle, parallel fiber bundle and the twisted yarn. In idea of Braschler, we assume that the total fiber volume in yarn and fiber cross-sectional area, means fiber diameter do not change due to twist.

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2. Idea of total fiber volume
 Usually the following *assumption* is taken as granted (E. Braschler): Total fiber volume in yarn and fiber cross-sectional area (fiber diameter) do not change due to twist.

$V_0 = V \dots \text{const.}, \quad s \dots \text{const.}$

Fiber volume - non-twisted $V_0 = n s \zeta_0$
 - twisted $V = S \zeta$ (lecture 1)

$V_0 = V, \quad n s \zeta_0 = S \zeta, \quad \zeta / \zeta_0 = s / (S/n), \quad \zeta / \zeta_0 = k_n$

Retraction was defined by equation $\delta = 1 - \zeta / \zeta_0$, coefficient k_n was derived before for ideal helical model. Therefore

yarn retraction $\delta = 1 - \left(\frac{\zeta}{\zeta_0} \right) = 1 - \frac{1}{k_n} = 1 - \frac{2}{(\pi D Z)^2} \left[\sqrt{1 + (\pi D Z)^2} - 1 \right]$

Maybe, that on the periphery fibers are a little longer than the volume of such fiber is a little, maybe small, maybe in the center is a little pressed. So, it can be opposite, but these differences are so small that Braschler mentioned that, this assumption is possible to use.

When we use this, we can write V_0 is equal V , so that it is a constant **yeah** and also fiber cross section S is constant, now change through the process of twisting. Fiber volume in non-twisted V_0 is n times because in bundle is n fibers, n times S fiber cross section

times lengths. Length is zeta 0 fiber cross section is S times zeta 0 is volume of parallel fiber times, numbers of fibers. In twisted form, the volume of fibers, all fibers material in this portion is S times zeta. S is the substance cross section of our yarn times, final zeta because V equal V0 equal. We using this formula, we obtain this here. Then, we obtain zeta by zeta 0, which is S by S by n and capital S by n substance cross section by n. It is in the bean area, sectional area pair one fiber s star bar and it was definition of K n. It was K n. So, zeta by zeta 0 is equal to K n. How it is now in ideal helical model with yarn retraction? Yarn retraction delta is 1 minus zeta by zeta 0. It was starting slight to retraction problem, but this is K n, so it is 1 minus K n.

We know K n from earlier analysis of ideal helical model number of fibers in cross section yarn corresponding to ideal helical model. Isn't it? So, we can use our equation derived on the place of K n and we obtained that delta is here. A lot is only rearranging. Let us rearrange this equation using this way to this equation rearranging only common denominator and so on and so forth.

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(Continuation)

$$\delta = \frac{\sqrt{1+(\pi DZ)^2} - \frac{2}{(\pi DZ)^2} \left[\sqrt{1+(\pi DZ)^2} - 1 \right] \left[\sqrt{1+(\pi DZ)^2} + 1 \right]}{\sqrt{1+(\pi DZ)^2} + 1}$$

$$= \frac{\sqrt{1+(\pi DZ)^2} + 1 - \frac{2}{(\pi DZ)^2} \left\{ 1 + (\pi DZ)^2 - 1 \right\}}{\sqrt{1+(\pi DZ)^2} + 1}$$

$$\delta = \frac{\sqrt{1+(\pi DZ)^2} - 1}{\sqrt{1+(\pi DZ)^2} + 1} = \frac{\sqrt{1+\tan^2 \beta_D} - 1}{\sqrt{1+\tan^2 \beta_D} + 1}$$

In another form

$$\left(\frac{\zeta}{\zeta_0} \right) = 1 - \frac{2 \cos \beta_D}{1 + \cos \beta_D} \cdot \frac{1 + \cos \beta_D}{1 + \cos \beta_D} = \frac{1 + \cos \beta_D - 2 \cos \beta_D}{1 + \cos \beta_D} = \frac{1 + \cos \beta_D - 2 \cos \beta_D}{1 + \cos \beta_D}, \quad \delta = \frac{1 - \cos \beta_D}{1 + \cos \beta_D}$$

Well, I think you can make it own self. No special routine is here. Well, so on the end we obtain delta squareroot from one plus pi DZ square minus 1 by 1 plus pi DZ square plus 1 or because pi DZ is tangents beta D. We can write it also in that form.

