

Power System Analysis
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Lecture - 58
Power System Stability (Contd.)

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$$X_{eq} = \left(0.25 + 0.15 + \frac{0.2 \times 0.2}{0.4} \right) = \underline{0.50 \text{ pu}}$$
$$\cos \phi = 0.80; \quad \therefore \phi = 36.87^\circ \text{ (lagging)}$$

current into bus-2 is:

$$I = \frac{1.0}{1 \times 0.80} \angle -36.87^\circ = 1.25 \angle -36.87^\circ \text{ pu}$$

The voltage E_g is then given by

$$|E_g| \angle \delta = |V_2| \angle 0^\circ + j X_{eq} I$$
$$\therefore |E_g| \angle \delta = 1 \angle 0^\circ + j 0.5 \times 1.25 \angle -36.87^\circ$$
$$\therefore |E_g| \angle \delta = \underline{1.463} \angle \underline{20^\circ}$$
$$\therefore |E_g| = \underline{1.463 \text{ pu}}; \quad \delta = \underline{20^\circ}$$

Now, voltage E_g is then given by magnitude E_g angle δ is equal to magnitude your voltage V_2 angle 0 plus $j X_{eq} I$ had very the circuit diagram I mean if you make it like a circuit.

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$|E_g| \angle \delta$ $\rightarrow I$ $|V_2| \angle 0^\circ$
 jX_{eq}

$X_{eq} = (0.25 + 0.15 + \frac{0.2 \times 0.2}{0.4}) = 0.5 \text{ pu}$ (31)

$\cos \phi = 0.80; \therefore \phi = 36.87^\circ \text{ (lagging)}$

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The voltage E_g is then given by

$|E_g| \angle \delta = |V_2| \angle 0^\circ + jX_{eq} I$

So, this is your one bus bar, this is your infinite bus equivalent size about this thing. This is your angle $E_g \delta$ and current flowing through this is I , it is $j X_{eq}$ and this is $V_2 \angle 0$. So, that is the equivalent circuit if you do like this because X_{eq} any X_{eq} we have got 0.5 here. So, this way the current I also computed. This way if you make it then your magnitude $E_g \angle \delta$ we can write magnitude $V_2 \angle 0$ degree plus $j X_{eq} I$, but you know this magnitude V_2 is given 1 and X_{eq} we got 0.5 and I also you have got this value if you put it you will get magnitude $E_g \angle \delta$ is equal to 1.463 angle your 20 degree. Therefore, voltage magnitude 1.463 per unit E_g and δ is equal to 20 degree.

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$$P_e = \frac{E_g \cdot V_2}{X_{eq}} \sin \delta = \frac{1.463 \times 1}{0.5} \sin \delta$$
$$\therefore P_e = 2.926 \sin \delta$$

From eqn. (20),

$$\frac{H}{\pi f} \frac{d^2 \delta}{dt^2} = P_i - P_e \quad \dots (i)$$

If it is desired to work in electrical degrees then eqn. (i) can be written as:

$$\frac{H}{180f} \cdot \frac{d^2 \delta}{dt^2} = P_i - P_e \quad \dots (ii)$$

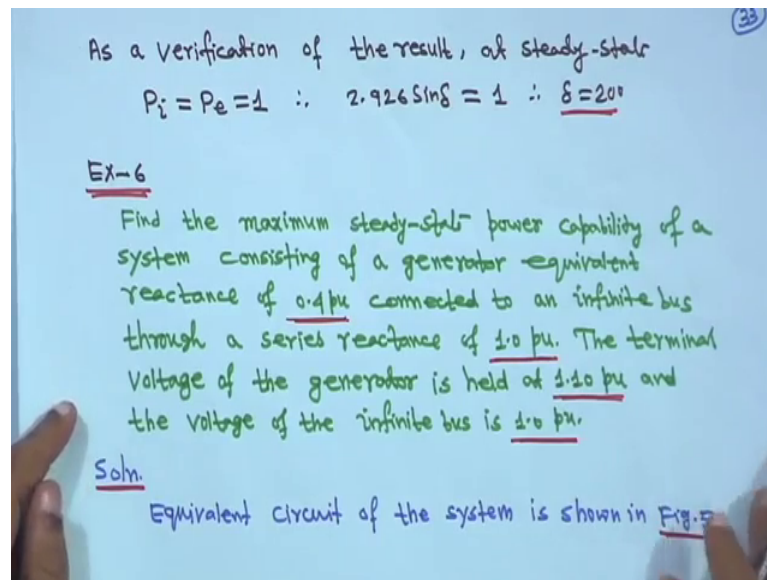
Here, $P_i = 1.0$ pu mechanical power input to the generator

$$\therefore \frac{H}{180f} \frac{d^2 \delta}{dt^2} = 1.0 - 2.926 \sin \delta$$

And next is that P_e is equal to E_g into V_2 up on x cube X_{eq} sin δ , therefore P is equal to E_g is 1.463 into 1 X_{eq} is 0.5 sin δ . Then with P is equal to 2.926 sin δ . Now from equation 20: this is the equation H up on π d square δ dt square is equal to P_i minus P_e . This is from equation 20. Now if it is desired to work in electrical degrees then this equation 1, I mean we are repeating equation 20, right. That is H up on 180 f into d square δ up on dt square is equal to P_i minus P_e . This is equation 2 say.

