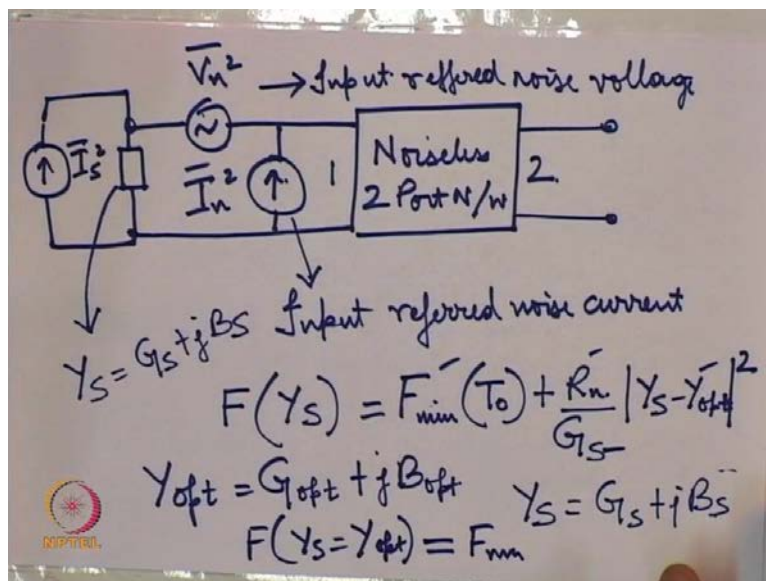


Microwave Integrated Circuits
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Module - 07
Lecture Number - 30
Noise Figure Circles (contd.)

Hello! Welcome to another module of this course “Microwave Integrated Circuits”. We are in the week 7 module 4. In the previous module we had covered the various aspects of noise how noise originates how to characterize noise and then we also introduced the concept of noise figure and noise measure. And then I mentioned how to how to adjust or how to arrange stages in cascades so that you get the lowest noise figure overall. In this module we will be covering the noise figure circles or how to design a circle which has a given requirement of noise figure. How do we design that circuit so as to achieve a particular value of noise figure?

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So in this module we will be just we will proceeding just like in the same way that we proceeded for the gain circles that is to design that is to design a circuit having a particular value of transducer gain, unilateral case or the operating power gain of the available power gain. So let us let us see how to how to obtain these noise figure circles. So the first aspect is that we have our two port network. This is power two port network and if we consider it to be a noise less circuit, so this is our noise less two port network and so what we have is two aspects of two quantities which have to be extracted.

The input referred noise voltage and the input referred noise current so this is port 1 and this is port 2. Now suppose we have a noise source here it is a current source now it can be shown that... Now suppose this is our entire arrangement this is our input ka noise current source, this is the impedance or admittance of this noise source this at the V_N square and I_N square of the input referred noise and noise voltage and noise current.

Then it can be shown that the noise figure for particular value of Y_S is given by where we have this Y_{opt} is equal to G_{opt} plus jB_{opt} so what we have is 1 2 3. There are 3 quantities this F_{min} , R_N and Y_{opt} if we know these three quantities then we can completely characterize the noise associated the noise (also) noise figure associated with a two port network. Now G_S here is given by this Y_S is given by G_S plus jB_S so it is the real part of Y_S .

So there is what this means is there is an optimum value of Y_S for which we obtain F_{min} , F_{min} that is F_{YS} equals to Y_{opt} is equal to F_{min} . This T is an argument just to emphasize that noise figure is a function of temperature.

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Normalization

$$F(Y_S) = F_{min} + \frac{\gamma_n}{g_s} |y_s - y_{opt}|^2$$

where $y_{opt} = \frac{Y_{opt}}{Y_0} = g_{opt} + j b_{opt}$
 $\qquad\qquad\qquad = \frac{1 - \Gamma_{opt}}{1 + \Gamma_{opt}}$

$$\gamma_n = \frac{R_n}{Z_0}$$

$$y_s = \frac{Y_s}{Y_0} = g_s + j b_s = \frac{1 - \Gamma_s}{1 + \Gamma_s}$$

Now this equation can be rewritten in terms of the normalized values like this. Now here I am not writing the argument Y argument T where small Y_{opt} is equal to Y_{opt} on Y_0 . R_N is equal to now this small Y_{opt} can also be written in terms of the reflection coefficient γ_{opt} like this. Now and this Y_S is equal to Y_S upon Y_0 .

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$$F(\gamma_s) = F_{min} + \frac{4r_n |\gamma_s - \gamma_{opt}|^2}{(1 - |\gamma_s|^2) |1 + \gamma_{opt}|^2}$$

For $F = \text{const}$; the loci of γ_s .