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Rearrangement

$$\delta = \frac{1 - \cos \beta_D}{1 + \cos \beta_D} = \frac{\left(\cos^2 \frac{\beta_D}{2} + \sin^2 \frac{\beta_D}{2} \right) - \left(\cos^2 \frac{\beta_D}{2} - \sin^2 \frac{\beta_D}{2} \right)}{\left(\cos^2 \frac{\beta_D}{2} + \sin^2 \frac{\beta_D}{2} \right) + \left(\cos^2 \frac{\beta_D}{2} - \sin^2 \frac{\beta_D}{2} \right)} = \frac{2 \sin^2 \frac{\beta_D}{2}}{2 \cos^2 \frac{\beta_D}{2}}, \quad \delta = \tan^2 \frac{\beta_D}{2}$$

Because $\kappa = \tan \beta_D = \pi D Z = 2\sqrt{\pi} \alpha / \sqrt{\mu \rho}$ (see before),

$$\delta = \frac{\sqrt{1 + (2\sqrt{\pi} \alpha / \sqrt{\mu \rho})^2} - 1}{\sqrt{1 + (2\sqrt{\pi} \alpha / \sqrt{\mu \rho})^2} + 1}, \quad \delta = \frac{\sqrt{1 + 4\pi \alpha^2 / (\mu \rho)} - 1}{\sqrt{1 + 4\pi \alpha^2 / (\mu \rho)} + 1}$$

Using $\alpha = \alpha_0 / (1 - \delta)^{3/2}$, we can express δ as a function of latent twist coefficient α_0 as follows

$$\delta = \frac{\sqrt{1 + 4\pi (\alpha_0 / (1 - \delta)^{3/2})^2 / (\mu \rho)} - 1}{\sqrt{1 + 4\pi (\alpha_0 / (1 - \delta)^{3/2})^2 / (\mu \rho)} + 1}$$

Second expression for K_n , second version of rearranging of K_n for helical model was this here. K_n has a function of it, it is this here. So, that after rearranging, we can write the same delta also in such form. The fact is rearranging according Braschler, when delta is this here, we write it here. Then, after rearranging, we obtain delta is equal tangent square beta D by 2. I think it is this. This is the easiest formally easiest. All identical all is the same it is only all different shapes of interpretation.

Well, now we want also to know this delta yarn retraction as a function of this coefficient alpha. We know that intensity of this intensity is tangents beta BD is pi DZ and it was derived that it is also this here. Using this, we obtain for delta on the place of tangents beta D here or pi DZ here.

We obtain this equation on so that after small rearranging this. This may be fourth or fifth identical equation for yarn retraction. More interesting will be to express yarn retraction as a function of latent twist coefficient related to starting lengths where Z twist and the count, I relate it to starting values. Let us remember it.

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The discriminant of the quadratic equation must not be negative. Therefore $1 - \frac{4\pi \alpha_0^2}{\mu \rho} \geq 0$, $\alpha_0^2 \leq \frac{\mu \rho}{4\pi}$, $\frac{\alpha_0}{\sqrt{\mu \rho}} \leq \frac{1}{\sqrt{4\pi}}$

The latent twist coefficient is limited!

Limit case: $\frac{\alpha_0}{\sqrt{\mu \rho}} = \frac{1}{\sqrt{4\pi}} = 0.281$ $\delta = \frac{1}{2} \pm \frac{1}{2} \sqrt{1 - \frac{4\pi \alpha_0^2}{\mu \rho}}$, $\delta = \frac{1}{2}$

Since $\delta = \tan^2 \frac{\beta_D}{2}$, hence $\frac{1}{2} = \tan^2 \frac{\beta_D}{2}$, $\beta_D = 2 \arctan \sqrt{\frac{1}{2}}$, $\beta_D = 70.5^\circ$

From yarn retraction $\delta = \frac{(\sqrt{1 + \tan^2 \beta_D} - 1)}{(\sqrt{1 + \tan^2 \beta_D} + 1)}$
 we obtain $\delta \sqrt{1 + \tan^2 \beta_D} + \delta = \sqrt{1 + \tan^2 \beta_D} - 1$

 $\sqrt{1 + \tan^2 \beta_D} (1 - \delta)$, $\left(\frac{1 + \delta}{1 - \delta}\right)^2 = 1 + \tan^2 \beta_D$, $\tan \beta_D = \sqrt{\left(\frac{1 + \delta}{1 - \delta}\right)^2 - 1}$

We know that it was shown on the previous pages. It was shown that alpha is alpha 0 by 1 minus delta power 3 by 2. Sorry, I was here. So, we use this. We use this equation on the place of alpha here. We obtain this equation. The same is the here, this equation. The problem is that, now we have delta on left hand side as earlier, but also here and here. So, we must rearrange; its only mathematical operation.

We must rearrange this equation because to obtain the delta explicitly, it means in the form beta delta is equals some function on right hand side must not be delta. It is possible the way it is shown here. What is your quietly home step by step to see it. It is good in first step. For first step, call this ratio as a, then delta is this here rearranging. Then, I make square of left hand side as well as right hand side rearranging here. Yes, this, this, this and here. I give back to the helping quantity a, this ratio here. After rearranging, we obtain such resulting equation.