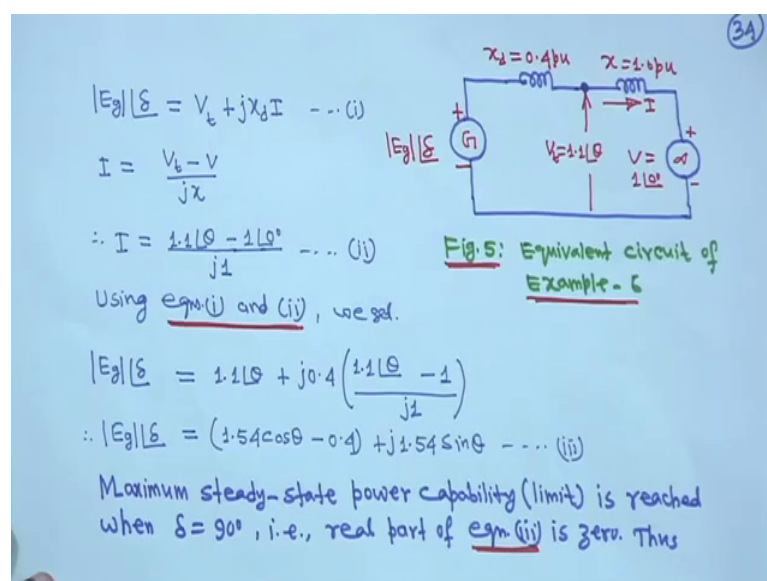
Now here P_i is equal to 1.0 per unit mechanical power input to the generator, therefore this can be written as H is by 180 f into d square δ dt square is equal to 1 minus 2.926 sin δ ; so as a verification right. At steady state your it your at steady state you will find that 1 minus 2.926 sin δ is equal to 0 and if you compute δ δ will become 20 degree. And there also you have got where this here also we have got δ is equal to 20 degree.

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So, this is the swing equation. Here also you will get as a verification of the result a steady state P_i is equal to P_e is equal to 1 therefore $2.926 \sin \delta$ is equal to 1, therefore δ is equal to 20 degree right. Now example 6: it is given that find the maximum steady state power capability of a system consisting of a generator equivalent reactance of 0.4 per unit, connected to an infinite bus through a series reactance of 1 per unit. The terminal voltage of the generator is held at 1.10 per unit and the voltage of the infinite bus is 1 per unit. That means if you put that all this language in the diagram that how it is given that equivalent circuit of the system.

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So, it is actually that generator voltage excited that is your E_g angle δ and this is given what you call generator equivalent reactance 0.4 per unit. So, this is x_t we are writing say 0.4. And your through a series reactance of 1 per unit, so this series reactance here it is 1 per unit and terminal voltage it is given 1.10 your magnitude. So, we are writing V_t is equal to 1.1 angle θ an infinite bus voltage is given it is 1 angle 0. So, you have to find out the maximum steady state power capability. So, this whatever has been x_t your mentioned here we are putting in this diagram.

Now what we will do that first you apply your what you call your KVL in this So, it is your magnitude E_g angle δ is equal to your $j X_d I$ $j X_d$ into current flowing through this is I plus V_t . This is one equation. Similarly, here I is equal to you can write V_t minus V divided by x_t ; this is series this x_t I mean here. So, I is equal to we can write V_t minus V up on x_t ; that means, we can write I is equal to V_t minus V up on your reactance it is, so $j x_t$ right.

So, I is equal to $1.1 \angle \theta$ minus $1 \angle 0$ divided by $j 1$. So, now, this equation using equation 1 and 2; that means, this I you substitute here you substitute here. If you do so and then your magnitude E_g angle δ again and again not calling magnitude understandable easy angle δ is equal to $1.1 \angle \theta$ plus $j 0.4$ $1.1 \angle \theta$ minus 8 upon $j 1$ if you simplify this if you simplify this you will get angle E_g your E_g angle δ is equal to $1.54 \cos \theta$ minus 0.4 plus $j 1.54 \sin \theta$. This is equation 3.

Now maximum steady state power capability limit is limit can be reached when δ is equal to 90 degree. That means real part must be is 0, if real part 0 then δ will become 90 degree. So, that means, if you put this one real part is equal to 0 then you will get the θ value. That means, $1.54 \cos \theta$ minus 0.4 is equal to 0, therefore you will get θ is equal to 74.9 degree. That means, if this part is 0 then magnitude E_g actually will become $1.54 \sin \theta$.

So, that is why magnitude of E_g is equal to $1.54 \sin \theta$ is equal to 74.9 degree; that means, you will get magnet is equal to 1.486 per unit. That means V_t is equal to actually $1.1 \angle \theta$.

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$$\begin{aligned} \therefore 1.54 \cos \theta - 0.4 &= 0 \\ \therefore \theta &= \underline{74.9^\circ} \\ \therefore |E_g| &= 1.54 \sin(74.9^\circ) \\ \therefore |E_g| &= \underline{1.486 \text{ pu.}} \\ V_t &= \underline{1.1 \angle 74.9^\circ} \\ P_{\max} &= \frac{|E_g| |V|}{(x_d + x)} = \frac{1.486 \times 1.0}{(0.4 + 1)} = \underline{1.061 \text{ pu.}} \end{aligned}$$

Equal-Area Criterion

A solution to the swing equation for $\delta(t)$, leads to the determination of the stability of a single machine operating as part of a large power system.