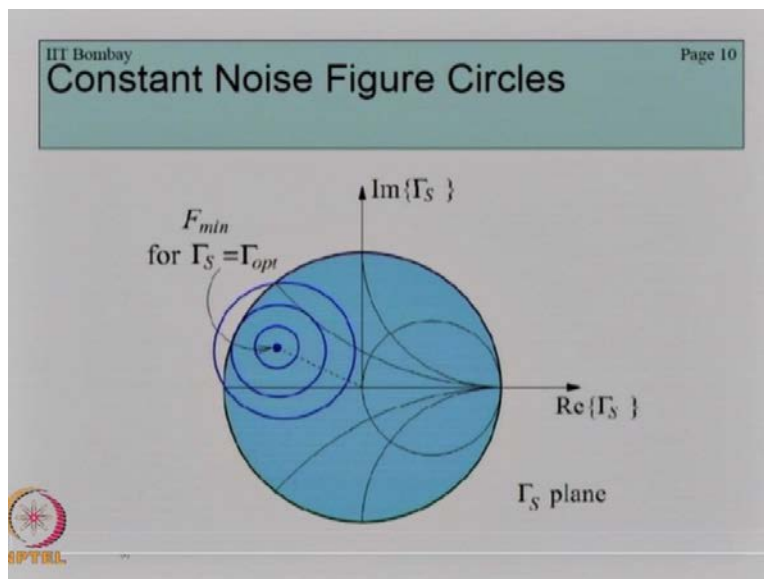
$$|\gamma_s - C_i| = R_i$$

$$C_i = \frac{\gamma_{opt}}{1 + N_i} \quad R_i = \frac{\sqrt{N_i^2 + N_i(1 - |\gamma_{opt}|^2)}}{1 + N_i}$$

$$N_i = \frac{F_i - F_{min}}{4r_n} |1 + \gamma_{opt}|^2 = \frac{|\gamma_s - \gamma_{opt}|^2}{1 - |\gamma_s|^2}$$

Now this noise figured f can be written as... Now it can be shown that for a constant noise figure F is equal to constant the locus of γ_s will be given as and then this R_i is given by like this... which this N_i is given by this relationship and we can show this is like this.

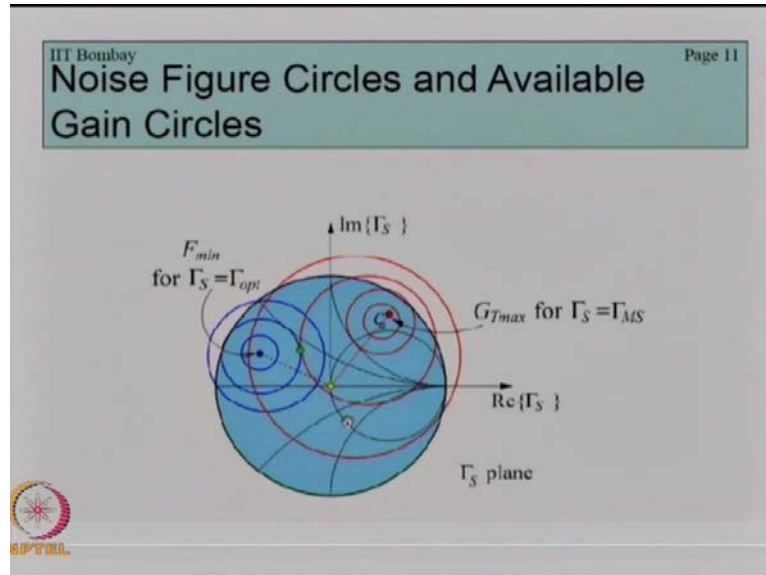
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Now if we plot these curves these noise figure circles then we go to the slides on the monitor, these are the circles this the γ_s plane and we know that γ_s plane is related to the available power of gain.

Because when we design a circuit using the available power of gain circle we are in the Γ_S plane and you can see that for Γ_S equal to Γ_{opt} that is for Γ_S equal to Γ_{MS} the radius of these circles is 0.

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For other values of Γ_S radius that is as the difference between Γ_S and Γ_{opt} increases the radius of these circles increases. So as I was saying that this is the Γ_S plane and we can draw the available power gain circles. Now we know that the center of the available power gain circles lie on this line joining the origin with CA and the radius for Γ_S equal to Γ_{MS} that is the bilateral solution of the transducer gain, at that point we get G_A equal to G_{Amax} equal to G_{Tmax} and at that point the radius of these available power gains circles is 0.