It is permanently same delta, but now the delta is function is explained as a function of latent twist coefficient alpha 0. See it from a one point of view. It is interesting. Why? Under square root must not be a (0) value. Isn't it? So, this value must be higher equal 0.

So, that this value must be higher equal 0 because under square root is not possible. We speak about the real values, not complex values. Well, it must be this here. So, Z is here. So, that this here is very important. It is very important because it says mu is some quantity from 0 to 1. Some think it is rho specific mass density of fibers. It is some value, some

constant. It is shown here that this α_0 by this constant square root must be smaller than some parameter 1 by square root of 4π .

So, that α_0 must have some border, must be smaller than some border value. Isn't it? It is not possible to give number of horse to run unit for starting such a starting fiber bundle. How you want? It exists some moment in which is not possible more to give the coil inside. When you prove it, then you obtain something. Other, I will show you later. Do understand what represents this equation here?

Let us calculate the parameters by maximum possible twist of the yarn. The maximum twist is, if this equivalency here is valid. So, that its valid α_0 by square root of μ , ρ is equal 1 by square root 4 times π , by the way 0.28 and something. Using this to the equation for retraction yarn retraction on this place, we obtain 0 . We obtain Δ is 1 half 50 percentage of this theoretical maximum retraction of the yarn.

Since, Δ equal tangent β square by 2 , hence 1 half 13 peripheral angle in this point of maximum twist β D is 70 degree. Now, using equations derived, we obtain also tangents β D , which is 2 times square root of 2 , roughly 2.8 . So, other equations or results, the border results for maximum twist. As a root from quadratic equation which was here, we obtain plus minus. The question is what is real? Automatically, we have two roots. Physically, only one is real, one is not. The second is not possible in reality to obtain. It is plus or minus C .

Plus somebody said plus. Plus do not be possible. Yes. You are right, you are right because let us imagine the structure without twist, then α_0 is equal 0 square root, this 0 square root from 1 is 1 . So, it is 1 half plus minus 1 half. You can obtain 0 or 1 . When you have parallel fiber bundle without twist, you cannot have the value of retraction 1 to 0 . You must have the value to 0 once. I mean, you must be having this value; this retraction must be equal to 0 . Therefore, this minus is real, real symbol here.

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and using the value $\delta = 1/2$ we get for the limit case

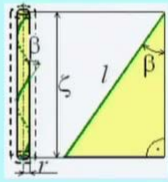
$$\tan \beta_D = \sqrt{\left(\frac{1+0.5}{1-0.5}\right)^2 - 1} = \sqrt{3^2 - 1}, \quad \kappa = \pi D Z = \tan \beta_D = 2\sqrt{2} = 2.828$$

The value of twist intensity is limited!

3. Idea of yarn axial force
 Starting fiber length ζ_0 changes its value to l due to twist.

Yarn retraction (definition): $\delta = 1 - \zeta/\zeta_0$
Fiber strain: $\varepsilon = (l - \zeta_0)/\zeta_0 = l/\zeta_0 - 1$

Since $l = \zeta/\cos \beta$, hence $\varepsilon = \frac{\zeta/\cos \beta - \zeta_0}{\zeta_0} = \frac{\zeta/\zeta_0}{\cos \beta} - 1$,

$$\varepsilon = \frac{1 - \delta}{\cos \beta} - 1$$


The third idea based on axial forces is also now important for us. This version according to Braschler is enough good. Yes and please any minutes for change of yarn 2. Let us continue our theme about a yarn retraction.

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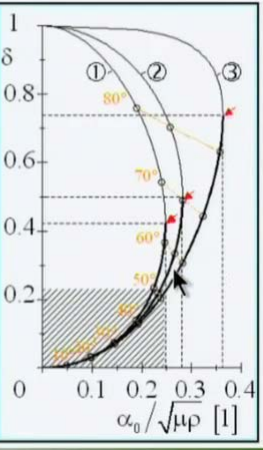
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Graphical interpretation

- ①... Idea of neutral radius
- ②... Idea of fiber volume
- ③... Idea of axial force

Thick part ... real
 Thin part ... hypothetical
 ... limit case - "saturated twist", parameters (summary):

Idea	$\frac{\alpha_0}{\sqrt{\mu\rho}}$	δ	κ	β_D
① Neutral radius	0.248	0.423	2	63°
② Fiber volume	0.281	0.5	2.828	70.5°
③ Axial force	0.363	0.737	9.528	84°