So, theta we have got. So, V_t is equal to 1.1 angle 74.9 degree. Then with P_{\max} is equal to E_g into v divided by $x_d + x$; that is your here magnitude E_g into v divided by $x_d + x$ the whole reactance of the line. So, it is actually 1.486 into 1 divided by 0.4 plus 1 that is equal to 1.061 per unit. So, with that we have taken few examples from the point of view of swing equation as well as steady state stability.

Next will come to the equal area criterion; now a solution to the swing equation for $\delta(t)$ is a function of t leads to the determination of the stability of a single machine operating as a part of large power system; that means whenever you try to it is this thing your solution for swing equation you have to go for some iterative technique. It leads to a determination of the stability of a single machine operating as a part of large power system. But we will see some, so that what you call that equal area criterion.

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However, solution of swing equation is not always necessary to investigate the system stability. Rather, in some cases, a direct approach may be taken. Such an approach is based on the equal-area criterion.

Now consider eqn. (28),

$$M \frac{d^2 \delta}{dt^2} = P_i - P_e = P_a$$

$$\therefore \frac{d^2 \delta}{dt^2} = \frac{P_a}{M} \dots (39)$$

As shown in Fig. 6, in an unstable system, δ increases indefinitely with time and machine loses synchronism.

Fig. 6: Plot of δ

However, solution of swing equation is not always necessary to investigate the system stability. All the time we do not. So, rather in some cases a direct approach may be taken such an approach is based on equal area criterion. For example, just come to that just consider equation 18 that $M \frac{d^2 \delta}{dt^2} = P_i - P_e = P_a$ is the accelerating power. That means, $\frac{d^2 \delta}{dt^2} = \frac{P_a}{M}$. This is equation 39.

Now if this is δ and this is t if that graph δ versus time we have moves like this then system is unstable. But if it oscillates and die out that at particular at any point that $\frac{d \delta}{dt}$ will be 0. So, as shown in figure 6 in an unstable system δ increases in the in your indefinitely it is continuously increasing with time and machine loose synchronism. So, it is unstable system, because δ is continuously increasing. But if the stable system δ undergoes oscillation; that means, in a stable systems which undergoes oscillation which eventually die out due to damping. So, it will go like this and finally it will die or what you call that oscillation will die out due to damping.

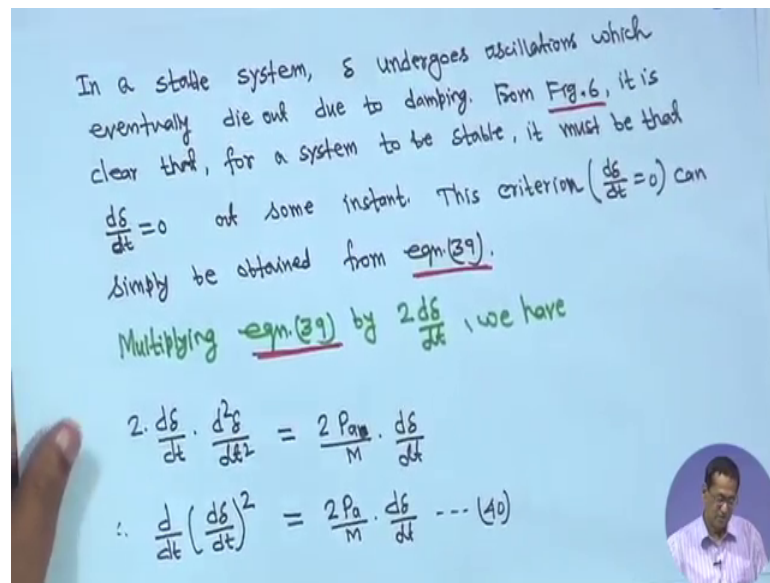
So, from this it is clear that it must be what you call for a stable system then at some point $\frac{d \delta}{dt}$ has to be 0. This criterion can simply be obtained from equation 39; from this one that if $\frac{d \delta}{dt}$ is 0 like this then system will become stable it will oscillate; and finally oscillation will die out.

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In a stable system, δ undergoes oscillations which eventually die out due to damping. From Fig.6, it is clear that, for a system to be stable, it must be that $\frac{d\delta}{dt} = 0$ at some instant. This criterion ($\frac{d\delta}{dt} = 0$) can simply be obtained from eqn.(39).

Multiplying eqn.(39) by $2 \frac{d\delta}{dt}$, we have

$$2 \cdot \frac{d\delta}{dt} \cdot \frac{d^2\delta}{dt^2} = \frac{2 P_a}{M} \cdot \frac{d\delta}{dt}$$

$$\therefore \frac{d}{dt} \left(\frac{d\delta}{dt} \right)^2 = \frac{2 P_a}{M} \cdot \frac{d\delta}{dt} \quad \dots (40)$$


So, multiply equation 39; that means this equation both side you multiply by 2 into δ by dt . So, if we multiply this two δ by dt on both side then $2 d\delta dt$ into $d^2\delta dt^2$ is equal to $2 P_a M$ into $d\delta dt$. So, left hand side can be written as $d dt$ or $d dt$ of $d\delta dt$ whole square if you take its derivative it will come like this. So, we are writing $d dt$ of $d\delta dt$ whole square is equal to $2 P_a$ up on M into $d\delta dt$. This is equation 40.