Now if we want to satisfy both the available power gain requirement and the noise figure requirement then we choose a point where, suppose this is the available power gain circle we want to we have and this is the noise figure circle we want the desired noise figure. And the point of intersection between the 2 will give the solution for both the noise figure and the available power gain.

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Noise Measure

The fundamental noise figure of merit is the noise measure :

$$M = \frac{F-1}{1 - \frac{1}{G_A}}$$

as it accounts for both noise figure F and gain G_A .

The Γ_S locus of constant noise measure are located on circles :

$$|\Gamma_S - C_m| = R_m$$


where

$$C_m = \frac{M|1 + \Gamma_{opt}|^2 C_1 + 4r_n |S_{21}|^2 \Gamma_{opt}}{M|1 + \Gamma_{opt}|^2 P + |S_{21}|^2 (4r_n - W)}, \quad R_m = \frac{\sqrt{M^2 M_s + M M_s + M_s}}{M|1 + \Gamma_{opt}|^2 P + |S_{21}|^2 (4r_n - W)}$$

$$W = |1 + \Gamma_{opt}|^2 (F_{min} - 1)$$

$$P = |S_{21}|^2 + |S_{11}|^2 - |\Delta|^2, \quad Q = |S_{22}|^2 + |S_{21}|^2 - 1, \quad M_s = |1 + \Gamma_{opt}|^4 (PQ + |C_1|^2)$$


$$M_s = |1 + \Gamma_{opt}|^2 |S_{21}|^2 [8r_n \text{Re}\{\Gamma_{opt} C_1\} - (4r_n |\Gamma_{opt}|^2 + W)P - (W - 4r_n)Q]$$

$$M_s = W |S_{21}|^4 [W - 4r_n (1 - |\Gamma_{opt}|^2)]$$


In the same that we can you know draw noise figure circles we can also draw noise measure circles and I don't want to go too much into these noise measure circles but they are useful sometimes.

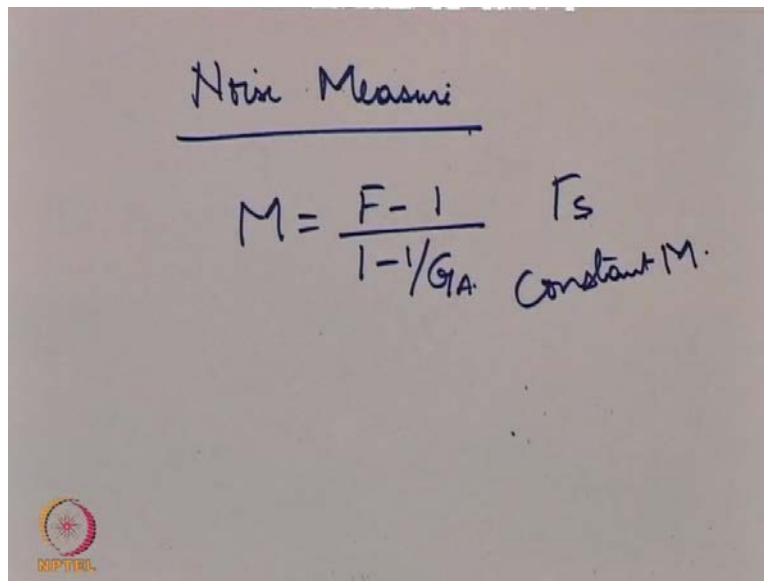
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Noise Measure

$$M = \frac{F-1}{1 - 1/G_A} \quad \Gamma_S \text{ Constant } M.$$


So if we come back to the slides on the written slides you know just like so noise measure of a stage is defined like this. So though not very common but these for a constant noise measure not very useful especially for single stages, but we can have noise measure circles where we trace the locus of gamma S for a constant M.

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Noise Measure

$$M = \frac{F-1}{1-1/GA} T_s$$

Constant M.

And if we go to the slides on the monitor so here we can see some sample noise measure circles which have been plotted these red circles and just like the noise figure circle, we also have something called Optimum Termination for optimum for minimum noise measure.

So in summary so if we just want to summarize this module in this module we learnt about the noise figure circles, we saw that there are 3 quantities which are needed to characterize to write an equation for the noise figure of a stage 2 port network.

One is the Y_{opt} , F_{min} and the $R_{s, RN}$. And we saw how we can draw this noise figure circles and how we along with the available power gain circles we can obtain optimum values of Y_S to satisfy both the available power of gain requirement and the noise figure requirement. Now this is a technique that is frequently used whilst designing low noise amplifiers. The derivations though I have not shown for how we got that equation for the noise figure the derivations are given in the book by Gonzales. I urge you to go through it once.

Thank you!