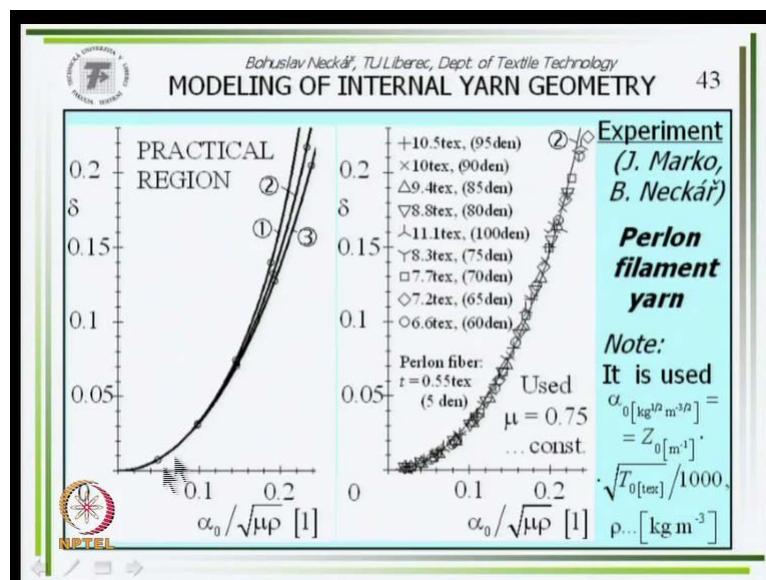


It is a summary for all three ideas. We analyze only the idea number 2, according to Braschler and we obtained this expression for yarn retraction. How it is graphically interpreted? Here is α_0 latent twist coefficient by square root of $\mu\rho$ in relation to yarn retraction δ . Our curve is the curve number 2. It is here. What we obtained by first course? Now, significant change in lengths, then the speed with increasing, with

shortening increase and increase and here is the maximum value. Here is the maximum possible value, the border value and now more is possible.

Theoretically, when we use minus than plus in our equation, you obtain the second thin curve. It is only for completeness. The real is this thin line. Real is the thick line here. Usually, we have the chance to go to this theoretically derived end point and practical maximum twist is coming earlier, may be in this moment. How is this graph, this part of our graph is shown here?

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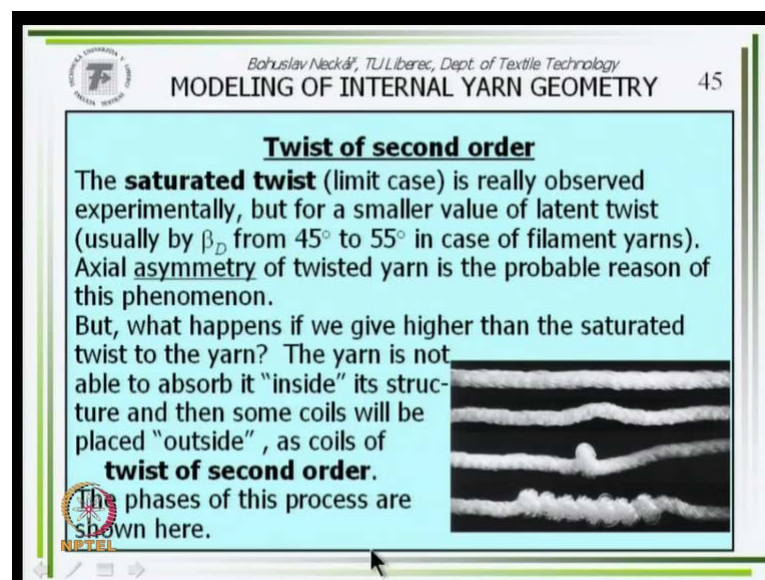
The second curve is the middle curve among these three. So, you see that all three hypotheses are very similar. Is it well? Is not well? In relation to the reality because we apply ideal helical model, evidently to this model nearest structure is the structure of twisted filament yarn. Lot years ago, we measured together with my older colleague, Professor Marco, we measured lot of filament yarn on a special instrument which we created and we measured the yarn retraction.

You can see that all different counts, all different twists together are lying on only one curve. Using peck intensity 0.75 in our equation, this continual line show the curve in our, according our theoretical model. The curve Perkins is excellent. It is the best in my life. The comparison between experimental research and theoretical curve, so perfect it is, but around 0.25, around this point, stop the possibility in practice in laboratory, stop the

possibility to test filament yarn was not more possible. In relation to the theoretical model, it is roughly here in this moment, now here.

From point of view of yarn retraction, the difference is high, but from point of view of α_0 , the difference is not too high. The question is, why coming this border situation earlier? It is evident, because now our expressions are related to the very complicated structure of the real yarn. Real yarn is not axially perfectly symmetric. Therefore, one bending mechanism also is coming, when the peripheral fibers press the central and so on because the yarn is not absolutely perfect in symmetric axial symmetric. Therefore, this critical moment is coming a little earlier than our results from theory, but it is coming. It is coming.

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Twist of second order

The **saturated twist** (limit case) is really observed experimentally, but for a smaller value of latent twist (usually by β_D from 45° to 55° in case of filament yarns). Axial asymmetry of twisted yarn is the probable reason of this phenomenon.