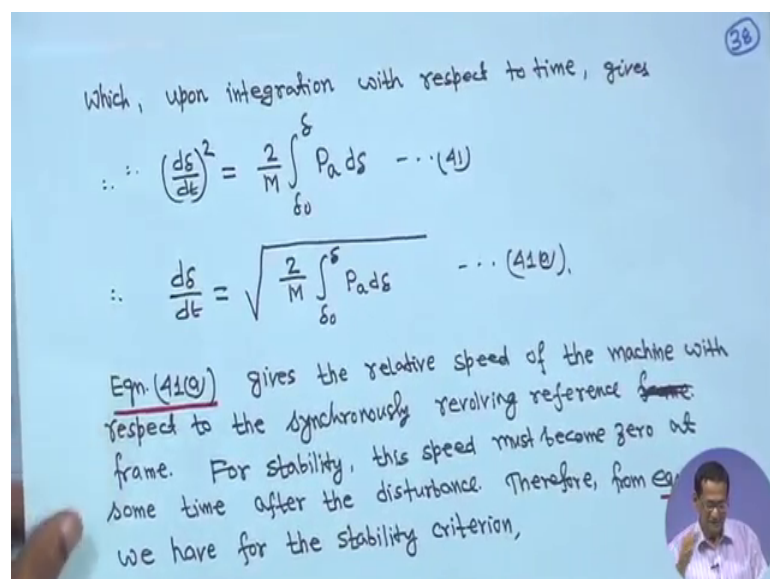
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Which, upon integration with respect to time, gives

$$\therefore \left(\frac{d\delta}{dt} \right)^2 = \frac{2}{M} \int_{\delta_0}^{\delta} P_a ds \quad \dots (41)$$

$$\therefore \frac{d\delta}{dt} = \sqrt{\frac{2}{M} \int_{\delta_0}^{\delta} P_a ds} \quad \dots (41B)$$

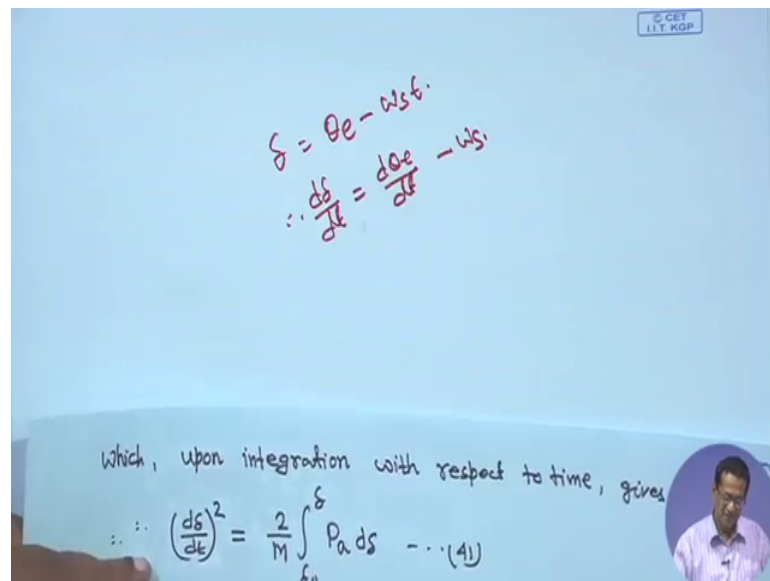
Eqn.(41B) gives the relative speed of the machine with respect to the synchronously revolving reference ~~frame~~ frame. For stability, this speed must become zero at some time after the disturbance. Therefore, from eqn. we have for the stability criterion,



So, that means, which up on integration if you integrate this equation 40 then it will be a $d\delta$ by dt whole square is equal to 2 by M your δ_0 to some angle say δ into P_a into $d\delta$. This is equation 41. So, or $d\delta$ by dt is equal to your root over 2 by M δ_0 to δ P_a $d\delta$. This is equation 41 a. Now this is this is 41, this is 41 a.

Now this equation 41 a actually gives the relative speed of the machine with respect to the synchronously revolving reference frame here.

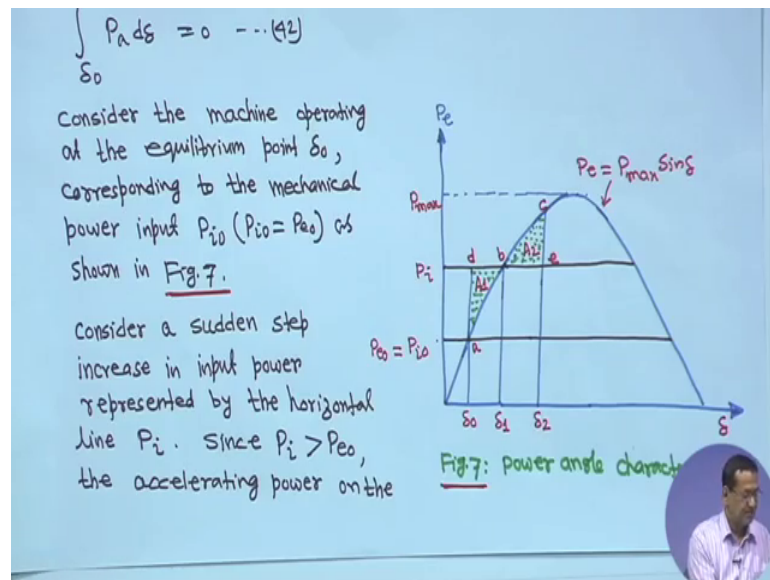
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We assume know somewhere that δ is equal to θe minus $\omega_s t$; that means, $d\delta$ by dt is equal to your $d\theta e$ dt minus ω_s ; That means, the same thing it gives the relative speed of the machine with respect to the synchronously revolving reference frame. So, for stability the speed must become 0; that means $d\delta$ by dt it must be your equal to 0.

So, that means, at some time after the disturbance. That means, your what you call therefore, from equation 41 a we have the we have further stability here. So, for stability the speeds must become 0 at some time after the disturbance. That means, I showed you know this graph that for stability somewhere $d\delta$ by dt has to be 0. So, in that case from equation 40 if $d\delta$ by dt 0 then integral of δ_0 to δ P_a $d\delta$ it can be written as 0.

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Therefore, we can write this that δ_0 to δ P_a δ is equal to 0. Say this is equation 42. Now you consider the machine that now will come to that what is equal area criterion. So, you consider the machine operating at an equilibrium point δ_0 . This is the equilibrium point that is your δ_0 . And corresponding to the mechanical power input P_{i0} ; this is the mechanical power, but this horizontal line this horizontal line mechanical power P_{i0} , but we are writing P_{e0} is equal to P_{i0} ; as shown in figure 7.

So, consider a sudden step increase in input power represented by the your horizontal line P_i . That means it was operating at steady state condition, but suddenly that your input power that increased for up to your P_i . So that means, say $P_i > P_{e0}$ or P_{i0} , I say $P_i > P_{e0}$. Suddenly your what you call input power is increased. So, in that case and $P_i > P_{e0}$ then P_i then greater than your P_{e0} then; that means, the accelerating power on the rotor is positive. And the power angle δ increases.

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Rotor is positive and the power angle δ increases. (10)

The excess energy stored in the rotor during the initial acceleration is

$$\int_{\delta_0}^{\delta_1} (P_i - P_e) d\delta = \text{area abd} = \text{area } A_1$$

$$\therefore \int_{\delta_0}^{\delta_1} (P_i - P_{\max} \sin \delta) d\delta = \text{area } A_1 \dots \dots \text{eqn (2)}$$

With increase in δ , the electrical power increases, and when $\delta = \delta_1$, the electrical power matches the new input power P_i .



So, as soon as your because this P_i actually your greater than your P_{e0} the accelerating power on the rotor is positive and the power angle δ increases, because δ now will increase δ will increase. So, what will happen that excess energy stored in the rotor during the initial acceleration is it will be δ_0 to δ_1 that is your δ this diagram that δ_0 to δ_1 , because it has increased from your suddenly to P_i . So, this is the horizontal line it is cutting here this sin curve that is your power your power curve at this point that is b right.

So, whenever that means, δ_0 to δ_1 that is that excess energy stored in the rotor due to initial acceleration that P_i minus P_e δ that is area a b d; that is this area a 1 area a b d right. And that can be equal to I am writing area a 1 or δ_0 to δ_1 is P_i and P_e is equal to $P_{\max} \sin \delta$. So, we are writing P_i minus $P_{\max} \sin \delta$ d δ this is area a 1. So, this is I am marking as equation 42 a. This is that excess energy stored in the rotor during the initial acceleration, because as soon as this P_i suddenly load has increased input power increase to P_i then rotor will start accelerating. So that means, what you call this excess energy stored will be only this area you have to find out a 1.

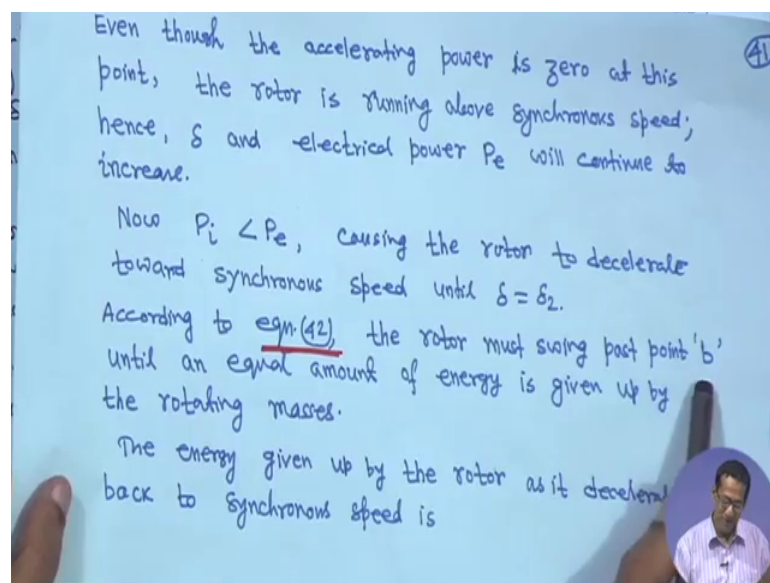
Similarly with the increase in δ the electrical power increases, because as δ is increasing then electrical power P also will increase. So, electrical power increases. And when δ is equal to δ_1 right I mean this value when δ is equal to δ_1 ; the electrical power matches the new input power P_i . That means, when δ is equal to

delta 1 you will get P is equal to $P_{\max} \sin \delta_1$, but that means, at that time your P_i will become $P_{\max} \sin \delta_1$. It matches your new input power P_i .

So, if it is so even though; that means, at this point your accelerating power is 0. At this point because P_i when it is coming to this point P_i is becoming your P_e is becoming $P_{\max} \sin \delta_1$ when δ is equal to δ_1 . So, at that time P_i will be I can say this is my P_1 $P_{\max} \sin \delta_1$ I have written when δ is equal to δ_1 P_1 is equal to $P_{\max} \sin \delta_1$ at this point P_i is equal to P_1 . So, it is to that means P accelerating power is 0 at this point if it matches.