But, what happens if we give higher than the saturated twist to the yarn? The yarn is not able to absorb it "inside" its structure and then some coils will be placed "outside", as coils of **twist of second order**.

The phases of this process are shown here.

The diagram on the right shows a cross-section of a yarn with internal fibers. The top part shows a regular helical structure, while the bottom part shows a more complex structure with some fibers forming external coils, illustrating the 'twist of second order' phenomenon.

What is twisted filament yarn? When we give more coils inside this one, the maximum of possible twist, we call it as a saturated twist, that terminology saturated twist. Then, it is not possible more to give the twist to our filament yarn. I start it first, and then, more and more helical of twist of second order. It is important, be under this border in the technology of texturing because when you have in machine, you use too high twist. Then, such moments like this or this can break your yarn and destroy this. The process is not continual.

More difficult for filament yarn, this model based on ideal helical model can be applied without problem, nevertheless for staple yarn, it brings complications. It is more

complicated. Why? Staple yarns are from staple fibers, so that the ends, fiber ends and something can slip, especially on the periphery of the yarn by twisting. Isn't it?

Therefore, not so high force for retraction as by filament yarn, therefore the yarn retraction in staple yarn is usually smaller. Not too much, but a little smaller than the retraction by filament yarn. It is difficult to measure it, very difficult, retraction by staple yarn. Now, some experimental results exist. Therefore, I can recommend you. When you have not something better, then I can recommend you, use it. To use our equation for, the shape of our equation for yarn retraction but on the place of real yarn diameter D gives some more defined diameter $D\delta$. Some smaller, a little smaller value, than real yarn diameter D and this $D\delta$ is related to D . Using this pure empirical form, it is pure empiric expression based on some set of experimental results.

So, that D yarn diameter, staple yarn diameter times this expression, where μ specking density and S is substantial cross section of the yarn. It is better than nothing, built now too good, but it is difficult to say what is good and what is bad because it is very difficult to measure yarn retraction by yarn, experimentally. When we are speaking about different applications of helical model, let us mention also yarn stress strain relation model, according a generalize theory of Gegauff and others. By the way, Gegauff was one of us and of 19th century, second half of 19th century.

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Yarn stress-strain relation
 like Gegauff and others

The general element of the helical fiber (length dl , angle β) lying at the radius r determines an elementary cylindrical surface (green) with dimensions $r d\phi$, $d\zeta$. After yarn elongation the same element shifts itself to a new (yellow) position at a smaller radius r' with new angle β' and new dimensions $r' d\phi$, $d\zeta'$. It is valid: $\tan\beta = r d\phi/d\zeta$, $\tan\beta' = r' d\phi/d\zeta'$

axial strain: $\epsilon_a = (d\zeta' - d\zeta)/d\zeta = d\zeta'/d\zeta - 1$, $d\zeta' = (1 + \epsilon_a) d\zeta$

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In the picture, we have two fiber elements, 2 red fiber elements. 1 red fiber element is laying on the green surfaces of some cylinder and elemental part of this cylinder surface is shown. This height is $D Zeta$. This ends must be this is radius r . So, this ends is r times $D Zeta$. Well, the angle, the element of angle is $D phi$. Such element, this green element we said red fiber is also here. So, this length is $R D phi$. This is $D zeta$ and this angle, this angle, this angle $beta$ our known angle $beta$.

Well, now, let us take the yarn and load this yarn in some breaking machine or so. Then, you obtain a new position, a new geometry of our fiber element. By the way, do you know how it is in English? ((FL)). You know it. Did you use as eyes and when you use it make also no.

What did you see that the thickness of this ((O)) is decreasing, some contraction. Isn't it? The same effect is in the yarn by its holding, so that our element which started on the radius R is changed his position to another smaller radius r dash. Of course, because we elongate the yarn, balance the zeta starting length $D Zeta$ which also elongate to new length $D Zeta$ dash. Sorry, it is my mistake here. This arrow shall be here. It is my mistake in this in this picture. Sorry. Nobody is perfect. Well, to mu lengths d dash. So, the lengths of the fiber DL is now longer, have the lengths DL dash and the angle $beta$ is changed, B may be smaller, mu angle is B dash. Isn't it?

Let us, now define some relative quantities. Epsilon L , epsilon in axial direction, epsilon, therefore a. It is $D Zeta$ dash minus the zeta by $D Zeta$, each strain axial strain. So, that it is this one or $D Zeta$ dash is $1 + epsilon a$ times $D Zeta$. Well, it is a repetition from last picture.

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Radial strain: $\varepsilon_r = \frac{r' - r}{r} = \frac{r'}{r} - 1, \quad r' = (1 + \varepsilon_r) r$

Contraction ratio (like Poisson): $\eta = -\varepsilon_r / \varepsilon_a$

Fiber strain: $\varepsilon_l = \frac{dl' - dl}{dl} = \frac{dl'}{dl} - 1, \quad \frac{dl'}{dl} = 1 + \varepsilon_l$

Based on the Pythagorean theorem, it is valid

- before deformation: $d^2l = d^2\zeta + (r d\varphi)^2$
- after deformation: $d^2l' = d^2\zeta' + (r' d\varphi)^2 =$

$$= (1 + \varepsilon_a)^2 d^2\zeta + (1 + \varepsilon_r)^2 (r d\varphi)^2 = (1 + \varepsilon_a)^2 d^2\zeta + (1 - \eta \varepsilon_a)^2 (r d\varphi)^2$$

Note: Because of continuity of yarn body, $d\varphi$ must be the same.

Radial strain is final radius minus starting radius by starting radius. So, it is this one. So, it is this here. Let us think that epsilon r must be major difference because r dash is smaller than starting r. The chewing gum effect contraction, isn't it?

Contraction ratio you know, it may be under the Poisson contraction ratio. It is defined as a minus epsilon r by epsilon a. So, it is positive value because minus epsilon r is positive value. Well, fiber strain epsilon L is DL dash minus DL by DL evidently. So, it is this one. DL dash by DL is 1 plus epsilon L.

Now, based on Pythagorean Theorem, we can write D square L dash is DL dash. So, square of this is equal D Zeta dash square D square zeta dash this length square plus this length square. It is this here. Nevertheless, according to the reality quantities which we derived, we can write on the place of this here, such expression and here, this expression and after rearranging using also the quantity contraction ratio, we obtain D square L dash in such form, rearranging trivial rearranging.

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Using earlier derived equation, we obtain

$$(1 + \epsilon_l)^2 = \frac{d^2 l'}{d^2 l} = \frac{(1 + \epsilon_a)^2 d^2 \zeta + (1 - \eta \epsilon_a)^2 (r d\phi)^2}{d^2 \zeta + (r d\phi)^2} = \frac{(1 + \epsilon_a)^2 + (1 - \eta \epsilon_a)^2 \left(\frac{-r \tan \beta}{r d\phi / d\zeta}\right)^2}{1 + \left(\frac{r d\phi / d\zeta}{1}\right)^2}$$

$$= \frac{(1 + \epsilon_a)^2 + (1 - \eta \epsilon_a)^2 \tan^2 \beta}{1 + \tan^2 \beta} = \frac{(1 + 2\epsilon_a + \epsilon_a^2) + (1 - 2\eta \epsilon_a + \eta^2 \epsilon_a^2) \tan^2 \beta}{1 + \tan^2 \beta}$$

$$= \frac{1 + 2\epsilon_a + \epsilon_a^2 + \tan^2 \beta - 2\eta \epsilon_a \tan^2 \beta + \eta^2 \epsilon_a^2 \tan^2 \beta}{1 + \tan^2 \beta} = 1 + \frac{2\epsilon_a - 2\eta \epsilon_a \tan^2 \beta}{1 + \tan^2 \beta} + \frac{\epsilon_a^2 + \eta^2 \epsilon_a^2 \tan^2 \beta}{1 + \tan^2 \beta}$$

$$(1 + \epsilon_l)^2 = 1 + 2\epsilon_a (\cos^2 \beta - \eta \sin^2 \beta) + \epsilon_a^2 (\cos^2 \beta + \eta^2 \sin^2 \beta)$$

Assumption: Strains are small. Then $\epsilon_l^2 \rightarrow 0$, $\epsilon_a^2 \rightarrow 0$ and

$$1 + 2\epsilon_l + \epsilon_l^2 = 1 + 2\epsilon_a (\cos^2 \beta - \eta \sin^2 \beta) + \epsilon_a^2 (\cos^2 \beta + \eta^2 \sin^2 \beta)$$

$\epsilon_l = \epsilon_a (\cos^2 \beta - \eta \sin^2 \beta)$ **Note: Gegauff (1907) used $\eta=0$ and then he obtained $\epsilon_l = \epsilon_a \cos^2 \beta$**

Now, all geometric quantities are changed by yarn elongation, but the angle $D\phi$ must stay the same. Why? We have not only one element, but lot of elements around and sum of all $D\phi$ around our yarn is cross section give two ϕ the 160 degree before as well as after elongation. If $D\phi$ for example, will be smaller than by elongation on the yarn, it will be some whole some. Something so, therefore $D\phi$ must not be changed.

Well, now your D square, it is here. From this triangle, the Pythagorean Theorem is easier is D square L is D square ζ plus $R D\phi$ square from this triangle. So, it is d square L and D square L dash. The ratio D square L dash by D square L is equal to 1 plus epsilon L . We said we used what? We derived this and this. We arranged this, we know what that for example, $r d\phi$ by $D \zeta$ is tangents beta and so on and so on.