So, that is why that is the electrical power matches the new input power P_i . So, in this case even though the accelerating power is 0 at this point the rotor is running actually above the synchronous speed, because it was accelerating. Although at this point that you are electrical this power is equal to that electrical power matching with this input power, but rotor is accelerating, so it is running above the synchronous speed.

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That means, what will happen then; hence δ and electrical power P will continue to increase. So, your δ will continually increase, so P also will increase the electrical power continuously will increase, but how long how far?

So, it will happen; now what will happen as rotor is above the synchronous speed and as it is your what you call it is continuously the δ will increase; that means, that P at that

time if it is δ_1 is increasing; that means, P will be greater than P_i . At that time P_e will be greater than P_i , because at this any point here P_e will be greater than P_i then what will happen rotor will start decelerating till it achieves its synchronous speed say at point c. That means, the rotor is running above synchronous speed hence δ and electrical power P will continue to increase.

That is why I am telling, now when P_i less than P_e negative. So, even P_i less than negative my rotor will decelerate. They consider the rotor to decelerate towards synchronous speed until δ is equal to δ_2 . When it achieves here δ is equal to δ_2 that it reaches to synchronous speed that is your say at point c. So, until δ is equal to δ_2 .

So, according to equation 42 that means your this equation according to equation 42 this equation the rotor must swing past point b until an equal terminal amount of energy is given up by the rotating mass. Up to this it was energy was stored right, and it will reach to a point; it will start oscillate until past point b until a point. That is when δ is equal to δ_2 it will what you call it will that your until and it equal amount of energy is given up by the rotating masses. Then whatever energy stored same amount of energy will be given up till it reaches at point δ is equal to δ_2 .

So, the energy given up by the rotor as it decelerates back to synchronous speed is this one.

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$$\int_{\delta_1} (P_e - P_i) d\delta = \text{area } bce = \text{Area 2} = A_2 \dots 42(b)$$

The result is that the rotor swings to point 'b' and the angle ~~is~~ δ_2 , at which point

$$\text{Area 1} = \text{Area 2} \dots 42(c)$$

This is known as the equal-area criterion.

The rotor angle would then oscillate back and forth between δ_1 and δ_2 at its natural frequency.

The damping present in the machine will cause these oscillations to subside and the new steady state operation would be established at point 'b'.

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So, the energy given up by the rotor as it decelerates back to synchronous speed it can be given as your you do your P_e , because at that time your P_e is greater than P_i . So, it is del integration will be δ_1 to δ_2 and it will be the integration of the P_e minus P_i $d\delta$ δ_1 is equal to area bce area is equal to area this area a 2 bce; is equal to area a 2.

Actually, somewhere you can also write some book also you can find that decelerating energy; you will find some somewhere there I also writing δ_1 to δ_2 they are writing P_i minus P_e $d\delta$ then we area will be this inter area will become negative after that they are telling taking that absolute of area 1 is equal to absolute a period; that is also true. But directly we are writing in that case if you take that P_i minus P_e $d\delta$ decelerating means it will become negative. And here it is storing, so it will be positive and when it is your what you call a decelerating side it will become negative. But here we have written δ_1 to δ_2 P_e minus P_i $d\delta$; that is area bce is equal to area a 2. This is equation say 42 b.

Now result is that the rotor swings to point b and the angle δ_2 . That mean rotor will swing till δ_2 and this area δ_2 that area 1 must be equal to area 2. So, this area 1 must be equal to area 2, because I said the rotor must swing past point b until an equal amount of energy is given up by the rotating masses. So, in that case it will be area 1 is equal to area 2; this equation I am giving 42 c.

Now what is the basic philosophy? That suddenly power has increased to P_i . So, in that case what will happen that P_i will be greater than P_e . So, rotor will start accelerating, and when it is accelerating it will come to a point when δ is equal to δ_1 . At the time P_i is equal to your this P is equal to P_i ; that means, accelerating power is 0. And if this term the rotor is storing energy. Now at this point the rotor is running above synchronous speed; that means, rotor will continue to; that δ will continue to increase because it is running your above synchronous speed till the point say c that is δ_2 and until it give up the equivalent amount of energy as it is a 1. So, it is going up to c.

So, this way this is accelerating energy this is decelerating energy both have to be equal; though area a 1 must be equal to area 2. But question is that is up to the synchronous speed till it is a synchronous speed. So, ultimately what will happen that area 1 must be, this is known actually equal area criterion. So, this is area 1 and this is area 2.

Actually, it will swing back and forth back and forth and because of the machine damping finally after some time it will settle to point b. So, these is the rotor angle would then oscillate back and forth between delta 0 and delta 2. I told you between delta 0 and delta 2 it will be swing back and forth and finally at its natural frequency. So, as damping present in the machine right will cause these oscillations to subside and new what you call new steady state operation would be established at point b, after some time this will oscillate back and forth. Finally, it will be stable at this point b. So, this is actually is called equal area criterion.

So, I hope this part is understandable. So, idea is that when it is going pass to up to this that power has increased to P_i and then it is accelerating, but it is above synchronous speed so it is further it will your actually your accelerate, but still it achieves to synchronous speed at the time P greater than your what you call P_i so it will decelerate. And finally, it will achieve a point your delta 2. So, this is actually power angle characteristic of your machine.