After re-arranging, we obtain this ratio where the green numbers have linear epsilon a , the black this and this, has epsilon r square and violet are result epsilon a . Some of these violet are same than the denominator here. So, that we can write our expression which start 1 plus epsilon L square is equal to such form and because 1 plus tangent beta square is on B by square is here too. So, we obtain this expression.

In our lecture, we usually solve the easiest cases. So, let us imagine because be easier and sometimes, it is real. In lot cases, it is possible to imagine that the formation, the elongation of the yarn is small.

If it is small, then epsilon L square is very small and epsilon a , sorry epsilon a square is also very small. It is limited to 0, so that 1 plus 2 time epsilon L plus epsilon L square. We

can write roughly 0 on the place of you have 1 plus 2 times epsilon l for epsilon r. We use those, we derived and then after rearranging formation, only we obtain epsilon l is epsilon a times square beta minus eta times sine square beta. Eta is a contraction ratio, Poisson's contraction ratio. Some think between 0 and 0.5 may be. Without this member which is the influence of contraction, this equation was derived by Gegauff in 1907.

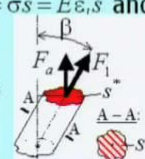
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Assumption (easiest case): The fiber tensile stress-strain relation is linear $\sigma = E\varepsilon_f$, where σ ...tensile stress and E ...Young modulus. Axial force in fiber is $F_1 = \sigma s = E\varepsilon_f s$ and the component force in the direction of yarn axis is $F_a = F_1 \cos \beta = E\varepsilon_f s \cos \beta$. The fiber sectional area (red) is $s^* = s / \cos \beta$. Normal stress on this area is

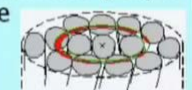
$$\sigma_a = \frac{F_a}{s^*} = \frac{E\varepsilon_f s \cos \beta}{s / \cos \beta} = E \varepsilon_f \cos^2 \beta$$



$\sigma_a = E\varepsilon_a (\cos^4 \beta - \eta \sin^2 \beta \cos^2 \beta)$ (Small deformation is assumed.)

Fiber sectional area inside the differential annulus (red) is $dS = 2\pi r dr \mu$ (derived earlier) and then the yarn axial force is

$$P = \int_{r=0}^{r=D/2} \sigma_a dS$$



You see that I do not present you some quite a new theoretical model. It is 100 year old model. Well, now it is which forces? In a fiber, the axial force is called as F_1 . F_1 because pair one fiber. The fiber tensile stress-strain relation, let us imagine I said easiest case that its linear, then the stress σ is proportional to ε . In Hooke's law, then E is young modulus, but it is a constant in our case. Axial force F_1 is to the area perpendicular to fiber axis, of course is σ times s . So, an ε times s . The vertical component F_a is F_1 times $\cos \beta$. So, that it is this here.

The fiber sectional area, this red is s^* which is s by $\cos \beta$. In today, we said it. Normal stress on this area, on this red area is σ_a , which is normal force F_a by area s^* . It is this here. Then, ε , for ε we use the expression for small deformation of course. We obtain σ_a is E times ε times this expression for small deformation I said.

Now back to our scheme which we used for number of fibers in yarn cross section. We know that in elemental annulus, the area of fibers is Ds . You know it was

derived. Now, the sigma a is given by this equation, so that we can integrate, we can say what is the total axial force as a sum from all areas of fiber sections. It is shown here.

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Rearrangement:

$$P = \int_{r=0}^{r=D/2} \sigma_a dS = \int_0^{D/2} E \epsilon_a (\cos^4 \beta - \eta \sin^2 \beta \cos^2 \beta) 2\pi r dr = 2\pi \mu E \epsilon_a \int_0^{D/2} (\cos^4 \beta - \eta \sin^2 \beta \cos^2 \beta) r dr =$$

Substitution: $r = \frac{2\pi r Z}{2\pi Z} = \frac{D \tan \beta}{2 \tan \beta_D} = \frac{D \tan \beta}{2 \tan \beta_D}$, $dr = \frac{D}{2 \tan \beta_D \cos^2 \beta} d\beta$

$$r dr = \left(\frac{D \tan \beta}{2 \tan \beta_D} \right) \left(\frac{D}{2 \tan \beta_D \cos^2 \beta} d\beta \right) = \left(\frac{D}{2 \tan \beta_D} \right)^2 \frac{\sin \beta}{\cos^3 \beta} d\beta$$

$$= 2\pi \mu E \epsilon_a \int_{\beta=0}^{\beta=\beta_D} (\cos^4 \beta - \eta \sin^2 \beta \cos^2 \beta) \left(\frac{D}{2 \tan \beta_D} \right)^2 \frac{\sin \beta}{\cos^3 \beta} d\beta = 2\pi \mu E \epsilon_a \left(\frac{D}{2 \tan \beta_D} \right)^2 \int_0^{\beta_D} (\cos^4 \beta - \eta \sin^2 \beta \cos^2 \beta) \frac{\sin \beta}{\cos^3 \beta} d\beta$$

All other substitution, only one substitution rearranging. Then, it is a way we assume. Yes in one moment, we assume that eta contraction ratio is constant is same in v in each point in yarn. Hence, we integrate and integrate and integrate. Nothing more traditional integration which you must absorb in your first semesters by mathematic, isn't it?