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Area 1 = Area 2

$$\therefore \int_{\delta_0}^{\delta_1} (P_i - P_{\max} \sin \delta) d\delta = \int_{\delta_1}^{\delta_2} (P_{\max} \sin \delta - P_i) d\delta \quad \dots (43)$$

$$\therefore P_i (\delta_1 - \delta_0) + P_{\max} (\cos \delta_1 - \cos \delta_0) = P_i (\delta_1 - \delta_2) + P_{\max} (\cos \delta_2 - \cos \delta_1) \quad \dots (44)$$

→ But $P_i = P_{\max} \sin \delta_1$,
which when substituted in eqn. (44), we get,

$$P_{\max} (\delta_1 - \delta_0) \sin \delta_1 + P_{\max} (\cos \delta_1 - \cos \delta_0) = P_{\max} (\delta_1 - \delta_2) \sin \delta_1 + P_{\max} (\cos \delta_2 - \cos \delta_1) \quad \dots (45)$$

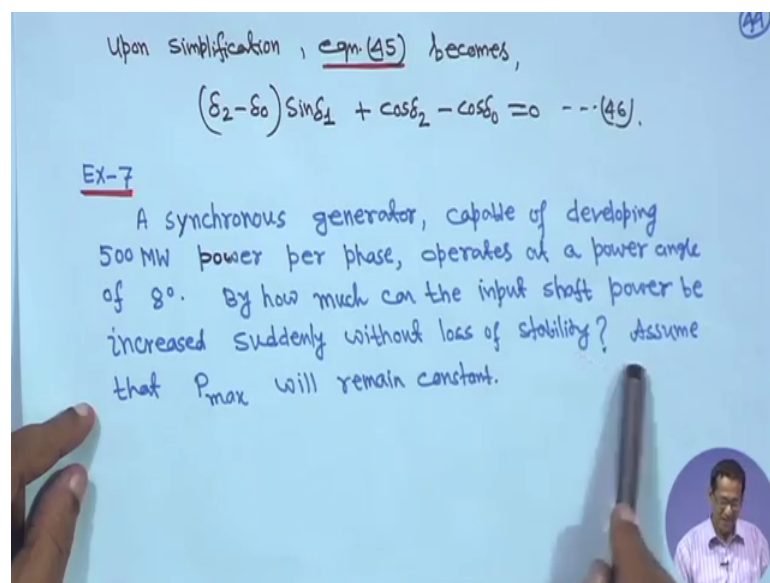
Therefore, if area 1 is equal to area 2 then this we can write all this equations shown that delta 0 delta 1 is equal to P_i minus P_e max sin delta d delta is equal to integral delta 1 to delta 2 $P_{\max} \sin \delta$ minus P_i d delta. This is equation 43.

Now if you integrate and if you simplify it will come like this: P_i into delta 1 minus delta 0 plus $P_{\max} \cos \delta_1$ minus $\cos \delta_0$ is equal to P_i into delta 1 minus delta 2 plus $P_{\max} (\cos \delta_2 - \cos \delta_1)$

max into $\cos \delta_1 - \cos \delta_2$. This is equation 44. But P_i is equal to $P_{\max} \sin \delta_1$ from this equation that P_i here is equal to when δ is equal to δ_1 P_i will be $P_{\max} \sin \delta_1$. So, if you substitute here P_i is equal to $P_{\max} \sin \delta_1$ and if you put it here and simplify it will become $P_{\max} \delta_1 - \delta_0 \sin \delta_1 + P_{\max} \cos \delta_1 - \cos \delta_0$ is equal to $P_{\max} \delta_1 - \delta_2 \sin \delta_1 + P_{\max} \cos \delta_1 - \cos \delta_2$. This is equation 45.

If you simplify this something will be canceled; I am giving you the final form.

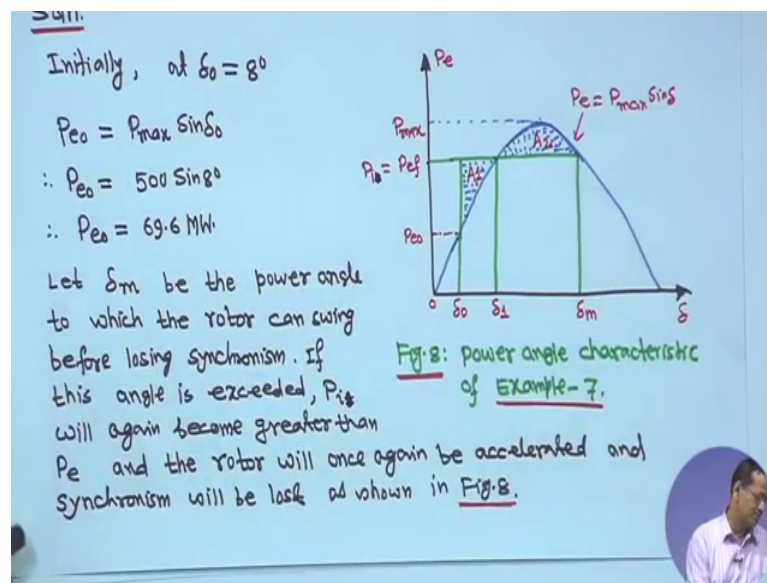
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If you simplify this then it will become that $\delta_2 - \delta_0 \sin \delta_1 + \cos \delta_2 - \cos \delta_0$ is equal to 0. This is equation 46. So, this one actually that equal area criterion whatever you have got different conditions are there; different conditions are there. So, for this thing although will solve in the next class, but I am giving you.

A synchronous generator capable of developing 500 megawatt power per phase, operates at a power angle of say 8 degree. By how much can the input shaft power be increased suddenly without loss of stability? Assume that P_{\max} will remain constant. Somewhere we will find this kind of problem has been taken as an mathematical development.

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But what we will do it; that we have taken this one. So, maximum will be your what you call that this is P_0 suddenly it has increased to P_i and this is that maximum angle it can go up to δ_m . If it goes somewhere I mean more than δ_m then what will happen P will be less than your P_i system will become unstable. So, I will come to that.

So, P_{e0} is equal to $P \sin \delta_0$ P_{e0} is equal to $P_{max} \sin \delta_0$. That is it is coming 69.9 megawatt. Now δ_m be the power angle to which the rotor can swing before losing synchronous. This is the maximum one can go. If this angle is exceed P_i I mean if it comes somewhere here say then that again it because that P will be what you call; that P_i will be again become that P_i will be greater than your P_e , because if it comes somewhere here. If it goes below that then P_i will be greater P_i somewhere here; P_i will be greater than P_e . And rotor will again we accelerated and it will lose synchronism.

So, maximum it can go up to this δ_m P is this is your δ is equal to δ_m and you have to find out this δ_m . So, P your P_i cannot be greater than P_e , if it goes more than δ_m then it will start accelerating and system will your go out of your what you call step. So, this is power angle characteristic of this one.

Now from this figure only and this equation we have derived that; therefore the equal area criterion requires that equation 46. That means, in this equation: equation 46 what you will do is that from this graph δ_m is equal to $\pi - \delta_1$ this is a sine curve. So, from symmetry δ_m is equal to $\pi - \delta_1$, because this is π

this is your what you call pi. So, it will be pi minus your delta 1. So, this delta M is equal to pi minus delta 1. That means, actually in this equation that delta 2 is equal to delta M is equal to your pi minus your delta 1. So basically, what you call here we have gone up to delta 2, but up to this it can come up to this delta m. So, delta 2 is equal to delta M actually what you call this.

So, instead of in this equation the delta 2 actually is equal to delta M is equal to pi minus your delta 1. So, that is for your understanding such that you should not make any this thing. This actually is equal to say delta 2. So, this delta 2 is equal to in this equation 46 you please put pi minus delta 1. Because in this equation is it up to delta 2 in this figure, but it can go up to your maximum delta M; delta 1 to delta M.

So, that is why for your understanding I am writing this is delta 2. So, put here pi minus delta M. So, here also delta 2 you put pi minus delta and minus cos delta 0.

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Therefore, the equal-area criterion requires eqn.(46) be satisfied with δ_m replacing δ_2 .

From Fig.8, $\delta_m = (\pi - \delta_1) = \delta_2$.

Therefore eqn.(46) becomes,

$$(\pi - \delta_1 - \delta_0) \sin \delta_1 + \cos(\pi - \delta_1) - \cos \delta_0 = 0$$

$$\therefore (\pi - \delta_1 - \delta_0) \sin \delta_1 - \cos \delta_1 - \cos \delta_0 = 0 \quad \dots (i)$$

Substituting $\delta_0 = 8^\circ = 0.139$ radian in eqn.(i), yields

$$\therefore (3 - \delta_1) \sin \delta_1 - \cos \delta_1 - 0.99 = 0$$

$$\therefore \delta_1 = 50^\circ$$

So, if you do. So, then as delta 0 is equal to 8 degree is equal to 0.139 radian. So, approximately 0.14 and equation 1 if you put that. So, if you put all these values then you will get 3 minus pi 3.14 and it is approximately 0.14. So, it is three approximately I am taking minus delta 1 into sin delta 1 minus cosine delta 1 minus 0.99 is equal to 0. Then with delta 1 is approximately 50 degree.

So, again repeat the delta M is nothing but delta 2; in the delta 2 is that previously previous figure equal area criteria

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Soln.

$$\text{Now, } P_{ef} = P_{\max} \sin \delta_1 = 500 \sin(50^\circ) = \underline{383.02 \text{ MW}}$$

Initial power developed by the machine was 69.6 MW.
Hence without loss of stability, the system can accommodate a sudden increase of

$$(P_{ef} - P_{e0}) = (383.02 - 69.6) = \underline{313.42 \text{ MW/phase}}$$

$$= 3 \times 313.42 = \underline{940.3 \text{ MW (3\phi)}} \text{ of input shaft power.}$$

So, with that that P f this one Pe f right just where has diagram has gone that just; let me see. But anyway the diagram here; P f, P f is equal to P max sin delta 1. So, it is delta is equal to delta 1. So, P max sin delta 1. So, 500 sin 50; so 383.02 megawatt. So, initial power delivered by the machine was 69.6 megawatt that was at this point we computed 69.6 megawatt and now hence without loss of stability the system can accommodate a sudden increase of P f minus Pe0; that is 383.02 minus 69.6. So, this is your 383.02 minus 69. So, that is 313.42 megawatt per phase. So, if it is a three phase multiplied by 3 it will become 940.3 megawatt of the your input shaft power.

Only once again before closing this lecture; that it cannot be more than your delta M then Pi will become Pe because any point as you take Pi will become greater than Pe then machine will start accelerating and it will lose synchronism.

So with that, thank you.