Well, then on the final form, we obtain this equation, nothing more than integration of this one. Logically, it is clear. We obtained this equation for force P force. P is given by this pi times mu pecking density times module, may be young modulus times epsilon a axial strain of our yarn 1 half of diameter square and here is angle beta D peripheral angle of fiber in yarn on the yarn surface and eta and eta. It is nice, but more interesting can be the tensile force utilization coefficient.

It was one side. We know the force which we need for elongation of yarn using strain epsilon a axial strain. In other case, let us imagine another yarn without twist parallel fiber bundle or something. So, let us ask how we must, how is the force for the same strain in such parallel fiber bundle strain? Yeah same count.

Well, sigma a, was e times epsilon a, because the fibers are perpendicular to cross section parallel fiber bundle. So, it is equal and S is equal to PD square by 4 times mu. Isn't

it? Using this, we obtain such expression for force P^* , for force in the same yarn, but without twist. Then, the effect of twist to mechanical properties, we can do tensile force. We can express as a ratio axial force in twisted yarn by axial force in non-twisted yarn.

Using our equations, you can obtain this. Here, you can see that this expression is same than which is before brackets. Therefore, it is this here. Well, how it is theoretically and how is the comparison to some experiments? This is the utilization coefficient ϕ is called ϕ here. It is utilization coefficient and it based on angle β D peripheral angle and also, η is playing η contraction ratio. This is angle β d. This is our utilization coefficient and there are functions for different values of η . If η is equal 0, so that the traditional Gegauff's idea, we obtain such function. Here higher is η , then the function is smaller. If smaller and smaller values of ϕ , but η is same. The theoretical curves are here based on our equation, which is this here.

How this practically? John Heiro, a very known professor from **mist** from Manchester, now he is old man, but he was really the top person among his years. As his PHD student studied the strength of different types of filament yarns, and they obtained such points for these yarns. It is from the book of Heiro and co-workers. Now, book on mechanics.

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3. Strength of staple yarn is usually interpreted – beside others - as

- a) a resultant of fiber path and fiber straining in yarn and
- b) a complex of frictional mechanisms.

First of them (|) is described – say about - by our ϕ (in an easiest case). The second one (|) is still an open problem in yarn theory.

Closing note: Helical model is the best known theoretical concept in internal yarn geometry. We showed only a few basic imaginations in this lecture. Many other versions and their applications can be found in traditional textile literatures.

Well, this is the axis of our ϕ . This is our βd and using η equal 0.5, we obtain this function. So, you see that, only here is not it is little order for, but from this moment, it corresponds to our result. So, you can say that from filament yarn, this result can be roughly used for estimation of strength. Having higher twist, this quantity ϕ is decreasing. It means, when I want elongate, I do not know 5 percentage parallel fibers bundle and twisted yarns and counts, then the twisted, both filament yarn. I mean, then in parallel fiber bundle, I need a higher force than by twisted yarn. **Twisted yarn is not,** filament yarn is not so tough than parallel fiber bundles.

Why because the forces, it will be a variant I think from equations which I have and not to the strength of staple yarn. You know that the staple yarn among others, for strength of staple yarn influences two important phenomenons. One is twist and second is our friction among fibers, then the internal geometry of the yarn. The internal geometry brings some decreasing curve, this green decreasing curve for yarn tenacity or something. In similar way, then our model of course, our model is based on lot of assumptions, but principally this is same effect.

The second effect is the blue curve here, which shows symbolically the effect of friction. When we have very small twist or 0 twist, then in filament yarn, for elongation of filament yarn, we need highest force. Therefore, also easier, say the strength of parallel fiber bundle is highest, but we cannot use it by staple yarn because friction fiber was so small as a blast in air. So, the friction effect is increasing principally according to this blue curve and two such influences together with energy give something like this, a red curve. Therefore, this curve has some maximum point, point of critical twist point in which the strength of the yarn is maximum. Isn't it?

Now, to the future of such modeling, I said that this curve, we principally are able to create. The easiest version of it, I present it here now. From others eye, the blue curve is in whole world, the secret to these days. The problem is friction among fibers. We only know that the traditional equations like Coulomb equation and Euler's equations and soon are not enough well for use in modeling of yarn internal structure. How it is? That is a question. Hope, somebody of you in future will be successful and will solve these special laws which are valid for friction among fibers in yarn and other fibers as well. I think that is all for today.